SIMULATION OF MULTIPHASE WATER-CARBON DIOXIDE MIXTURE FLOWS IN POROUS MEDIA cc Andrey Afanasyev

Abstract Two-phase models are widely used for simulation of CO₂ storage in saline aquifers. These models support gaseous phase mainly saturated with CO₂ and liquid phase mainly saturated with H_2O (e.g. TOUGH2). For aquifers where CO_2 injection may result in a plume of supercritical CO_2 compositional simulation approach must be applied.

The goal of the present study lies in development of a new mathematical approach for compositional simulation of CO₂ sequestration processes. The approach is applicable both for single-phase and twophase states of liquid-gas type as existing simulators and also for two-phase states of liquid-liquid type and three-phase states at high pressures. The liquid-liquid states are formed by two liquids. The first liquid is mainly saturated with H₂O while the second is mainly saturated with CO₂. These thermodynamic equilibriums with liquefied CO₂ phase were detected experimentally (Takenouchi et. Al. 1984). The three phases in the three-phase states are liquid H_2O and CO_2 in liquid and gaseous states. The proposed approach was implemented in MUFITS simulator that was used for 1D, 2D and 3D simulations of CO₂ injection in water saturated reservoirs subjected to CO₂ liquefaction effect.

Balance equations	
$\left \frac{\partial}{\partial t} \left(m \sum_{i=1}^{3} \frac{M_{(j)} x_{i(j)}}{v_i} s_i \right) + \operatorname{div} \left(\sum_{i=1}^{3} \frac{M_{(j)} x_{i(j)}}{v_i} \mathbf{w}_i \right) = 0 \qquad \begin{array}{c} -m \\ \mathbf{e} \\ e$	hass quatior ompon
$\frac{\partial}{\partial t} \left(m \sum_{i=1}^{3} \frac{e_i}{v_i} s_i + (1-m) \frac{e_s}{v_s} \right) + \operatorname{div} \left(\sum_{i=1}^{3} \frac{h_i}{v_i} \mathbf{w}_i - \lambda \frac{\partial T}{\partial \mathbf{r}} \right) = A_g$	=1: CO - en equa
$\mathbf{w}_{i} = -K \frac{f_{i}}{\mu_{i}} \left(\frac{\partial P}{\partial \mathbf{r}} - \frac{M_{i}}{v_{i}} \mathbf{g} \right) - \text{multiphase Darcy correlation,} \\ i = 1 \dots 3 - \text{phase number}$	done gravi

Mixture properties design

A Peng-Robinson type equation of state was fitted to more than 150 CO₂-H₂O mixture properties measurements. The equation has an advantage for polar substances (e.g. H,O) properties prediction. Both measurements of single-phase state and two-phase states of liquid-liquid and liquid-gas type were used for the equation coefficients determination. The figure shows parameters of the measurements of pure water or CO₂-H₂O mixture in single- (red or green) and twophase (blue or violet) states. The sizes of 600the symbols correspond to the equation of state error under the measured conditions. The bigger the symbol is the larger the equation of state error. The maximum error does not exceed 20%.

- e T -	equation of state. P – – temperature, v – vo
C	D ₂ molar fraction
/ 1200 -	
т(к)	-
	•
900 -	• •
	•

Multiphase equilibrium

The tuned cubic equation of state was used for CO₂-H₂O binary mixture thermodynamic potential calculation. Entropy 🏲 $\sigma(P,h,x)$ depending on pressure P, enthalpy h and composition x is determined. This approach results in simplification of \square three-phase states calculation. The following conditional extremum problem is solved to determine the multiphase equilibrium. The entropy maximum is evaluated over 1-phase, 2-phase and 3-phase states. Pressure *P* and summed by phases enthalpy h_t and composition x_t are known. The problem solution defines parameters of phases h_i , x_i and V_i .

$\sigma_t = \sum_{i=1}^{5}$	$\sigma_i V_i \to \max,$	$\sigma_i = \sigma(P, h_i, x_i)$) V-phase molar fra
3	3	3	



liquid 1

liquid 2

 $\sum V_i = 1, \quad \sum h_i V_i = h_t, \quad \sum x_i V_i = x_t, \quad 0 \le V_i \le 1$

Institute of mechanics, Moscow State University, e-mail: afanasyev@imec.msu.ru

conservation each for ent, *j*=1,2, $j=2: H_2O$

ergy conservation tion, Ag – work by the force of

MUFITS simulator

The proposed approach was implemented in MUFITS (MUltiphase FIltration Transport Simulator) code for three-phase compositional simulations of non-isothermal flows in porous media. The code is capable of real heterogeneous reservoir geology and support parallel computations and commonly used input data formats. Mixture thermodynamic properties can be specified within the code. The simulator was used for 1D, 2D and 3D simulations of carbon dioxide injection in water saturated reservoirs.

CO, injection (1D example) The sample 1D simulation demonstrates a simple scenario when gaseous CO, injection through the left boundary of the layer results in underground CO₂ liquefaction and evolution of the three-phase flow zone with liquid CO₂ phase. The two-phase and three-phase flow zones are separated by a clearly visible phase discontinuities.





Phase diagram

The CO₂-H₂O phase diagram in pressure (P), enthalpy (h)and CO_2 molar fraction (x)space. R_1 (R_2) is H_2O (CO_2) critical point. Outside the surface bounded by the green lines the mixture is singlephase state while inside the region bounded by the surface the mixture is in two-phase state. The two-phase states at high pressure are of liquidliquid type. The red lines bound the three-phase state parameters $(Q_1Q_2Q_3R_3R_4)$ region).



т(к)	gaseous H ₂ O	Parameters of t phase state at P=1		
620 - 540 -	2-phase pure H_2O H_2O crit. point liquid H_2O	Phase	Density (kg/m ³)	CC fr
460 -		Liquid H ₂ O	995	(
380 -	3-phase IH ₂ O+ICO ₂ +gas crit. point	Liquid CO ₂	1026	
300 -	CO ₂ CO ₂ crit. point liquid CO ₂ 5 10 15 20 P(MPa)	Gas	246	

The negatively buoyant liquid CO₂ can result in non-classical hydrodynamic effects in the aquifer with CO₂ sinking and consequently in non-classical structural trapping scenarios. The possibility of the liquefaction strongly depends on the reservoir pressure, temperature and mixture composition.

The CO₂ plume evolution

The gaseous CO_2 buoyancy is the principal Liq. H2O satur. effect used for conventional CO, structural trapping. The gas comes to the surface filling the upper regions of the folded reservoir. The sample simulation conducted for quite high reservoir temperature $(T=360 \ K)$ demonstrates this effect. The reservoir is initially saturated Pressure with water. Hydrostatic conditions are hold on the left and right boundaries of the reservoir. The negatively buoyant liquid CO₂ sinks in the aquifer filling the Liq. H2O satur. lowest regions of the reservoir. The second sample simulation on the right conducted *T=330K* reservoir temperature demonstrates this effect. Liquid H₂O, liquid CO₂ and gas phase are present in the reservoir. As in the conventional scenario gas fills the upper layers of the reservoir. However, the CO₂ liquefaction process results in non-classical CO, distribution with liquid CO₂ sinking.



CO, injection in heterogeneous reservoir The 10th SPE comparative solution project reservoir was used to test MUFITS robustness in simulation of flows in highly heterogeneous reservoir. The simulation was conducted in the 50th layer of the reservoir. The channels in the layer are clearly visible through the porosity distribution. The layer was initially saturated with water. Gaseous CO, is injected through the left boundary while at the right boundary pressure is fixed. Thus CO₂-H₂O mixture flows from the left to the right through highly permeable zones channels in the porous media. Subject to phase transitions the saturations distribution in the layer is quite complicated. The 10th SPE project reservoir, layer 50 SACS projects 3D simulations MUFITS code was applied to simulations of CO₂ plume **LOMPa** appreciated.

A new approach for three-phase compositional hydrodynamic simulations is proposed. The approach is **Conclusions** applicable for single-phase, two-phase and three-phase CO_2 -H₂O mixture flows with liquefied CO_2 phase. The proposed model results in a more accurate prediction of supercritical CO₂ plume evolution because it accounts for possible threephase thermodynamic equilibriums. The approach was implemented in MUFITS simulator applied to 1D, 2D and 3D sample simulations of CO₂ injection subjected to CO₂ liquefaction effect. The simulator can be applied to analysis of CO₂ injection in real storage sites taking into account the reservoir heterogeneity and complex multiphase character of the flow in gravity field.



 D_{2} mass raction

0.039

0.773

0.989

EGU2012-6194

evolution at the Sleipner storage site. The CO₂ plume shape is in a good agreement with the existing hydrodynamic simulations results (Varunendra Singh et al 2010). However some details of the plume behavior determined by the seismic surveys still can't be predicted. Detailed simulation results can be demonstrated on the laptop. Discussions of the proposed model improvement for better calibration of the reservoir uncertainties are

Acknowledgments: Statoil and the Sleipner License are acknowledged for provision of the Sleipner 2010 Reference dataset. Any conclusions in this paper concerning the Sleipner field are the authors' own opinions and do not necessarily represent the views of Statoil