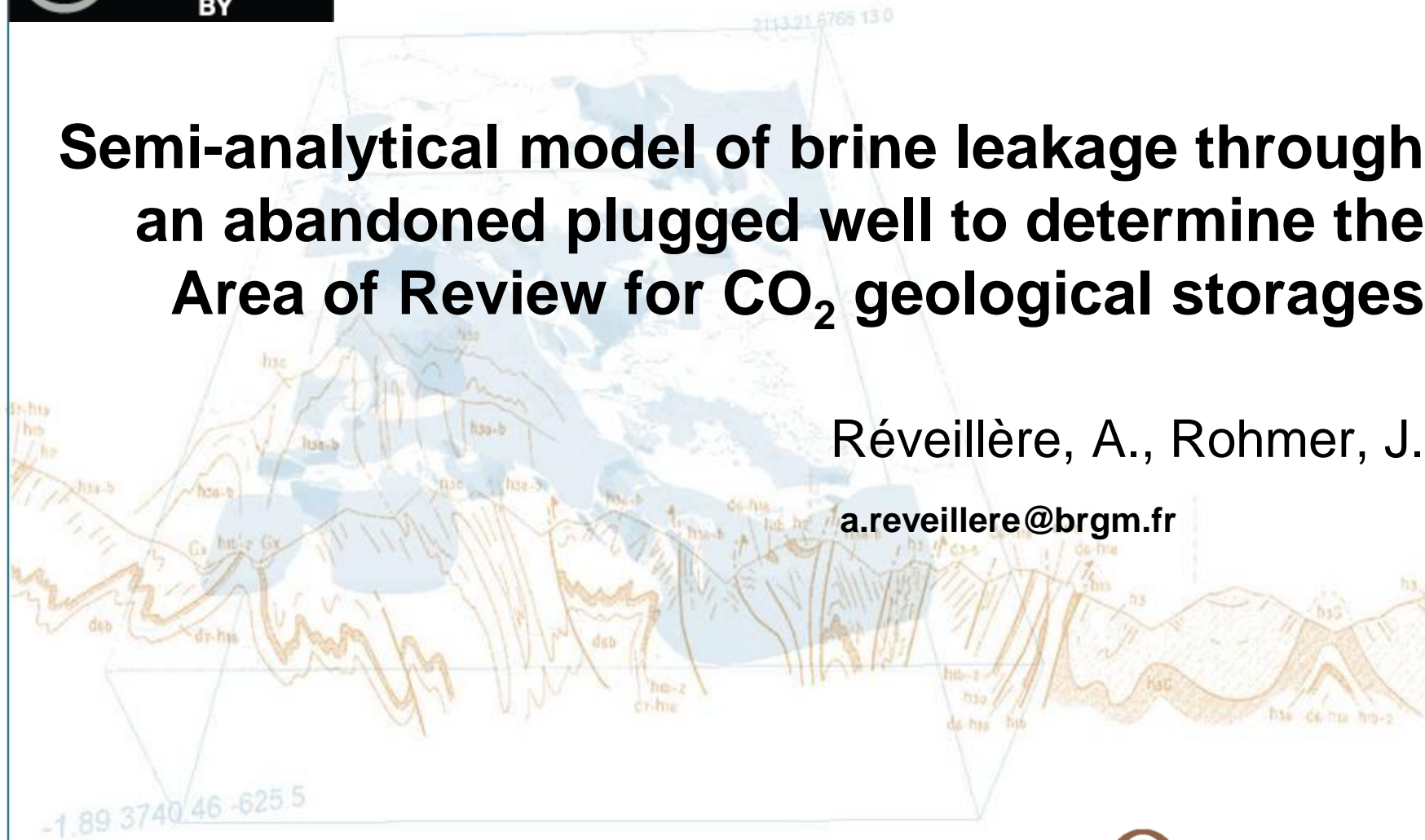




# Semi-analytical model of brine leakage through an abandoned plugged well to determine the Area of Review for CO<sub>2</sub> geological storages

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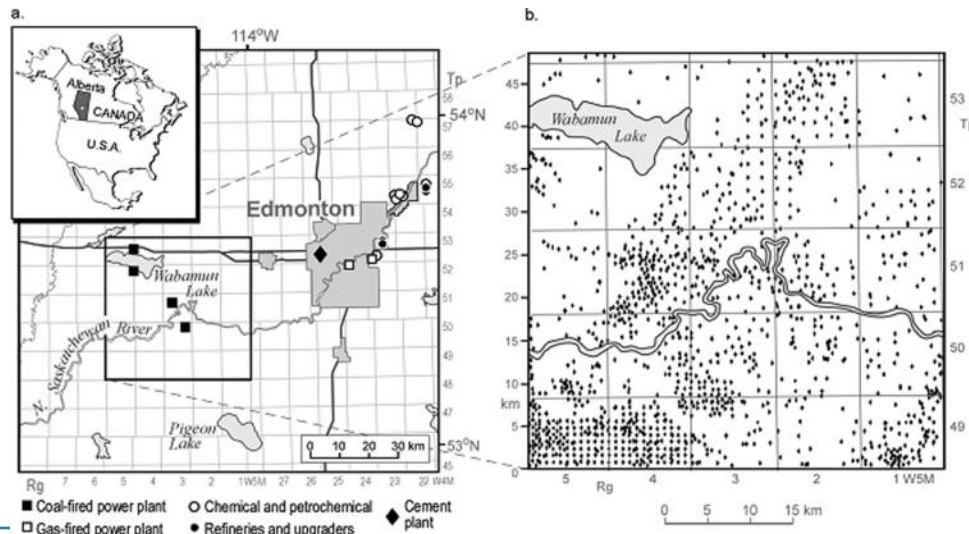
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# Abandoned wells review – context overview



- > **Many CO<sub>2</sub> storage projects target deep saline aquifers located in sedimentary basins**
  - Possible historical oil & gas operations
  - Abandoned wells with sometimes unknown plugging records
- > **By leaking through abandoned (plugged) wells, the saline brine risks to leak into overlying fresh water aquifers**
  - wells in the area where this is possible should be reviewed (“Area of review”)
  - This model enables to prioritize the areas to review supposing minimum plug parameters



**Example in Alberta, Canada: 508 wells in a 30km x 30 km area.**  
from Bachu and Celia, 2009

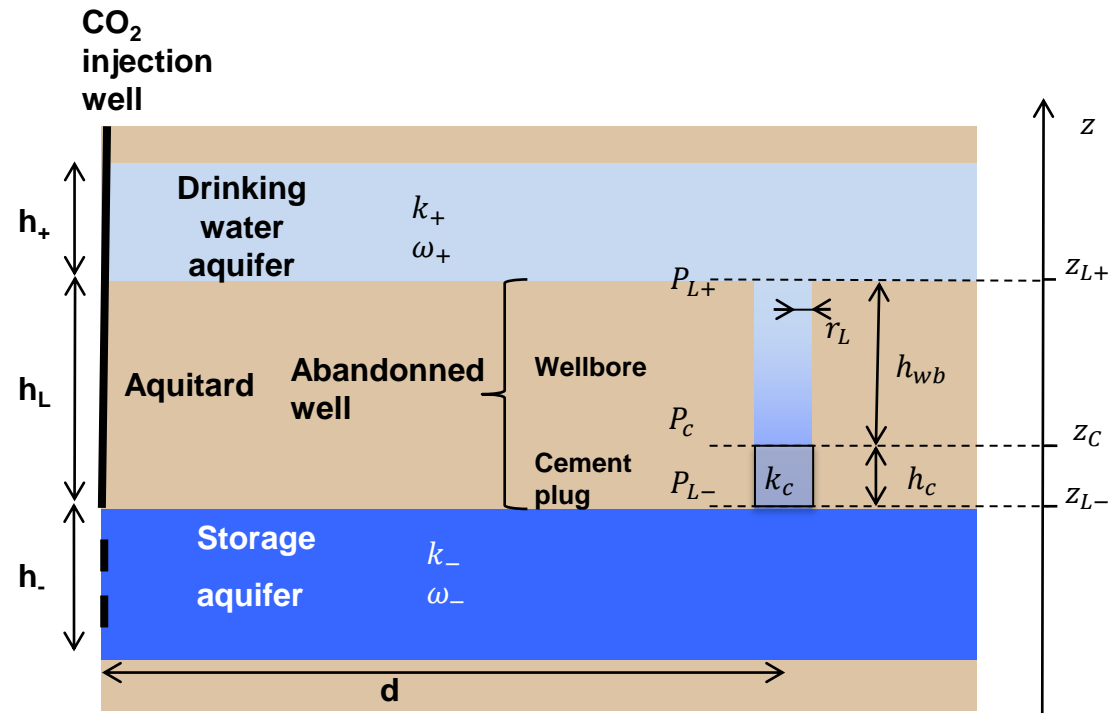
# Schematic layout of the model



## > 1 active injection well

## > 1 passive abandoned well, or « Leak »

- $z_c = z_{L-}$ : wellbore only
- $z_c = z_{L+}$ : porous column only
- $z_{L-} < z_c < z_{L+}$ : plug & wellbore

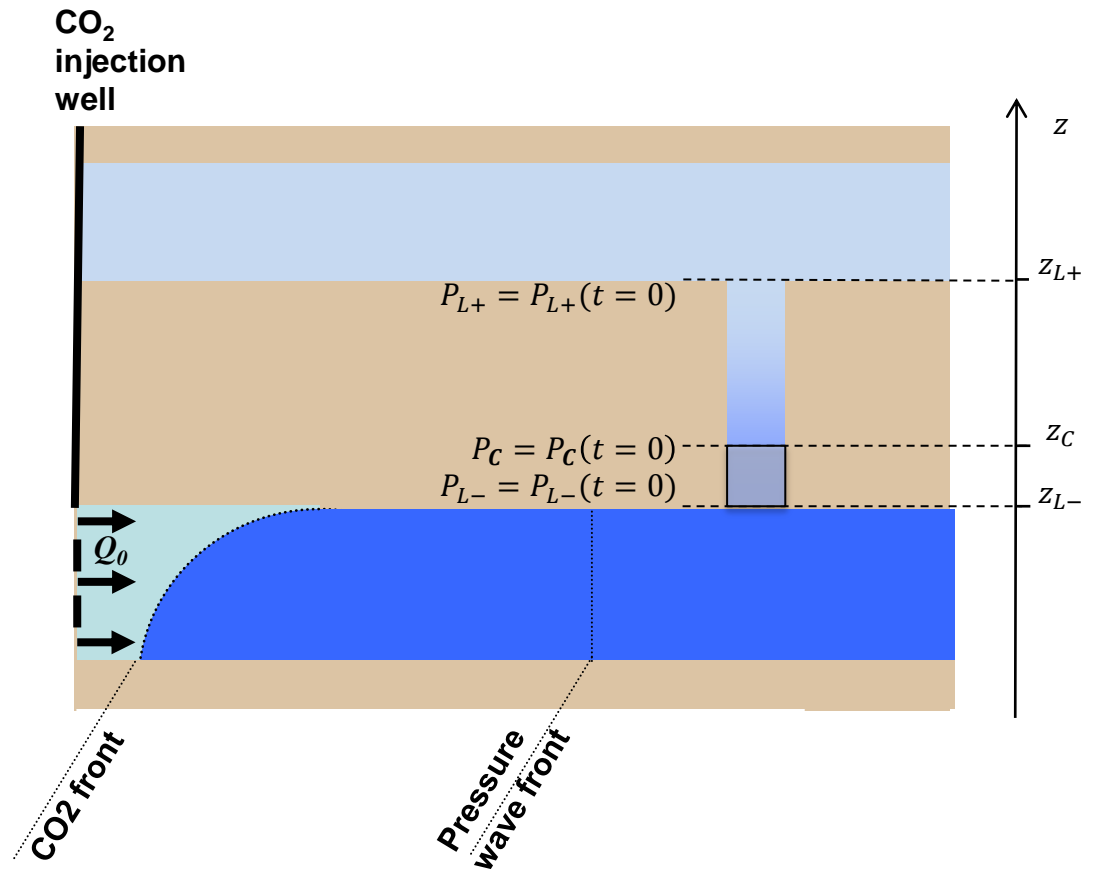


- Drinking water
- Storage aq. brine
- Wellbore brine (vertical salinity gradient)

# Beginning of CO<sub>2</sub> injection



- > Constant CO<sub>2</sub> injection flow rate starts ( $Q_0$ )

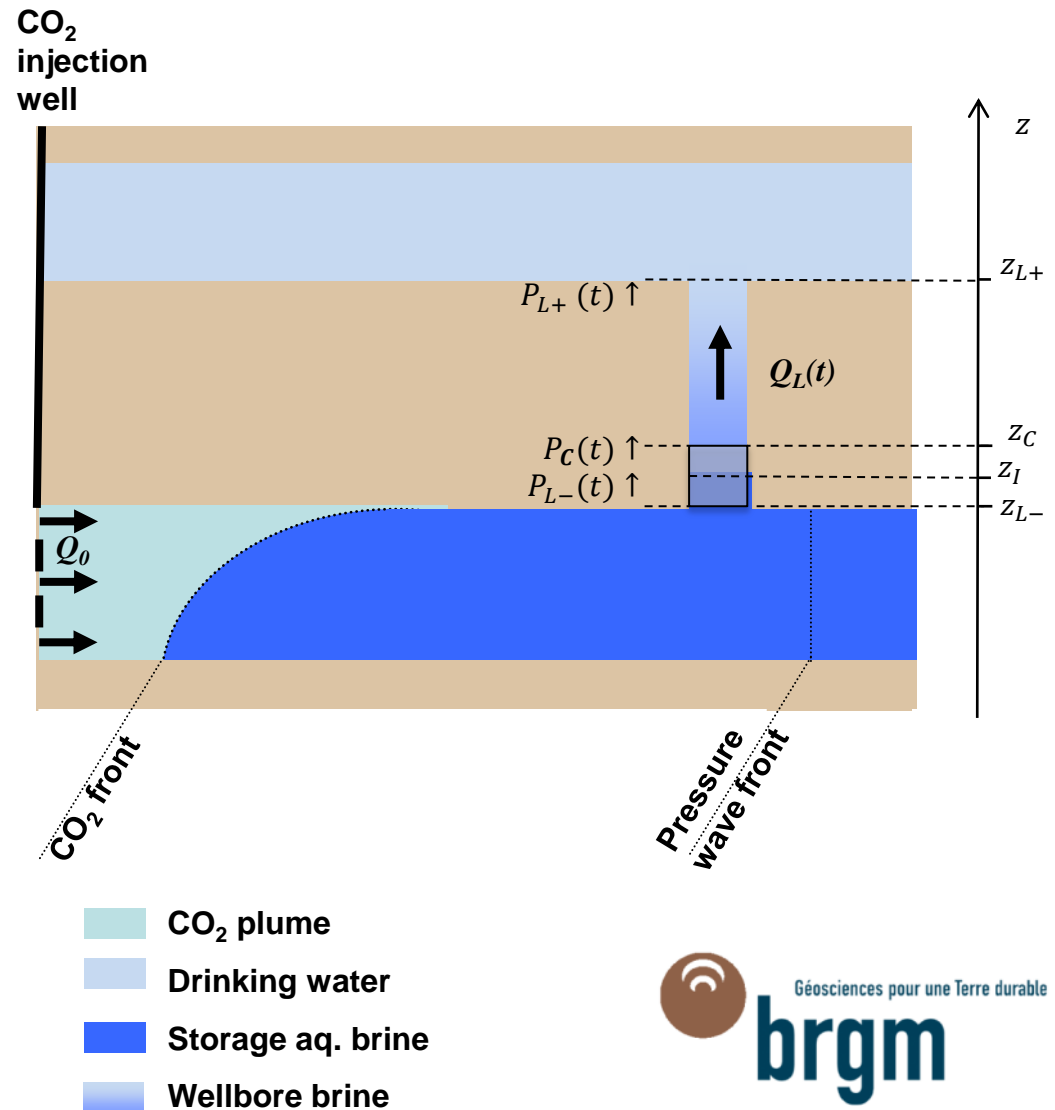


- CO<sub>2</sub> plume
- Drinking water
- Storage aq. brine
- Wellbore brine

# Brine leakage during CO<sub>2</sub> injection



- > Dense storage aquifer brine starts filling the leak up to  $z_l$
- > The « wellbore brine » is pushed up
- > Pressure increases in the abandoned well

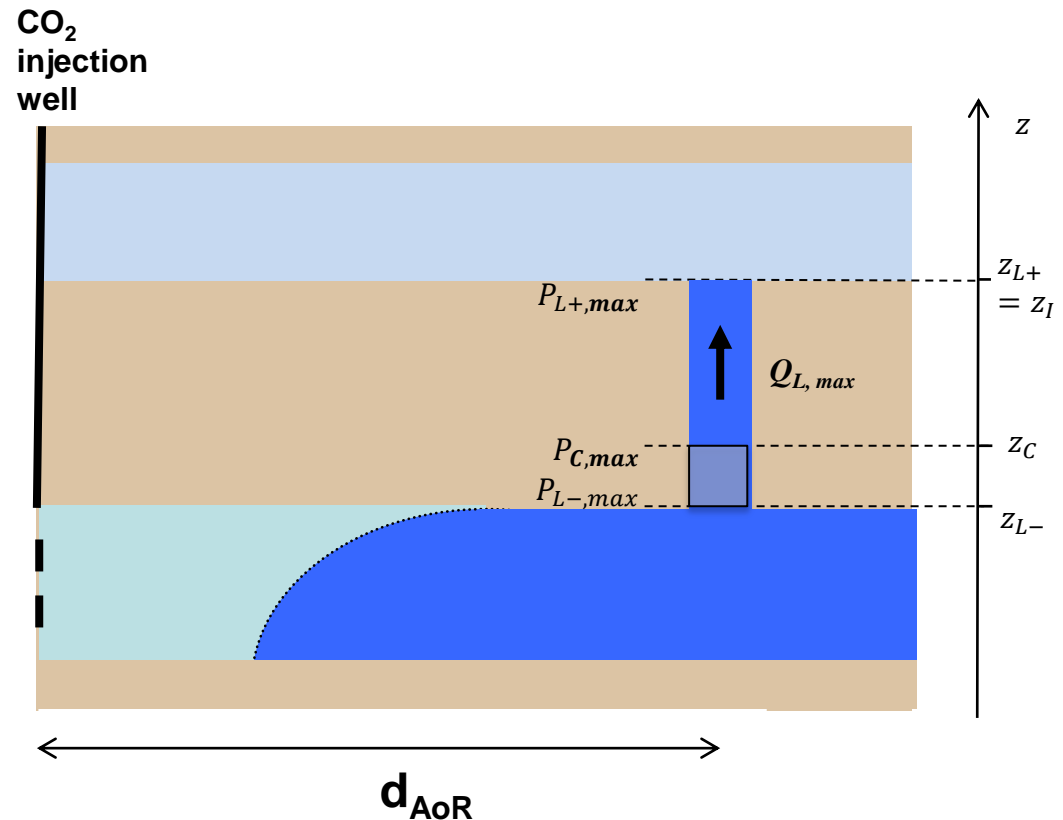


# End of the CO<sub>2</sub> injection & « AoR »



> « Area of review »  $d_{AoR}$ :

Area where the pressure changes due to the injection can drive the reservoir brine up to a shallower aquifer of interest



- CO<sub>2</sub> plume
- Drinking water
- Storage aq. brine

# Equations of the model



- > Static pressure equation in the abandoned well**
- > Pressure under the leak in the storage aquifer**
- > Pressure over the leak in the overlying aquifer**
- > Mass conservation**
- > Darcy flow in the cement plug**
- > Semi-analytical resolution**

# Static pressure equation in the abandonned well



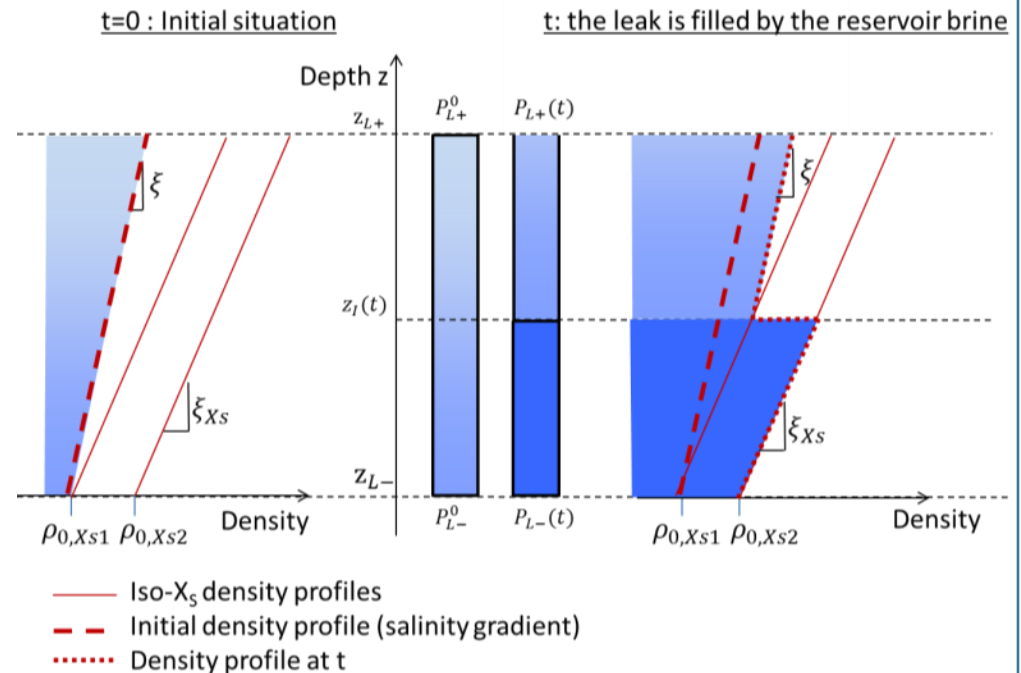
## > Well bore pressure gradient

$$\nabla P = \nabla P_{grav} + \nabla P_{fric} + \nabla P_{acc}$$

- « frictional and inertial pressure gradients contributing typically a few percent or less.” (Pruess, 2006, for geothermal wells)

- $\rightarrow \nabla P = \nabla P_{grav}$

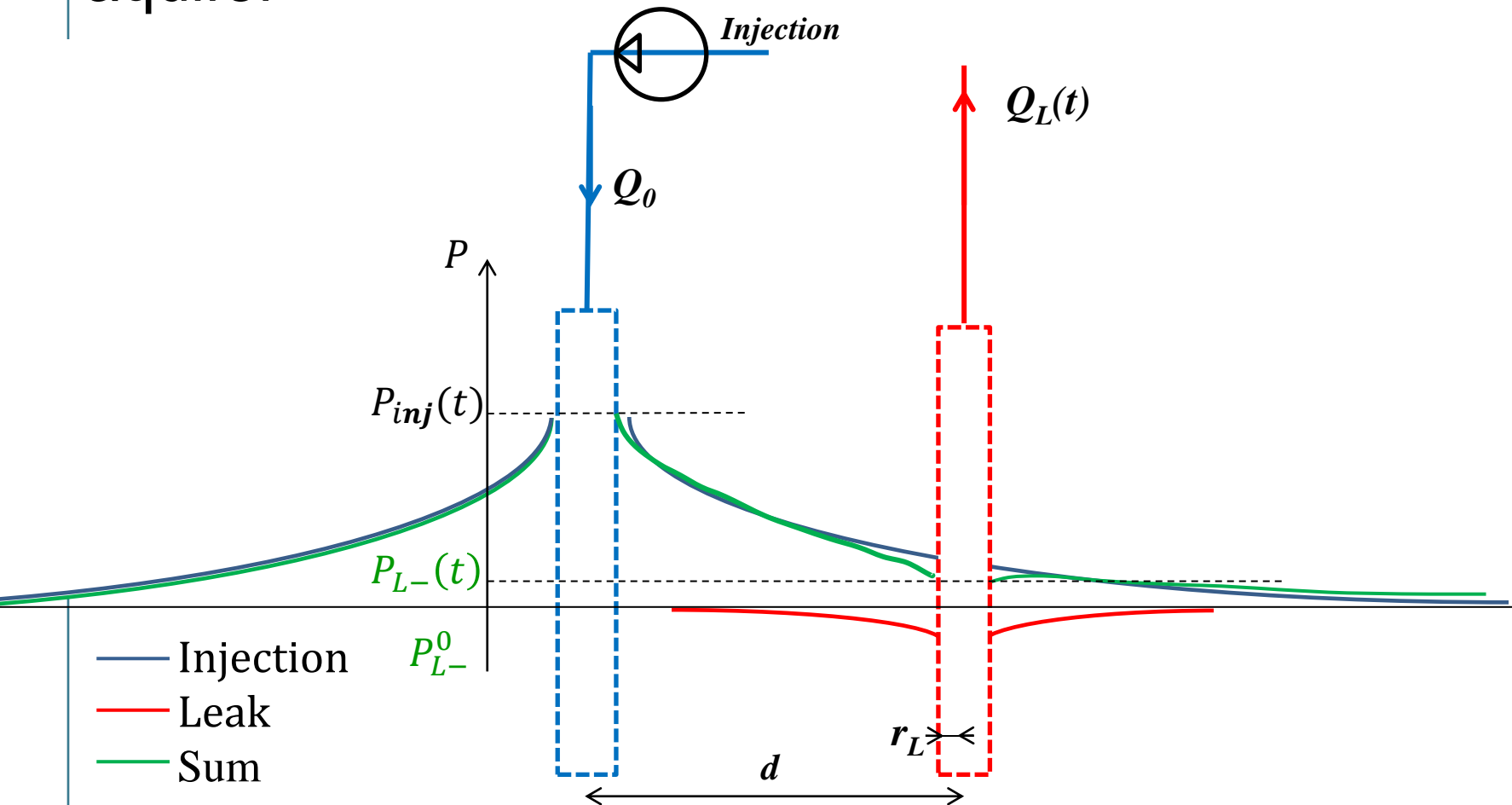
## > Thermal equilibrium (Oldenburg & Rinaldi 2011)



$$P_{L-}^{static} - P_C^{static} = \Delta P_{cp}^0 + \Delta P_{cp}^1(z_I)$$

$$P_C^{static} - P_{L+}^{static} = \Delta P_{wb}^0 + \Delta P_{wb}^1(z_I)$$

# Pressure under the leak in the storage aquifer



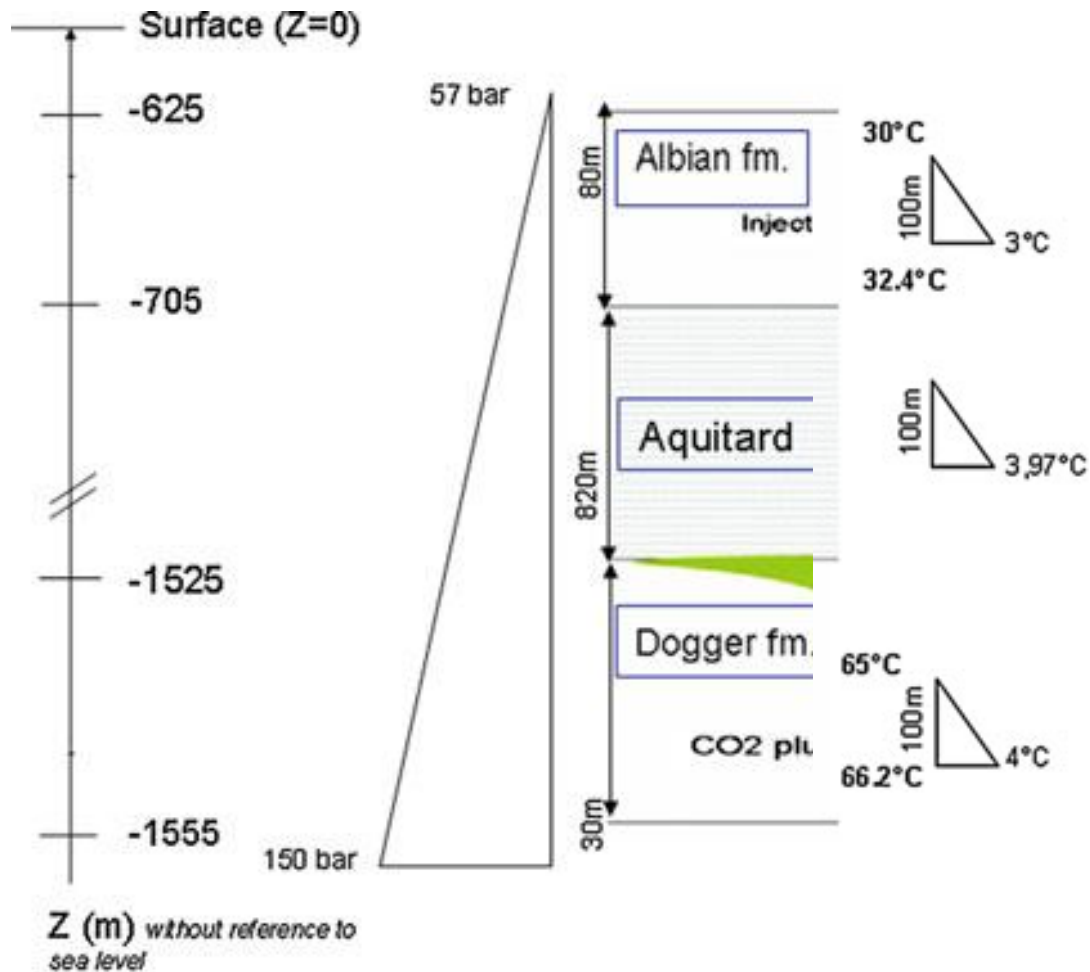
$$P_{L-}(t) - P_{L-}^0 = \frac{\mu_-}{4\pi k_- h_-} \left[ Q_0 E_1 \left( \frac{d^2 S_-}{4T_- t} \right) - \int_0^t \frac{dQ_L}{dt'} E_1 \left( \frac{r_L^2 S_-}{4T_- (t - t')} \right) dt' \right]$$



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# Application to the « PICOREF » sector, Paris basin

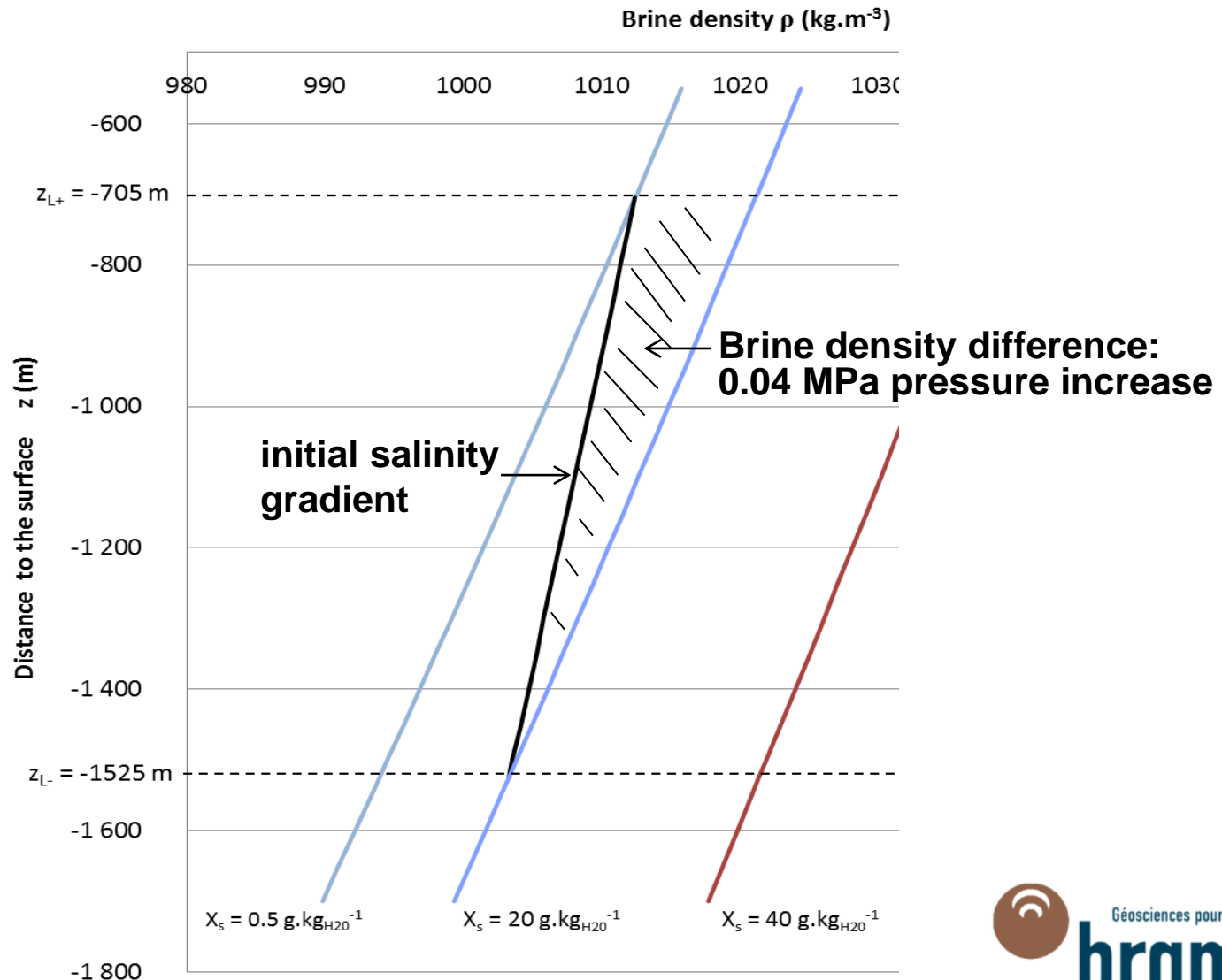


Hydrostatic pressure

hermal gradient

$P, T, X_S$  correspond to the Paris basin context as presented in Humez et al. (2011).

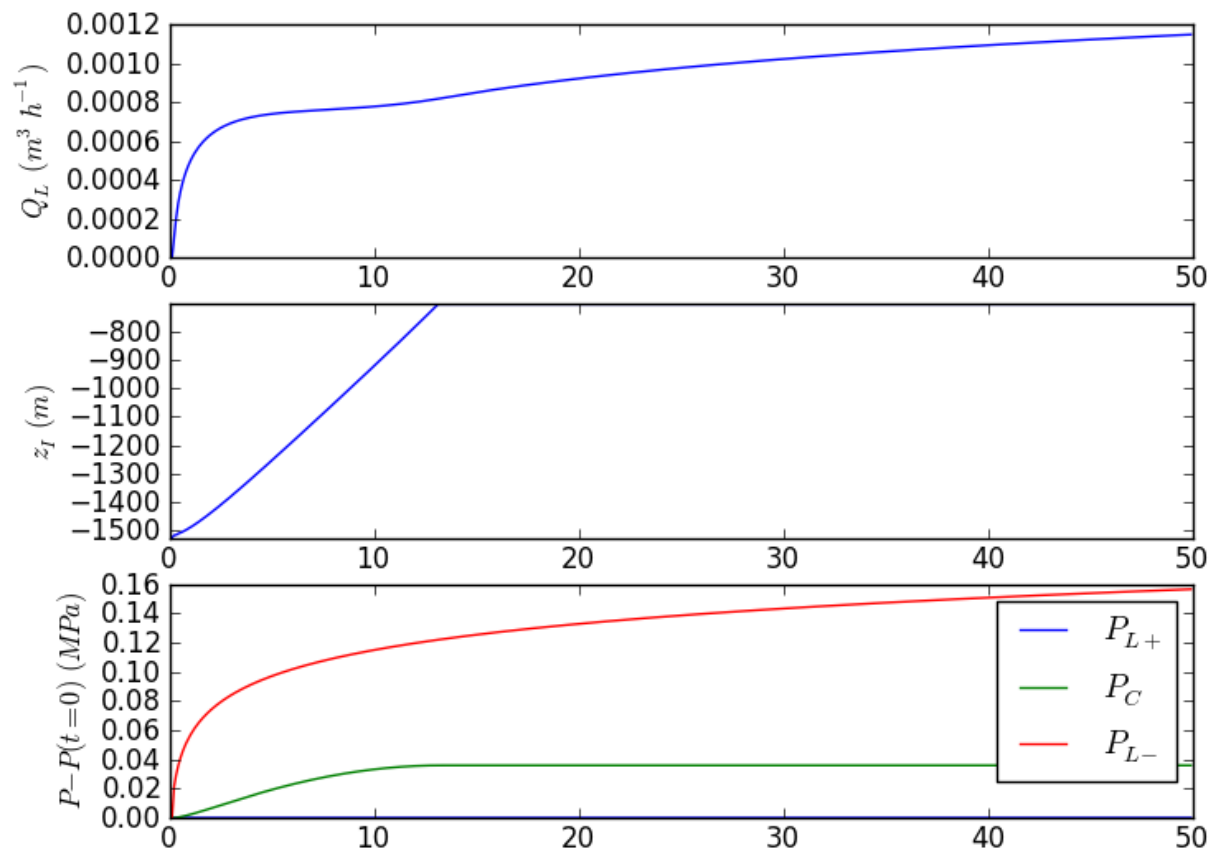
# Brine density profile



# Example of brine leakage



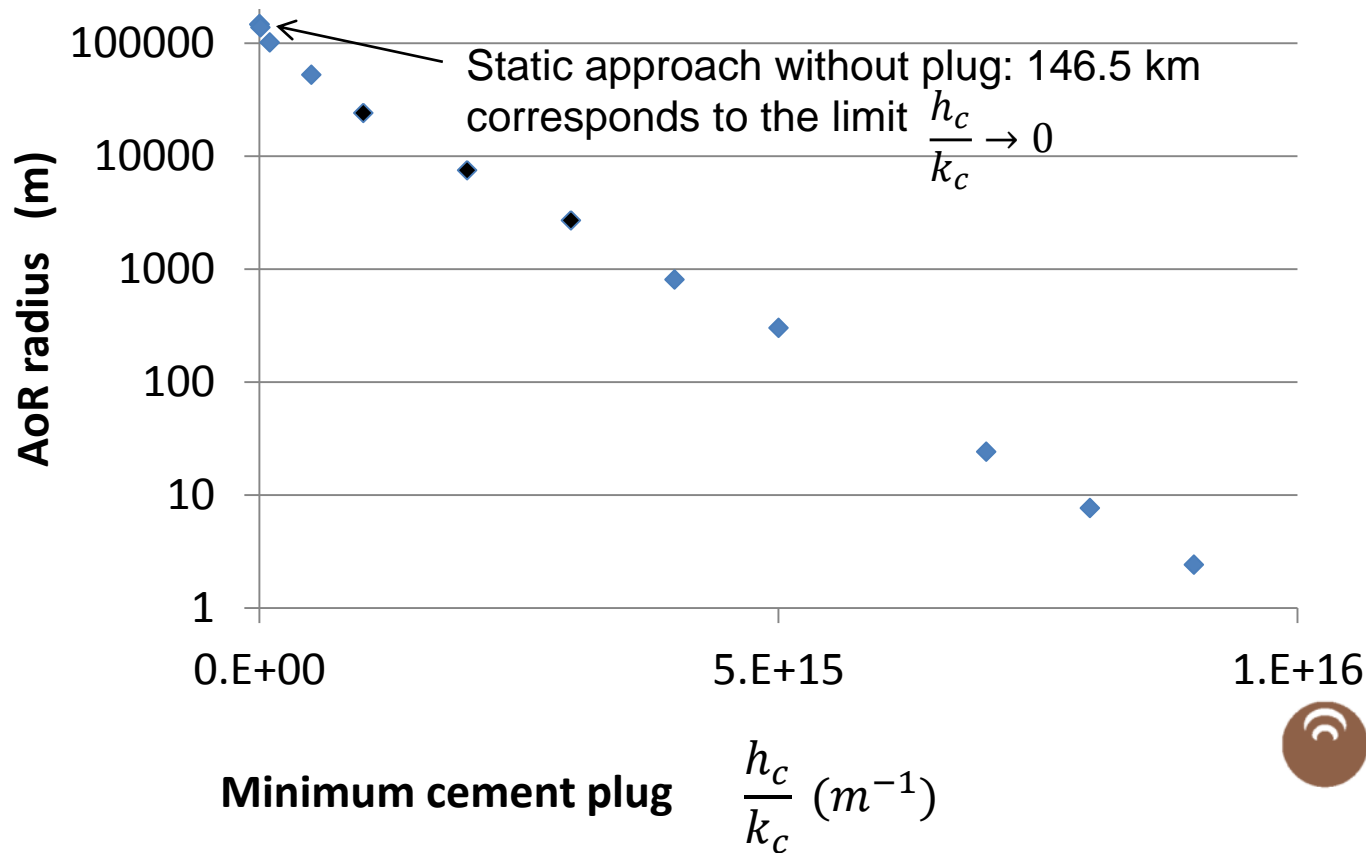
- CO<sub>2</sub> injection scenario: 1 Mt/y for 50 years
- D=6.7 km from the injection to the abandoned well
- Cement plug: 10 m high, weak permability of  $10^{-13} \text{ m}^2$



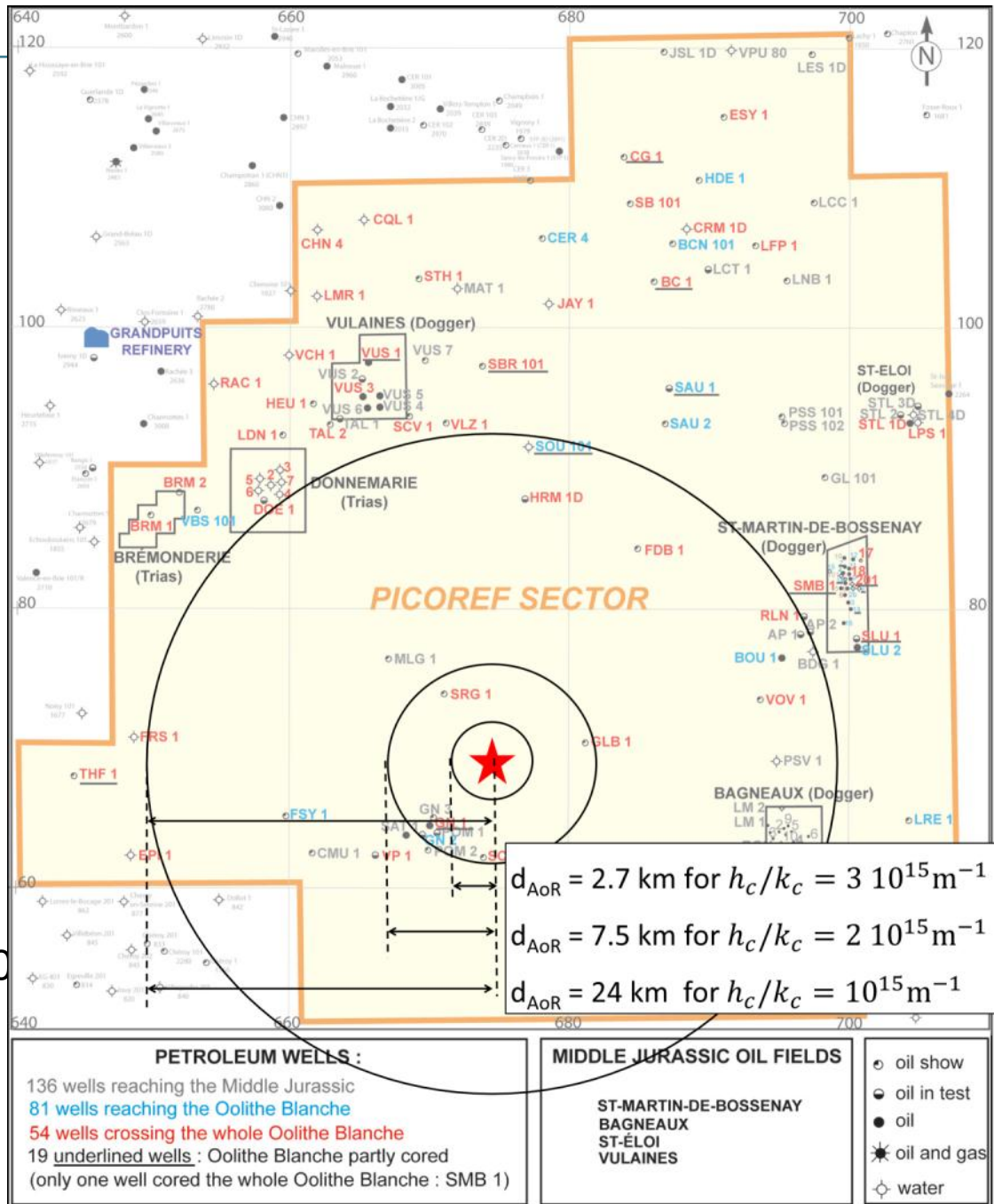
# Area to review for a minimum cement plug height on permeability ratio



## > CO<sub>2</sub> injection scenario: 1 Mt/y for 50 years



# Prioritization of the wells to review



Adapted from Delmas et al., 2010



## > Conclusions

- The model describes the leakage of brine through the leak. Compared to the state of the art (Nordbotten, Celia and co-authors, 2004-2009), it adds the possibility of accounting for density change within the leak due to the incoming of dense brine
- It shares the advantages (immediate computation) and drawbacks (homogeneous layers) of semi-analytical models
- Compared to a static approach (Nicot et al., 2009), this dynamic model enables less conservative estimation of the “Area of Review”, by including effects of cement plugs, of brine density differences and of leakage-induced pressure effects

## > Next steps

- Inclusion of the CO<sub>2</sub> leakage
- Monte-Carlo analyses

> **Thanks!**

> **Acknowledgements**

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