

The effects of impure CO₂ on reservoir sandstones: results from mineralogical and geomechanical experiments

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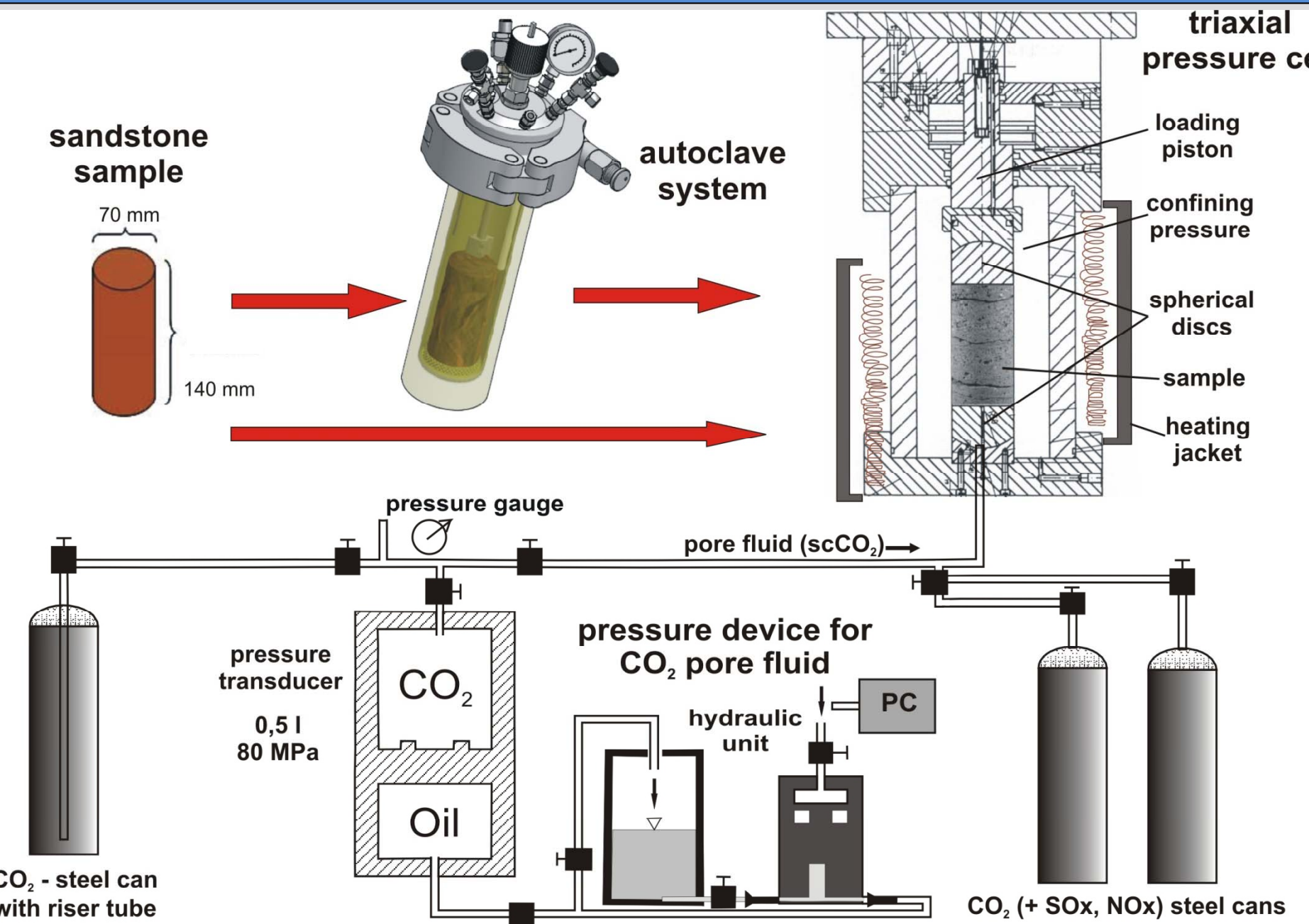


Fig. 1: The experimental flow: sandstone samples were controlled altered in an autoclave system (with brine + scCO₂ + NO_x + SO_x under 100°C and 100 bar, 2-4 weeks) and then loaded in a heatable triaxial pressure cell (under 50°C to 80°C and up to 30 MPa confining pressure, 25 MPa pore fluid pressure and a maximum of 107 MPa axial pressure) with CO₂ + up to 500 ppm NO_x and up to 1000 ppm SO_x as pore fluid. Also untreated samples were tested in the triaxial cell.

Project and Methodology:

Within the German project COORAL* the behaviour of potential reservoir rocks during the injection and geological storage of CO₂ with inherent impurities such as SO_x and NO_x is studied in laboratory experiments. A combination of geochemical and geomechanical studies are performed as autoclave experiments and subsequent tests in a triaxial pressure cell with dry and brine saturated sandstone samples. For a comparative study controlled altered rock samples (with supercritical (sc)CO₂ + SO_x + NO_x in an autoclave system) were loaded in a triaxial pressure cell under in-situ PT-conditions (Fig. 1), to study changes of the mineralogical, geochemical and geomechanical rock properties. Working materials are sandstones of possible reservoir formations of the North German Basin (Fig. 2).

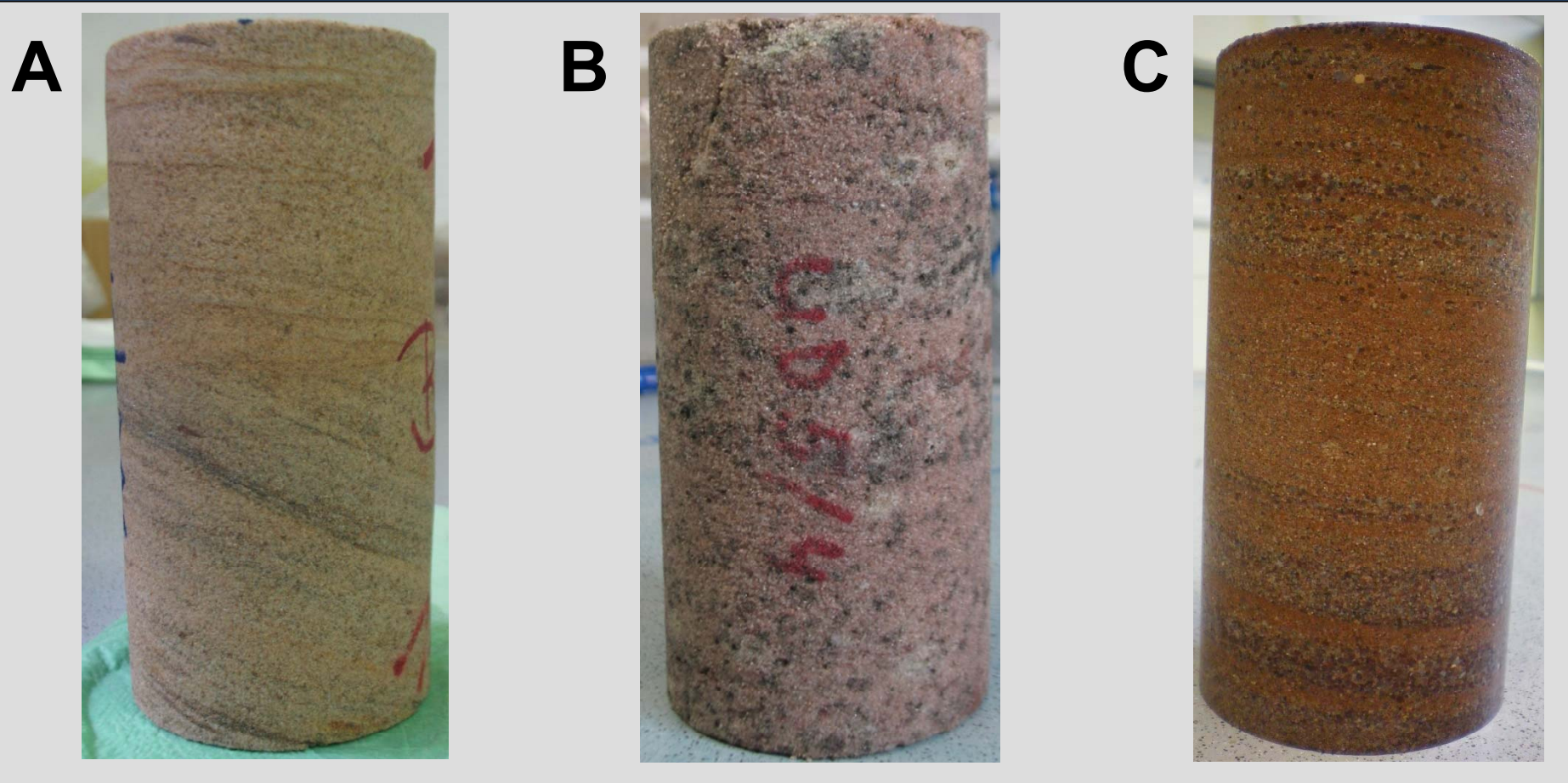


Fig. 2: Three types of sandstones from the North German Basin (samples with Ø=70 mm, L=140 mm):
A: Silicate sandstone "Mid Bunter Sandstone" (lower Triassic; porosity: ~ 22 %)
B: Carbonate sandstone "Mid Bunter Sandstone" (lower Triassic; porosity: ~ 16 %)
C: Silicate and carbon. "Rotliegend sandstone" (lower Permian; porosity: ~ 8 %)

Results:

- Silicate Bunter sandstone samples show decreased rock strength under enhanced pore fluid pressure (from 60% to 80% σ_3 ; Fig. 3 A).
- A clear dependency of chemical fluid composition and confining pressure (lithostatic) on the maximum differential stress (effective stress) especially on carbonate sandstones (Fig. 3 B) is obvious according to the experimental results.

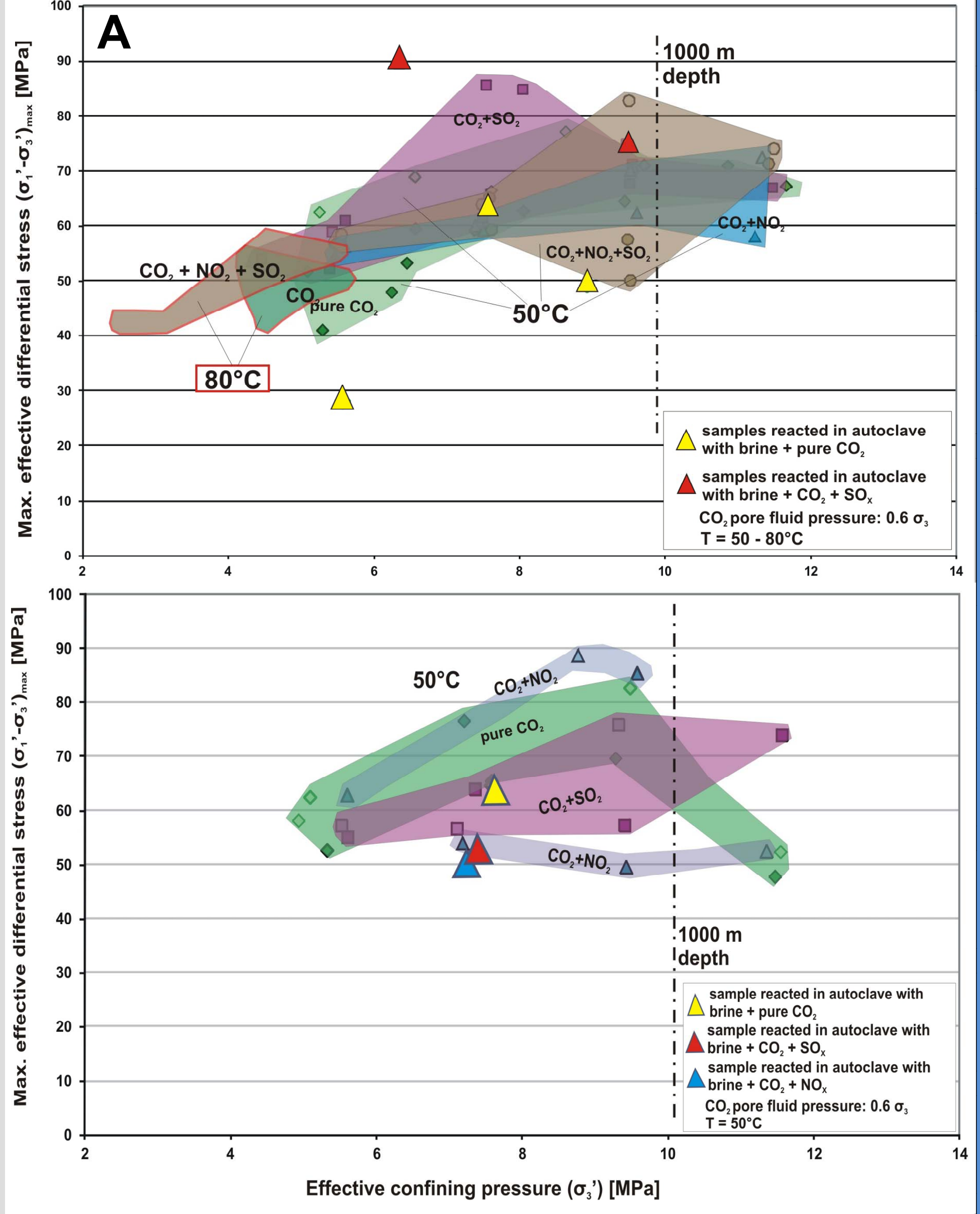


Fig. 3: Differential stress diagrams showing the influence of rock saturation, confining pressure (σ_3), pore fluid composition (CO₂ with SO_x and NO_x) and pore fluid pressure (p) on the maximum effective stress $\sigma_1' - \sigma_3'$ ($\sigma_1' = \sigma_1 - p$; effective confining pressure $\sigma_3' = \sigma_3 - p$) for silicatic (A) and carbonatic bound (B) Bunter sandstones. The differently coloured polygons connect sample points of equally pore fluid chemistry. A total confining pressure of 25 MPa corresponding 1000 m reservoir depth.

- Contents of dissolved metals in the reaction fluid during the autoclave alteration experiment depends on the impurities (SO_x and NO_x) in the CO₂ gas stream (Fig. 5 A).

- Dissolution rates (Fig. 5 B) of bulk rock (sandstones) as well of single minerals varies with the carbonate fraction. Rates are calculated according to the formula:

$$r = \frac{dm_i}{dt} \cdot \frac{V}{A_s \cdot M_s}$$

r : dissolution rate (mol m⁻² s⁻¹)
 A_s : inner surface (BET) (m²/g)
 m_i : molar concentration
 t : time (s)
 V : fluid volume (l)
 M_s : mass (g)

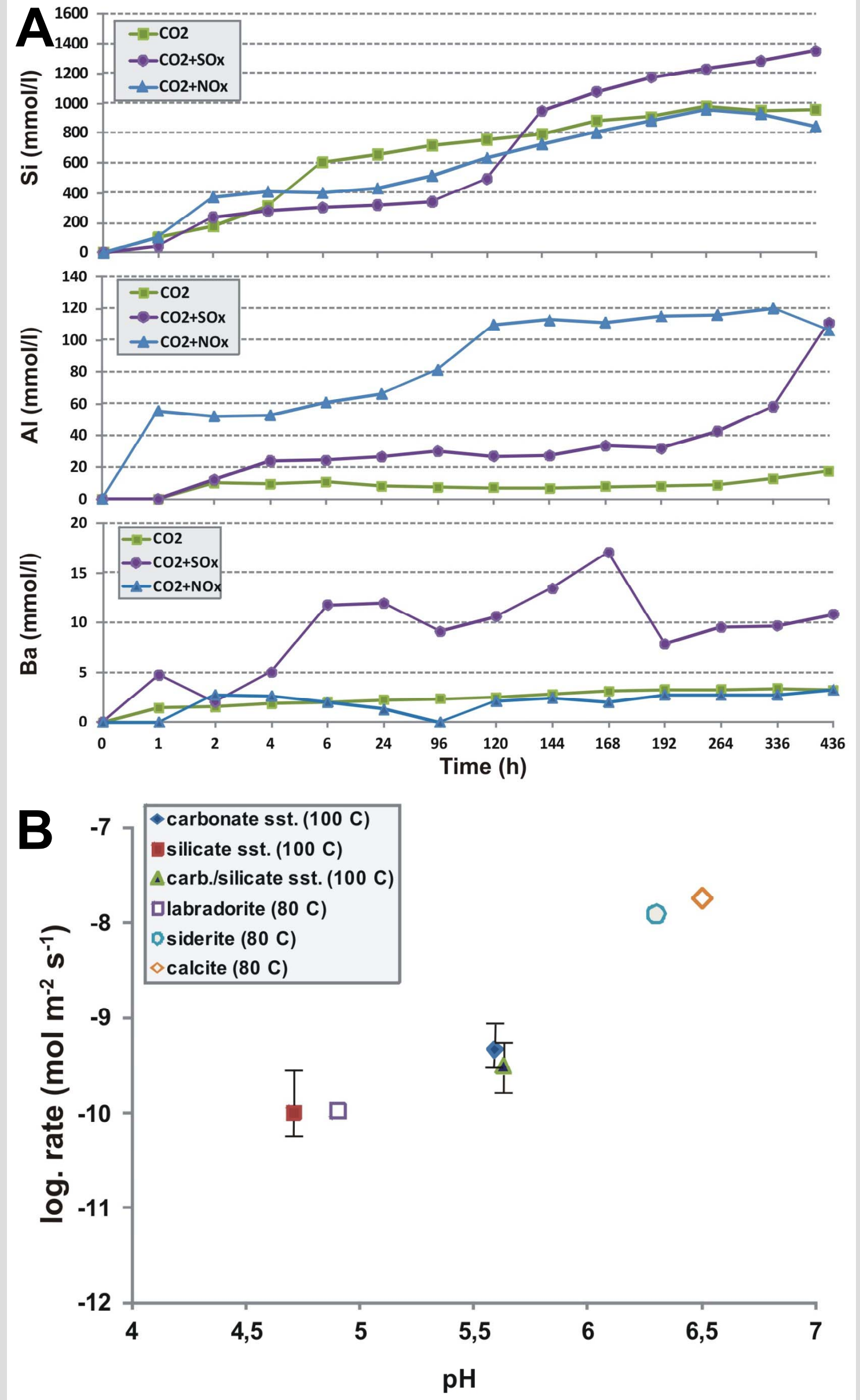


Fig. 5: Development of chemical fluid composition during alteration experiments on silicate sandstones (A); dissolution rates of bulk sandstone types and single minerals (B)

- After exposure to brine and scCO₂ + SO_x or NO_x in the autoclave, samples show alterations i.e. dissolution effects of the carbonatic cements and of single minerals (Fig. 6 A, B) and also secondary mineral precipitations (C, D).

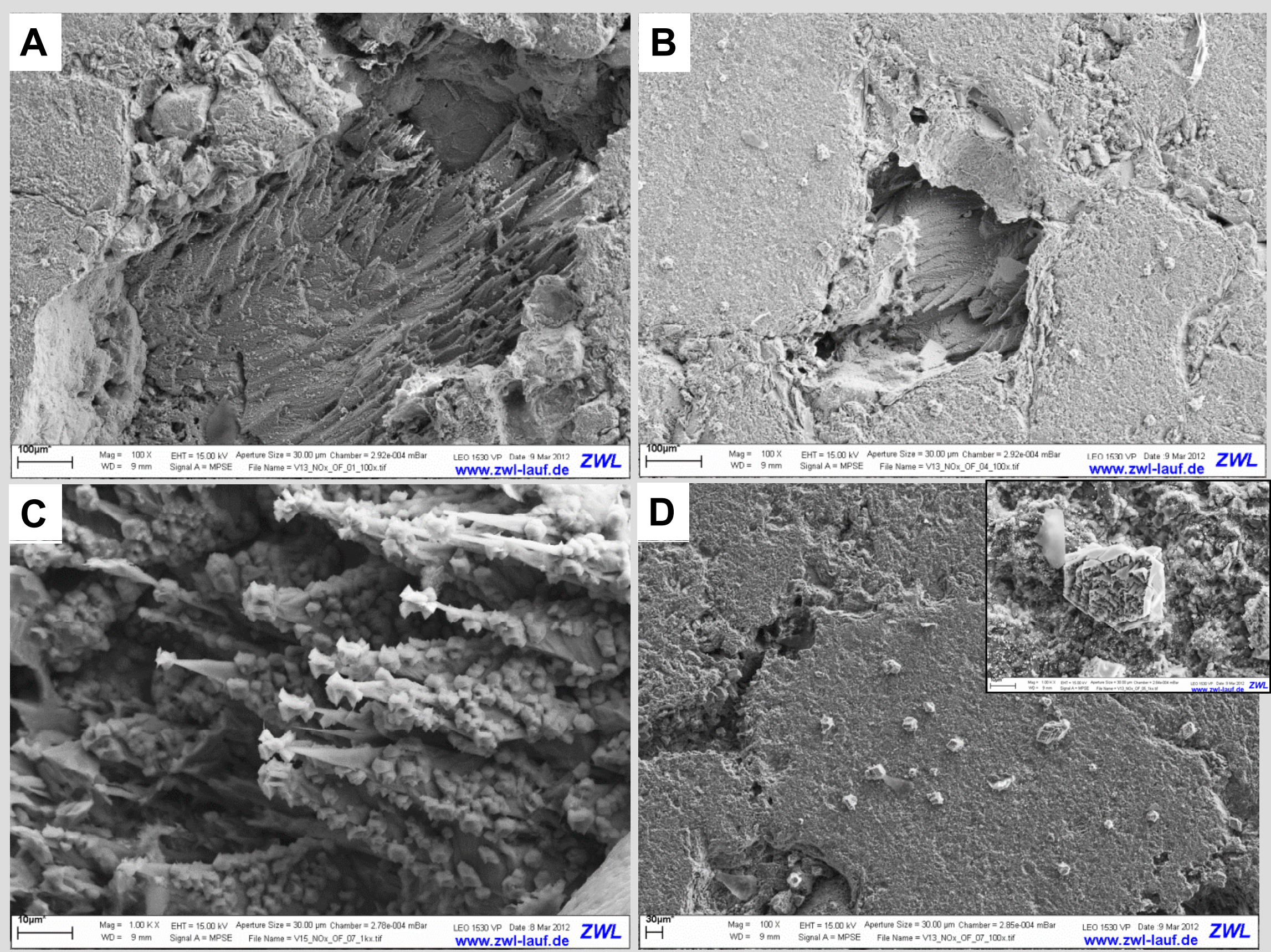


Fig. 6: SEM-images of silicate and carbonate bound Rotliegend sandstone samples after the treatment with brine and scCO₂ + 500 ppm NO_x in the autoclave. Images A and B shows dissolution effects on the carbonate matrix and C and D demonstrate secondary calcite precipitation axe-orientated on dissolved calcite tops (C) and on a carbonate surface (D).

- Decrease of rock deformability (strain softening) due to the alteration with pure scCO₂ (Fig. 4).
- Increase of rock deformability (strain hardening) during the alteration under the influence of CO₂ + 1000 ppm SO_x (Fig. 4).

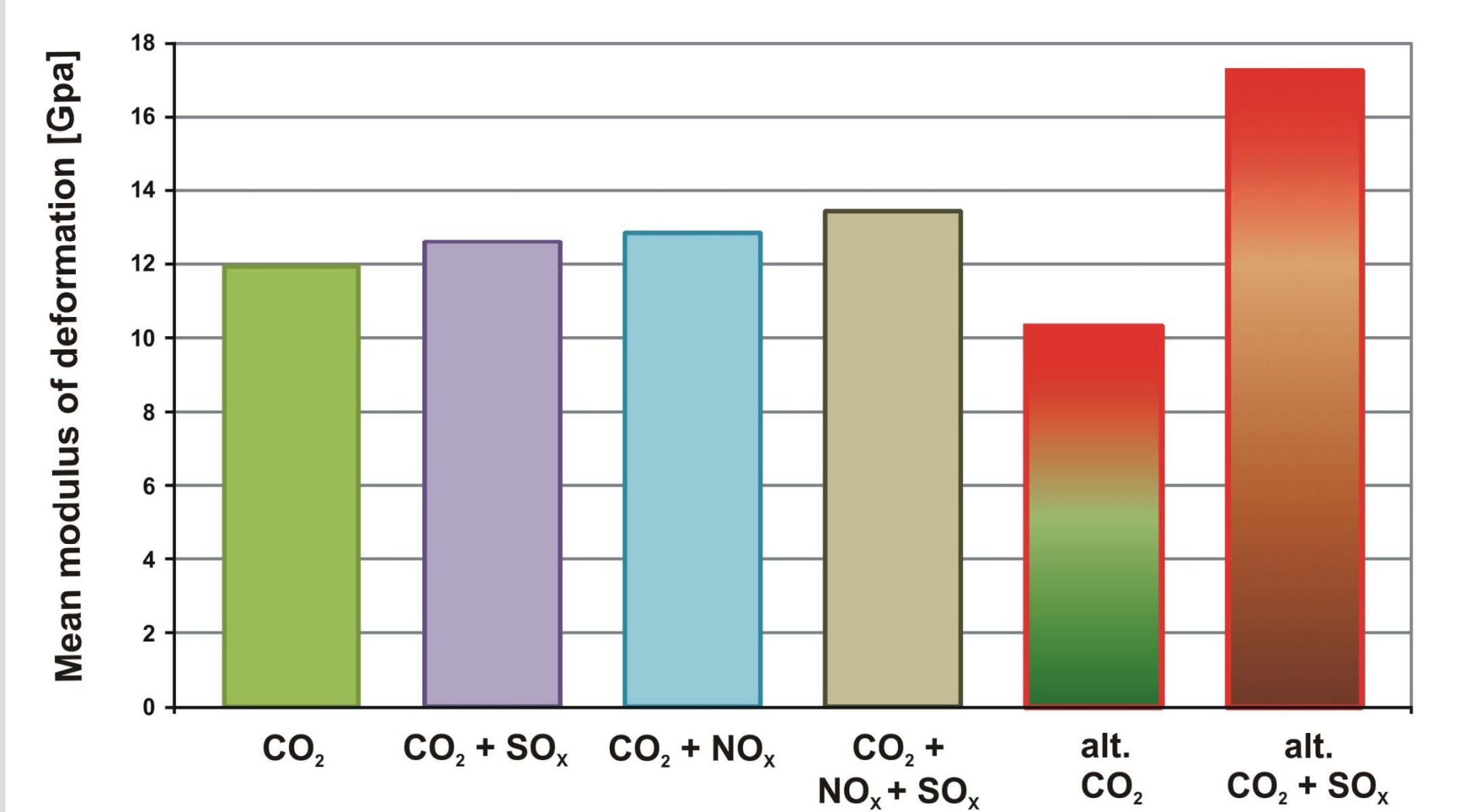


Fig. 4: Variation of elastic deformation properties (modulus of deformation) of silicate sandstone samples due to CO₂-alteration and the pore fluid chemical composition

Conclusions:

- The strength behaviour of different types of sandstones varies with the degree of sample saturation, the pore fluid pressure, pore fluid chemistry and temperature.
- Various types of fluids cause different maximum differential stresses (effective stresses) at changing pressure conditions. This may be due to different pore space geometries and permeability.
- Different impurities in the reaction fluids in the autoclave (pure CO₂ + SO_x or NO_x) showing variable but generally increasing element dissolutions from the rocks (Ca, Si, Al, Ba) during the experimental course.
- The experimental determined differences in rock strength and elastic deformability of altered samples demonstrates clear trends of chemically induced mechanical weakening of the studied sandstones.

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