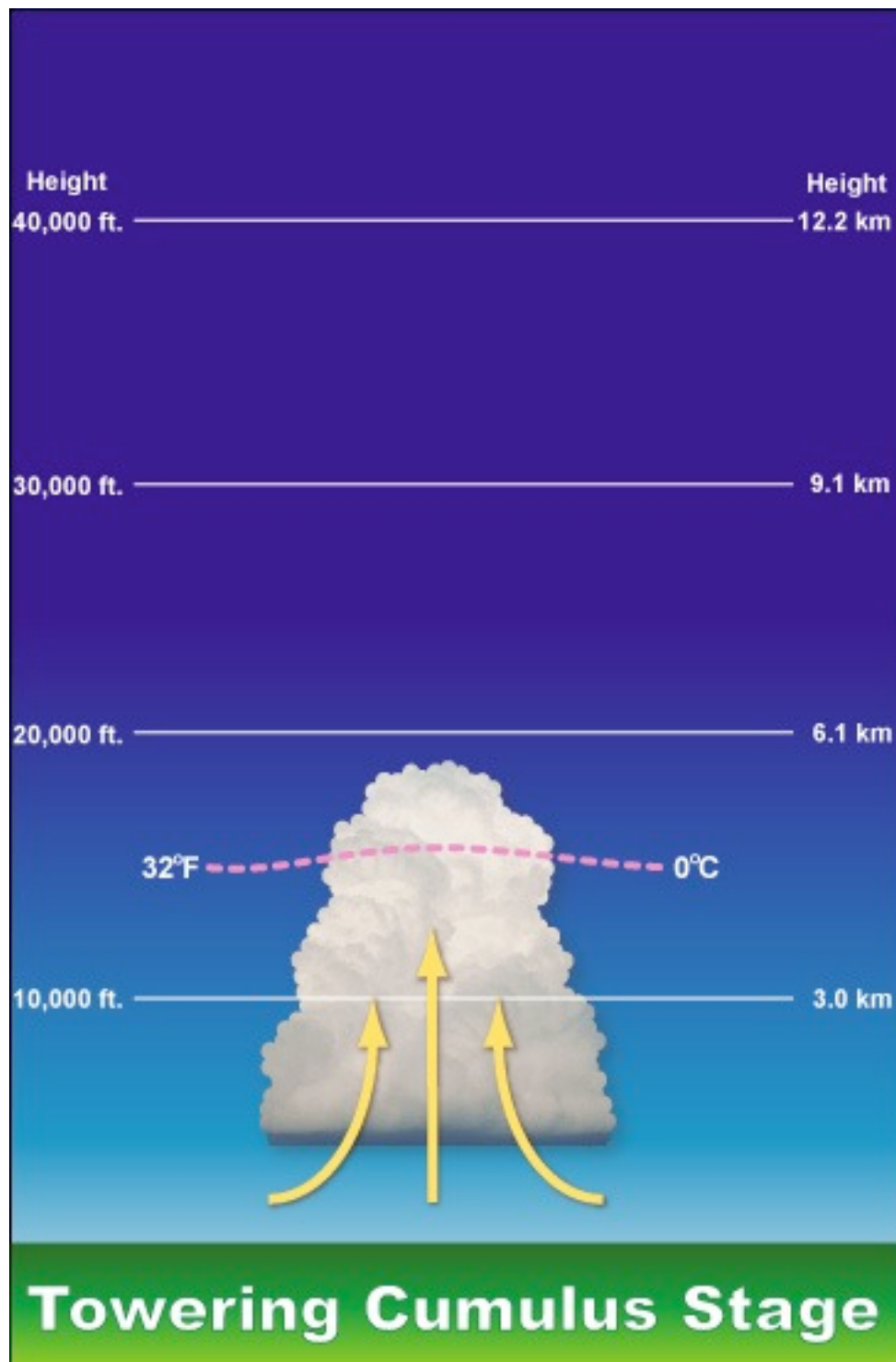


Cumulus air parcels and their vertical momentum budgets

Steven Sherwood, Daniel Hernández-Deckers,
Maxime Colin, Frank Robinson

Conceptual model of cumulus



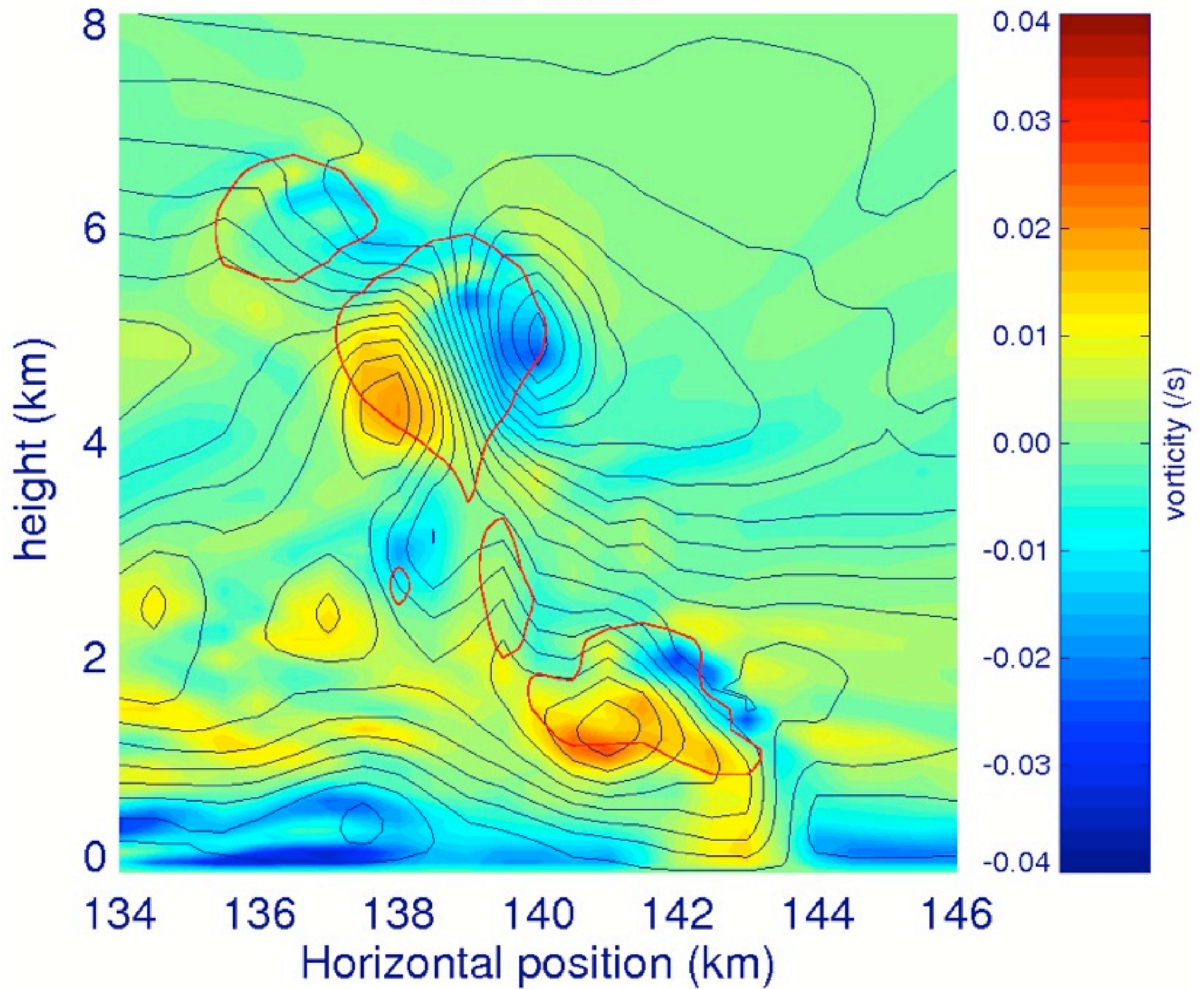
Assumptions

- Cloud properties horizontally uniform
- high shear at cloud edges
- net entrainment $\rightarrow dM/dz > 0$.
- Cumulus = rising cloud (wherever $w \gg 0$, $q_c \gg 0$)
- Parcel = cumulus

problem

- w , q_c are not conserved tracers, not good for tracking a rising parcel, especially w/entrainment.

Rest frame



Lab studies

Vortex rings propagate easily with less than 10% velocity loss after traveling 6 diameters (Dabiri and Gharib 2004)

highly robust (and virtually no drag)

--> “real” parcels!!

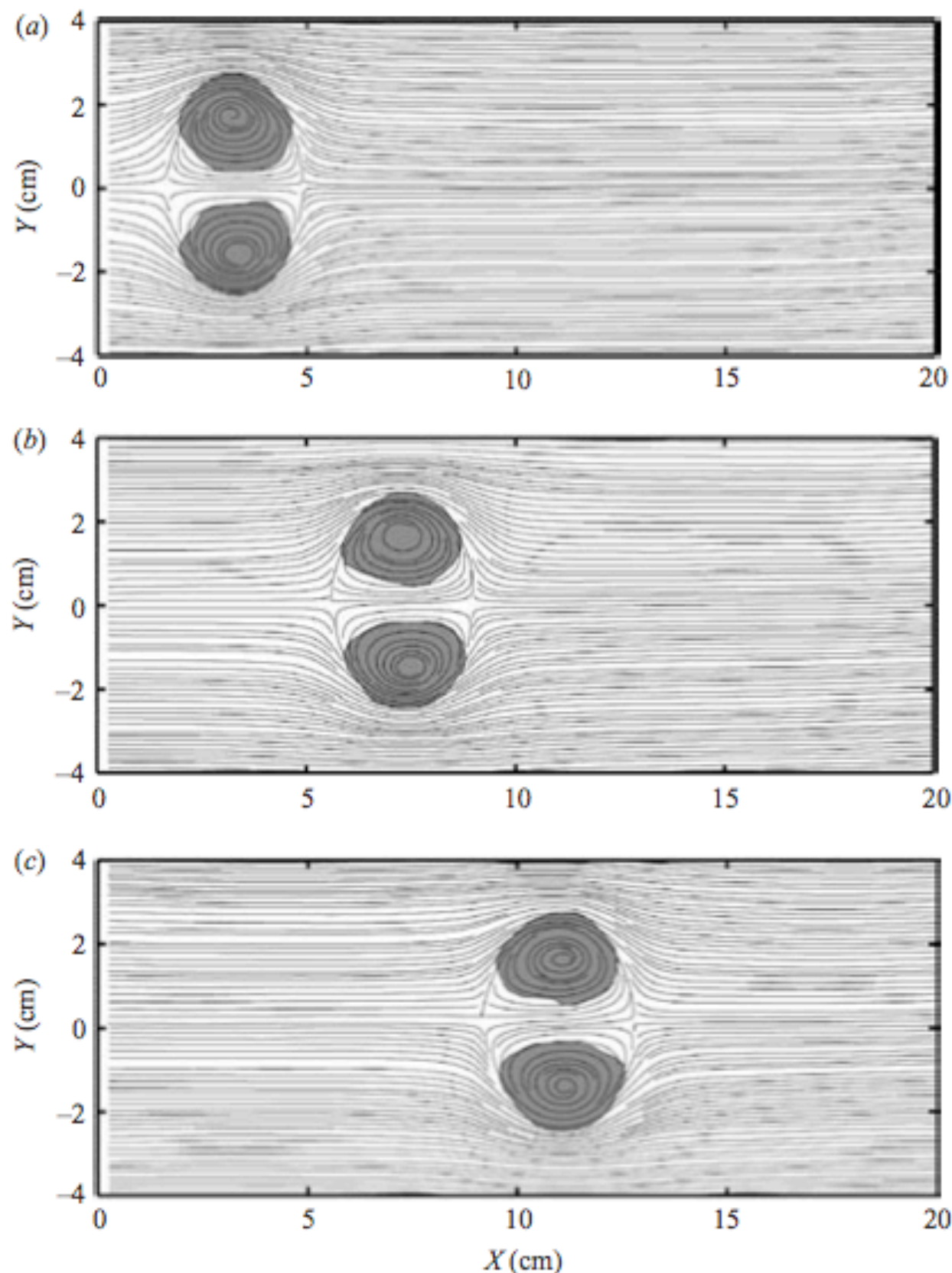
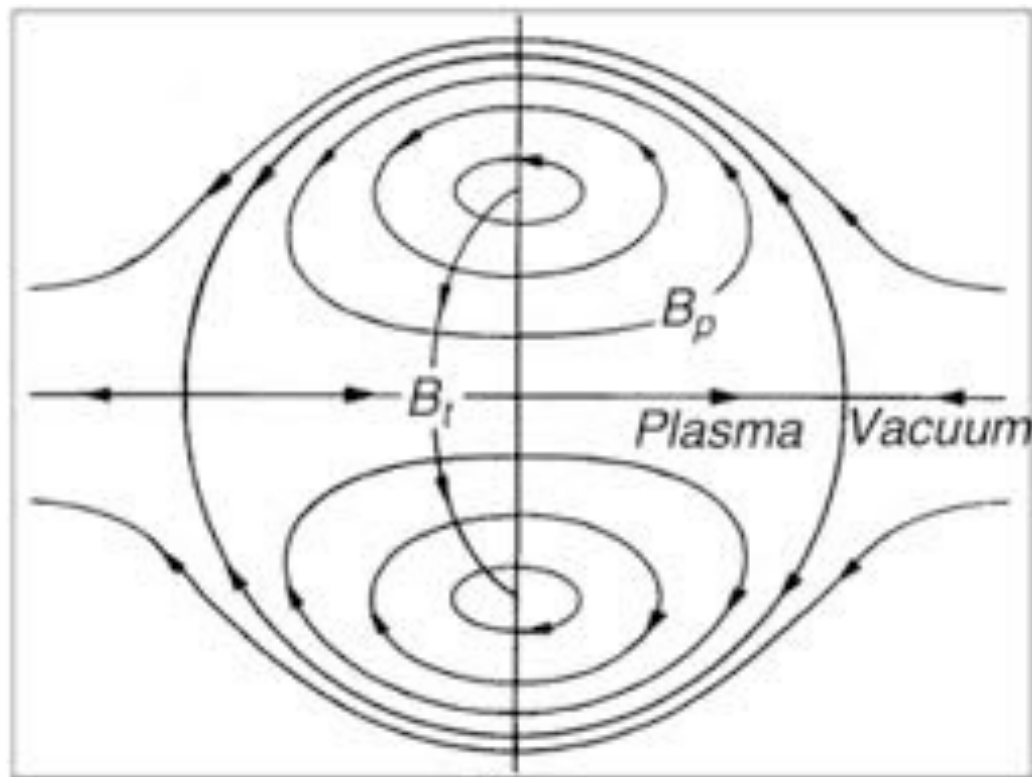


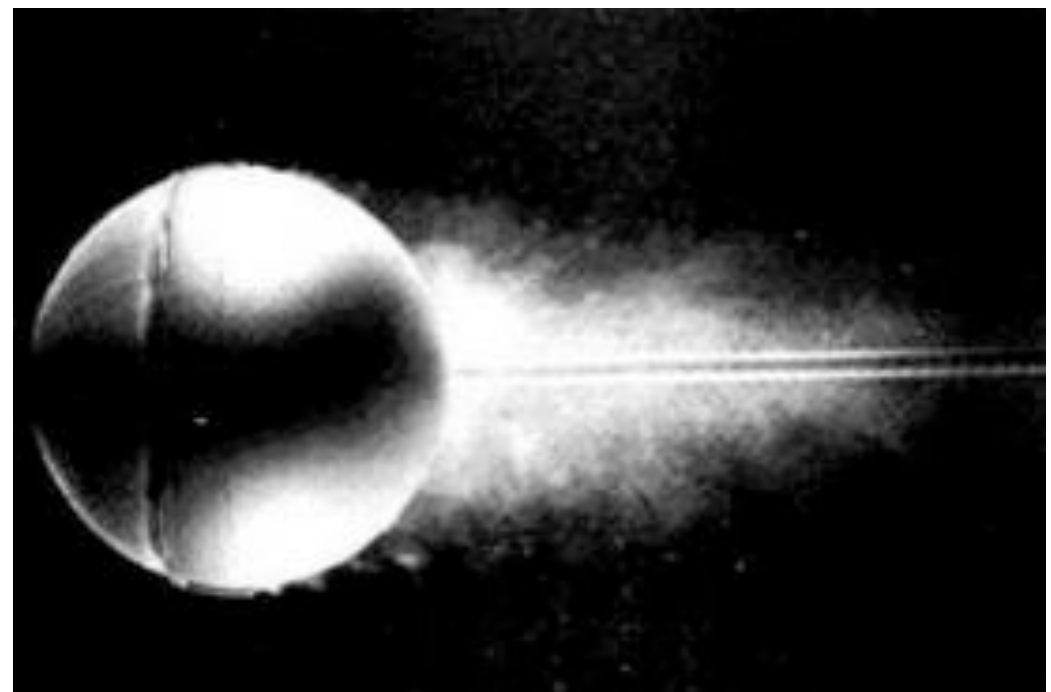
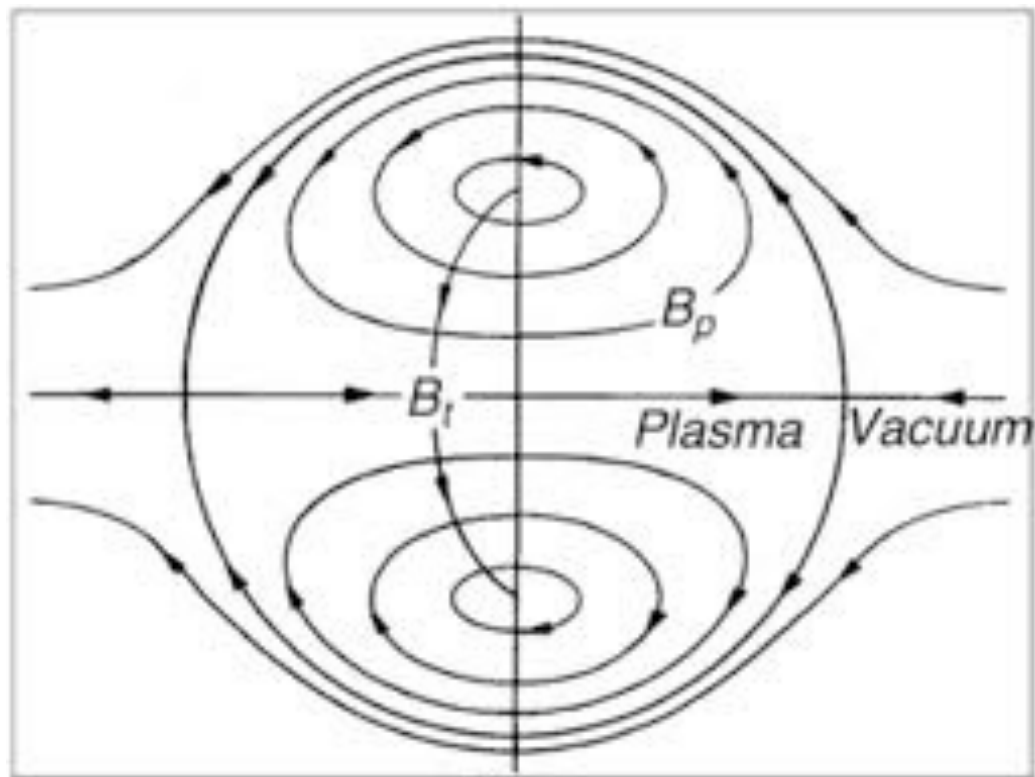
FIGURE 5. Instantaneous streamlines and vorticity patches for protocol *LD2-CF0*.
(a) $T = 1.67$ s; (b) $T = 3.54$ s; (c) $T = 5.34$ s. Minimum vorticity level is 1 s^{-1} .

Hill's spherical vortex



An exact solution to the Navier-Stokes equations.
Shear vanishes to first order on vortex boundary
surface

Hill's spherical vortex



An exact solution to the Navier-Stokes equations.
Shear vanishes to first order on vortex boundary
surface

Problems:

- Outside of vortex not conventionally counted as part of “cloud,” since $w \sim 0$
- Dry air entrained into vortex not counted (for a while) since $q_c = 0$.
- We propose that vortices be considered and tracked as the the fundamental entities. The vortex-parcels will have fractional cloud amount.

- We find radius r such that $\int_r w dV = dz_{\text{therm}}/dt$
- Entrainment distance calculated as:

$$D_{\text{entrain}} = \frac{\int_V \rho \omega dV}{\oint \vec{u}' \cdot \hat{n} H(\vec{u}' \cdot \hat{n}) \rho dS}$$

- Momentum flux M into thermal calculated as:

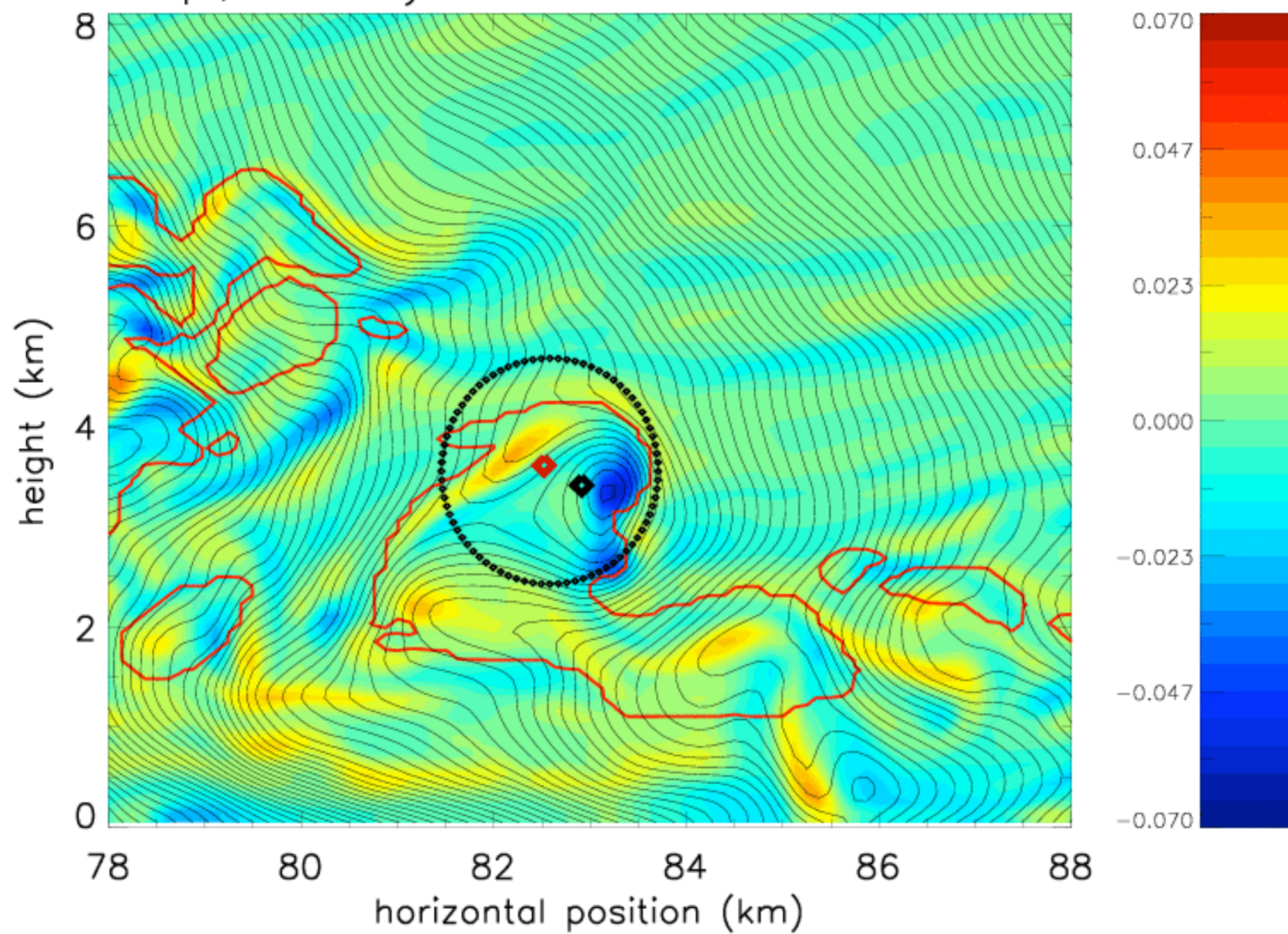
$$M = \frac{\oint \vec{u}' \cdot \hat{n} \rho \omega' dS}{\int_V \rho dV}$$

- Momentum budget of thermal is

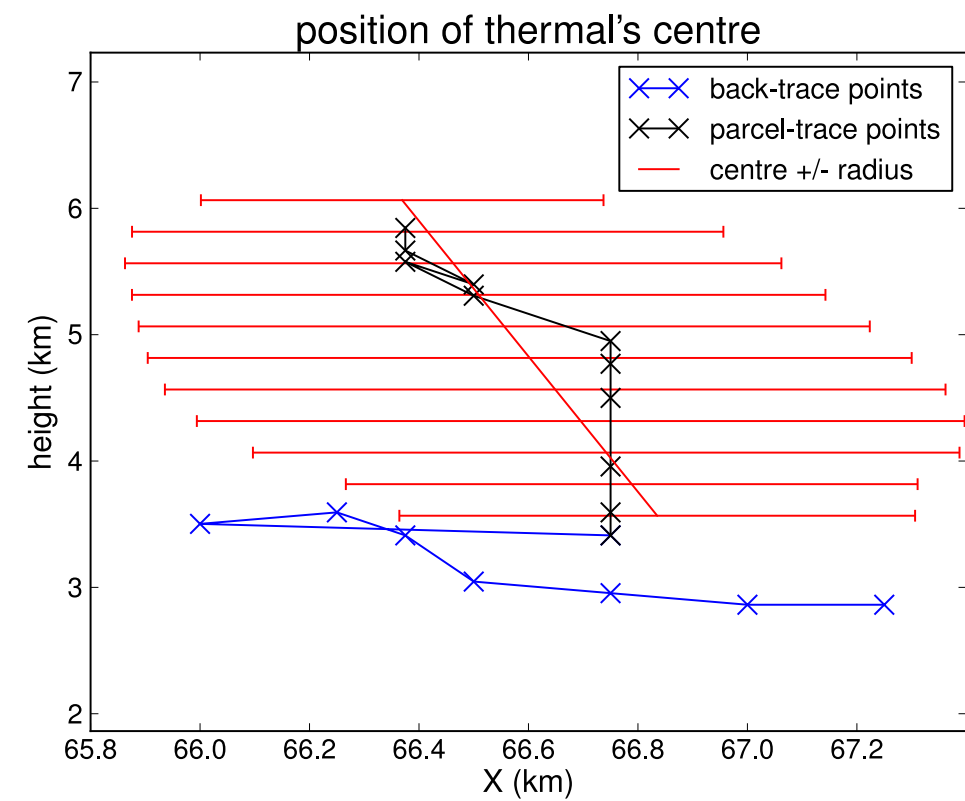
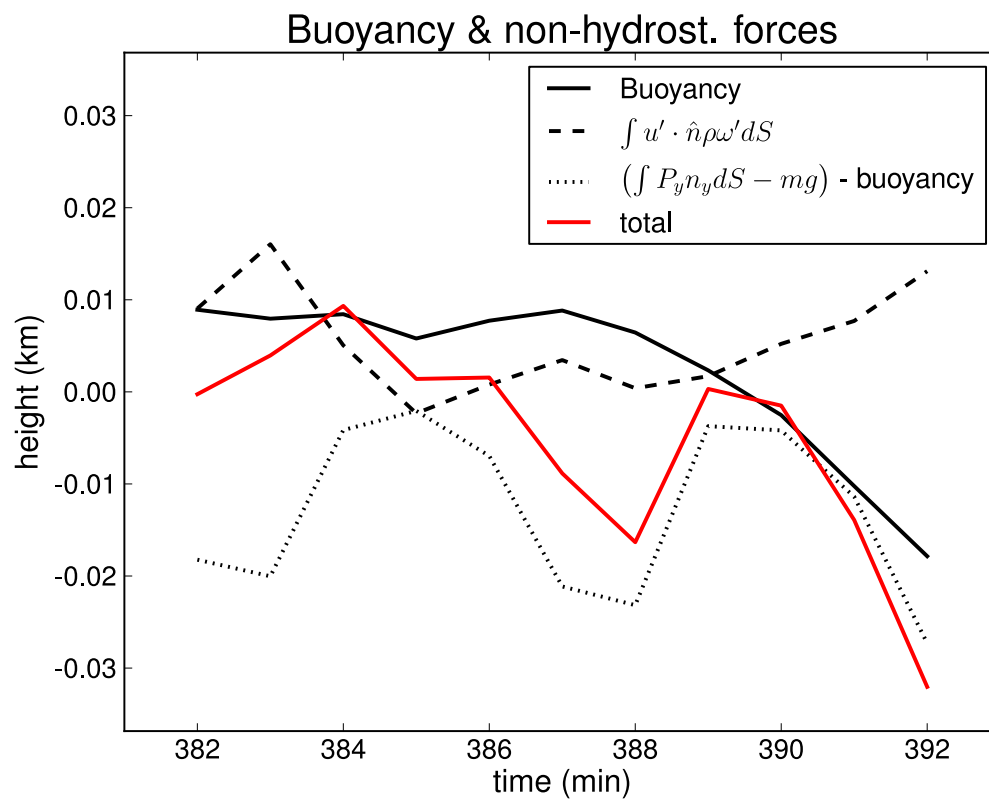
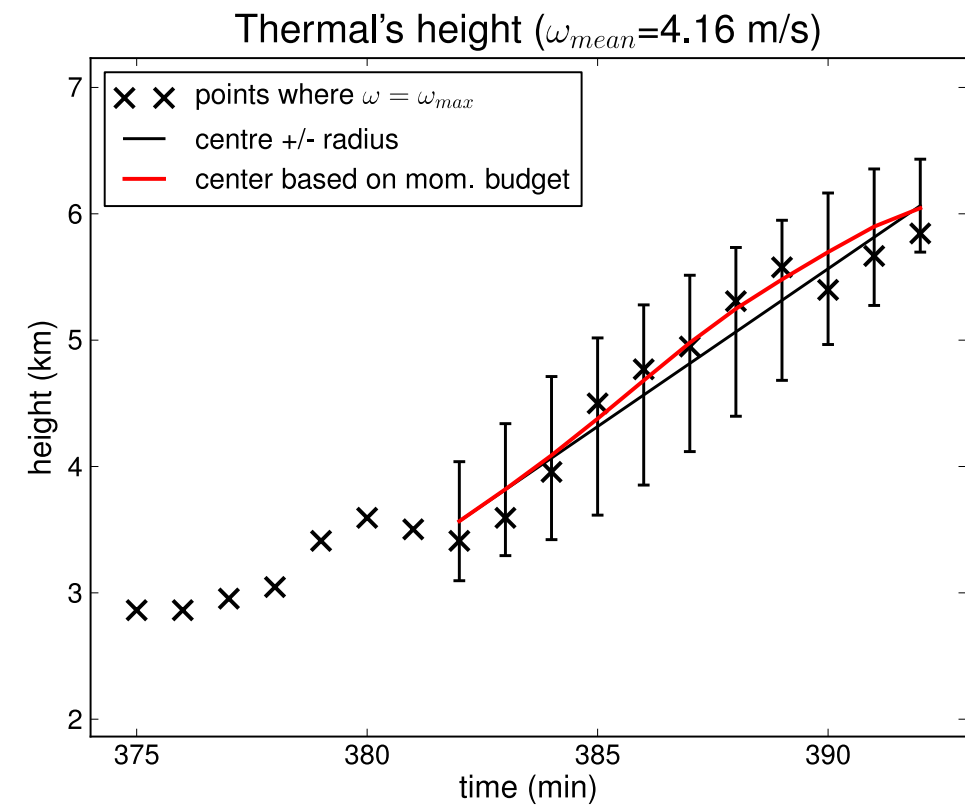
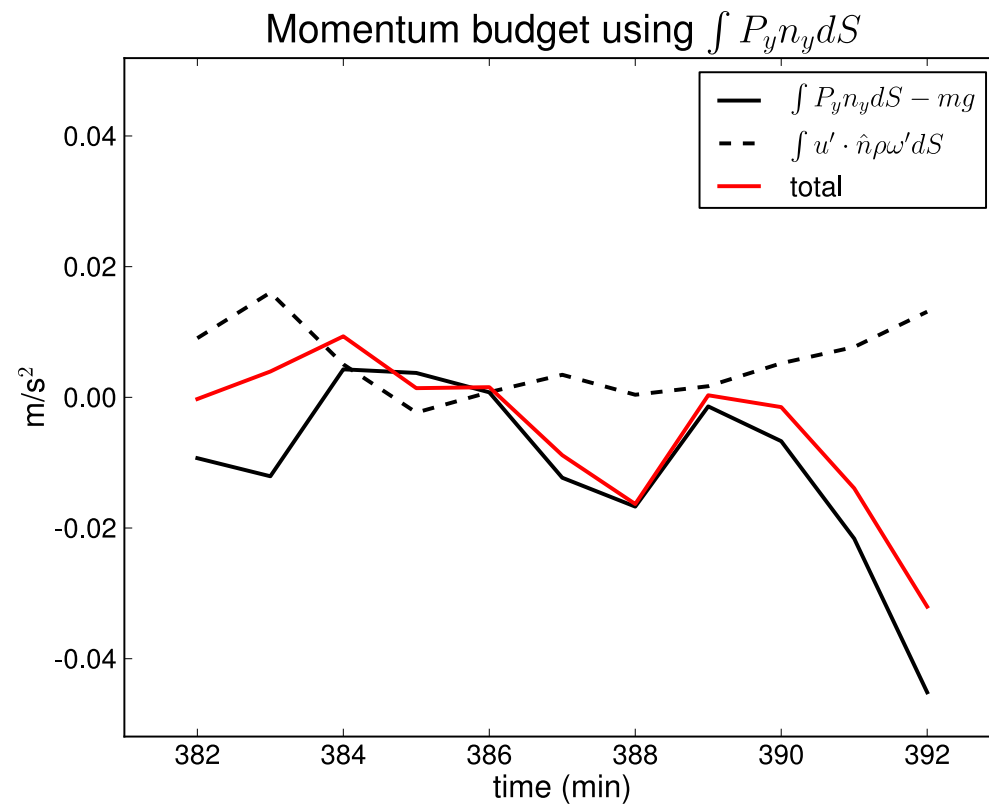
$$\rho dw/dt = \int p \mathbf{k} \cdot \mathbf{n} dS - mg + M$$

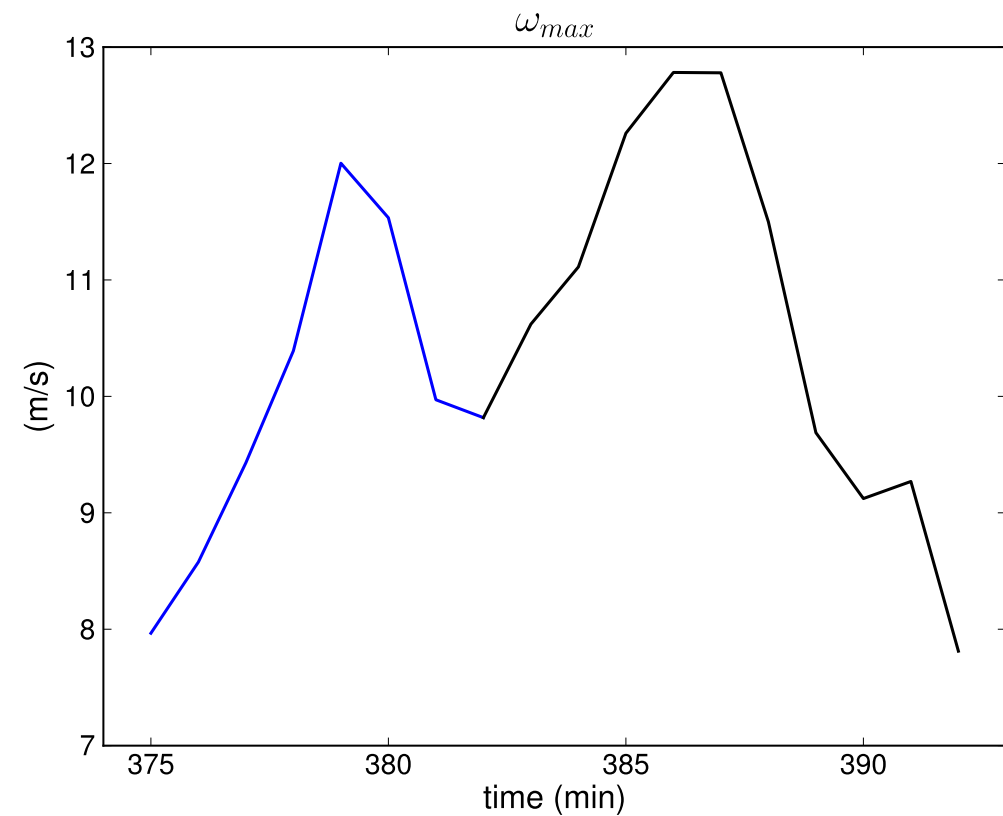
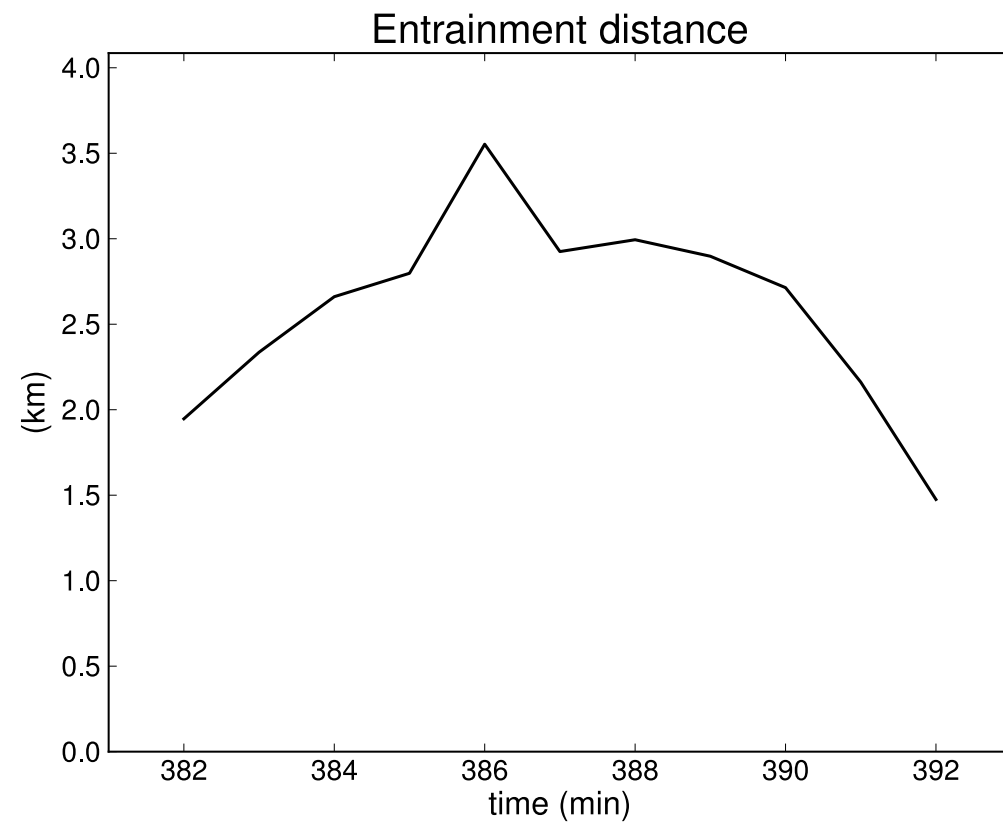
(buoyancy + wave drag + form drag + other nonhyd.)

qc, vorticity & streamfunction at t=8



Case 1 (t0 = 382 min)

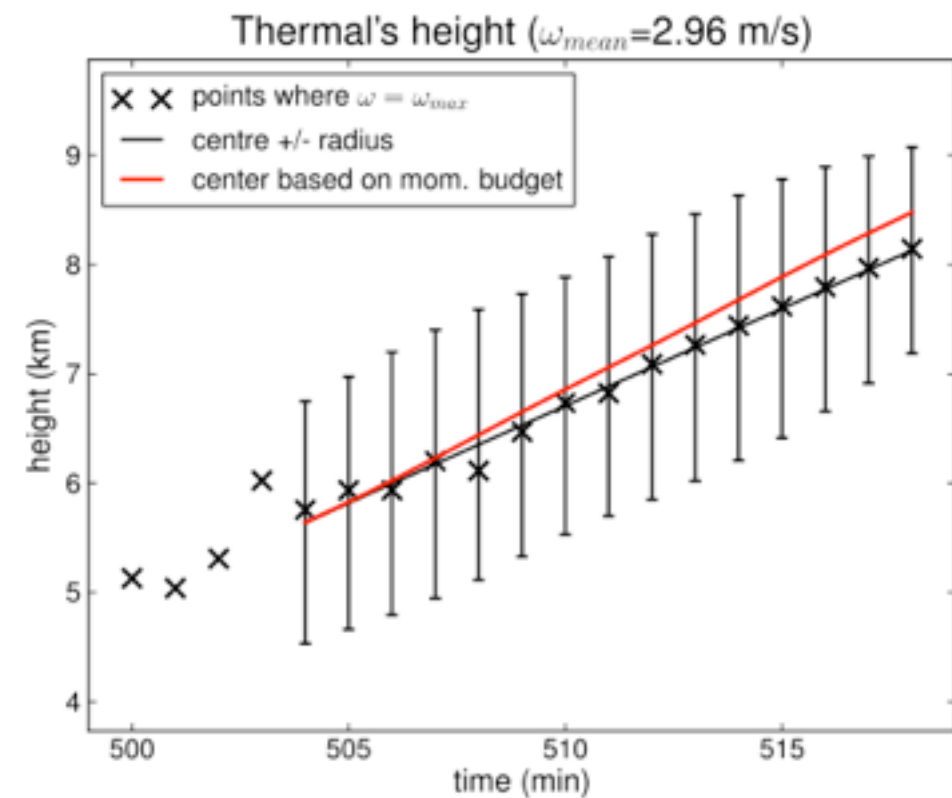
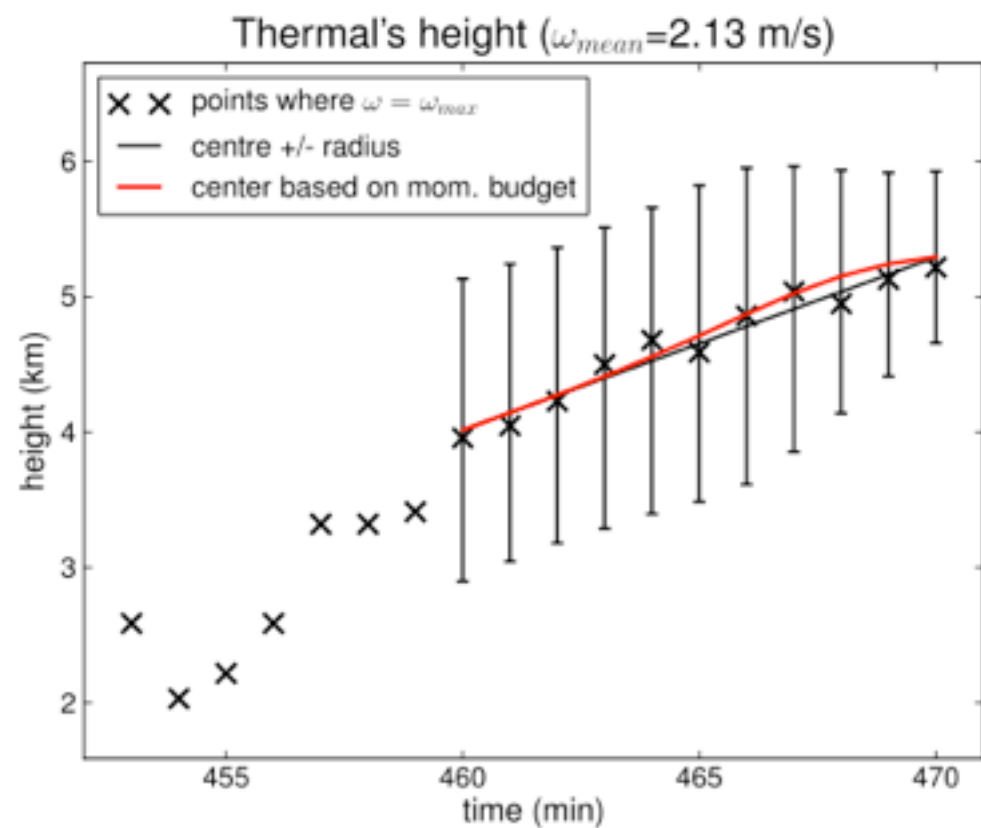
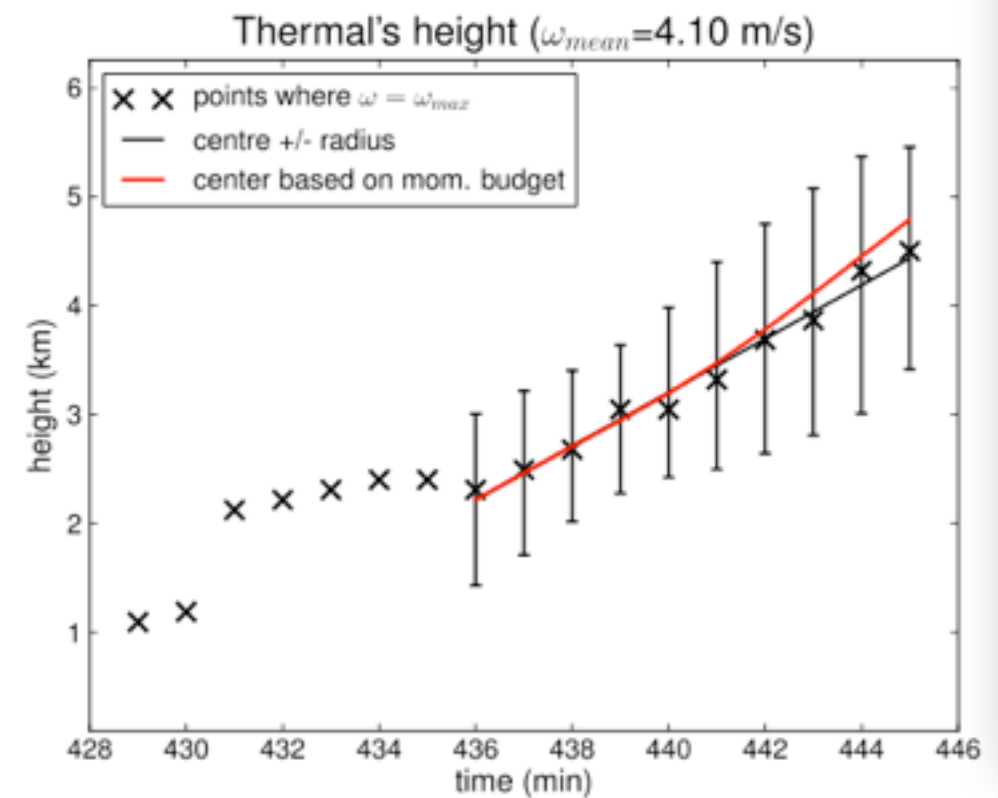
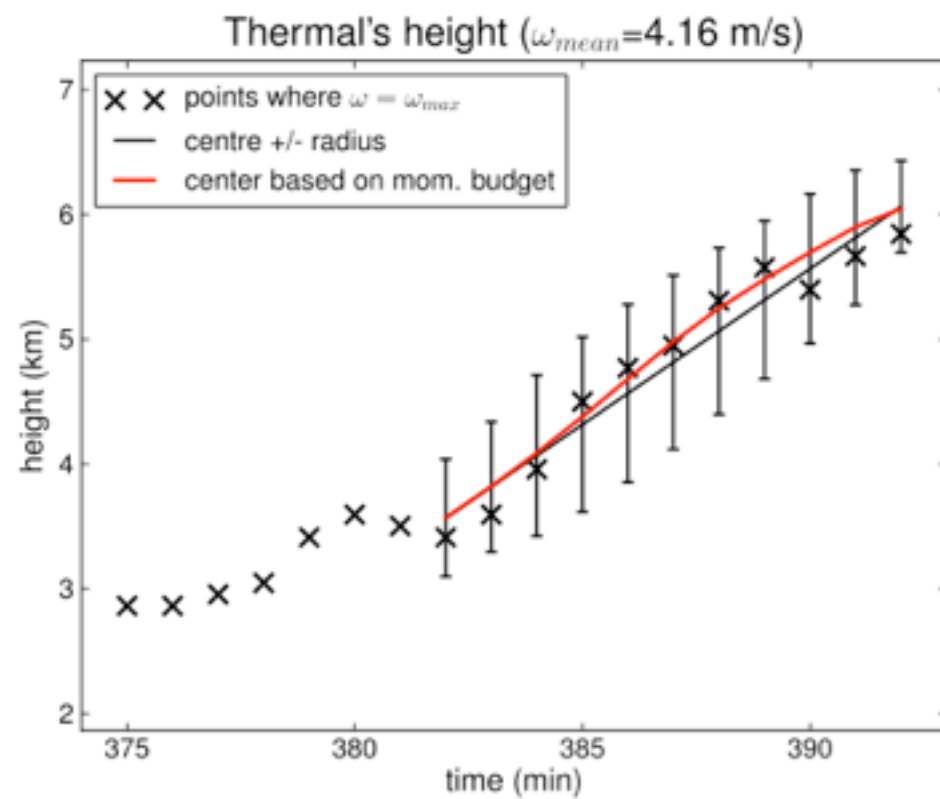




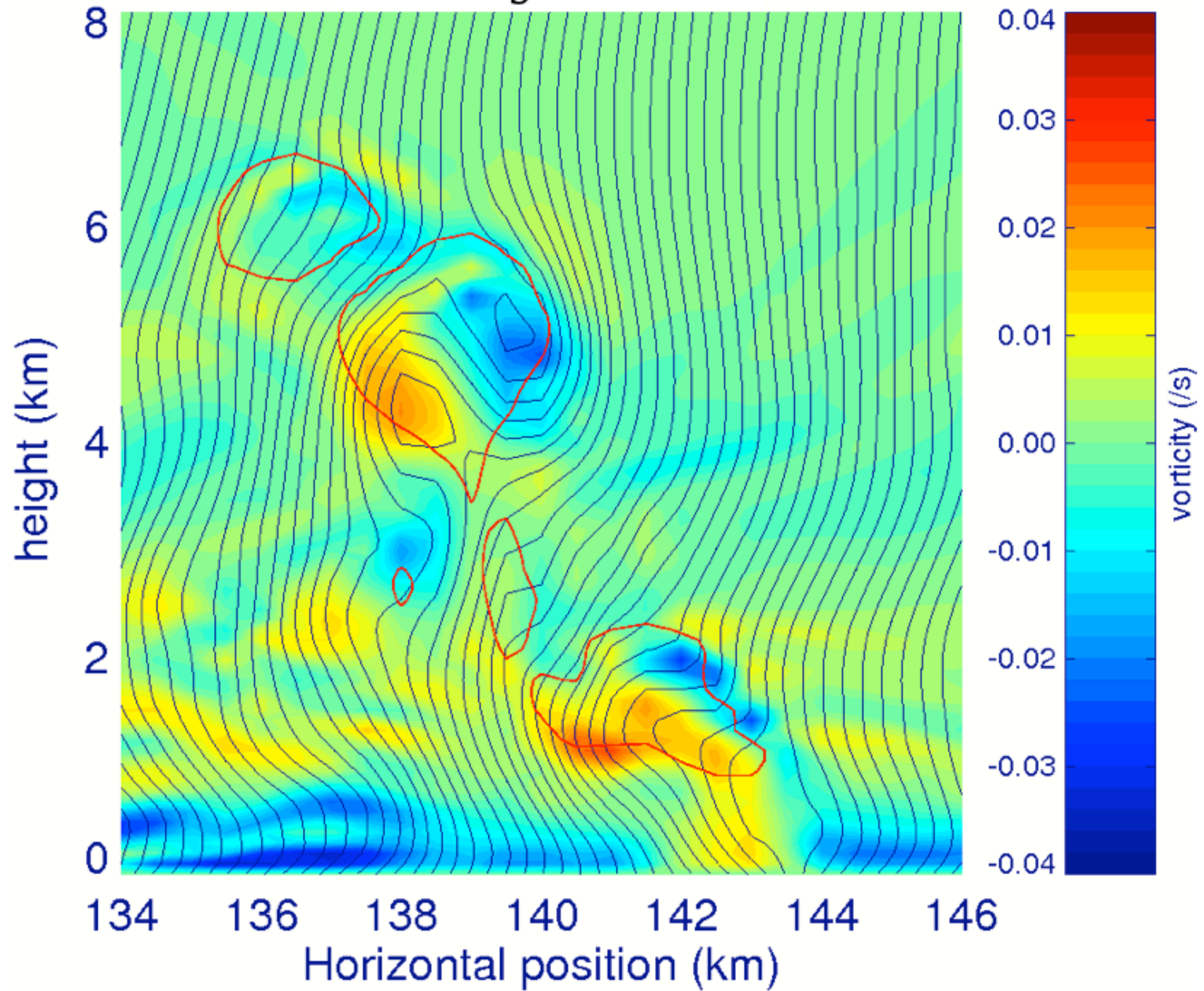
Peak w inside thermal is $\sim 3\times$ the rise rate
of the whole thermal.

1

Entrainment rates $\sim 0.3\text{-}0.5 \text{ km}^{-1}$

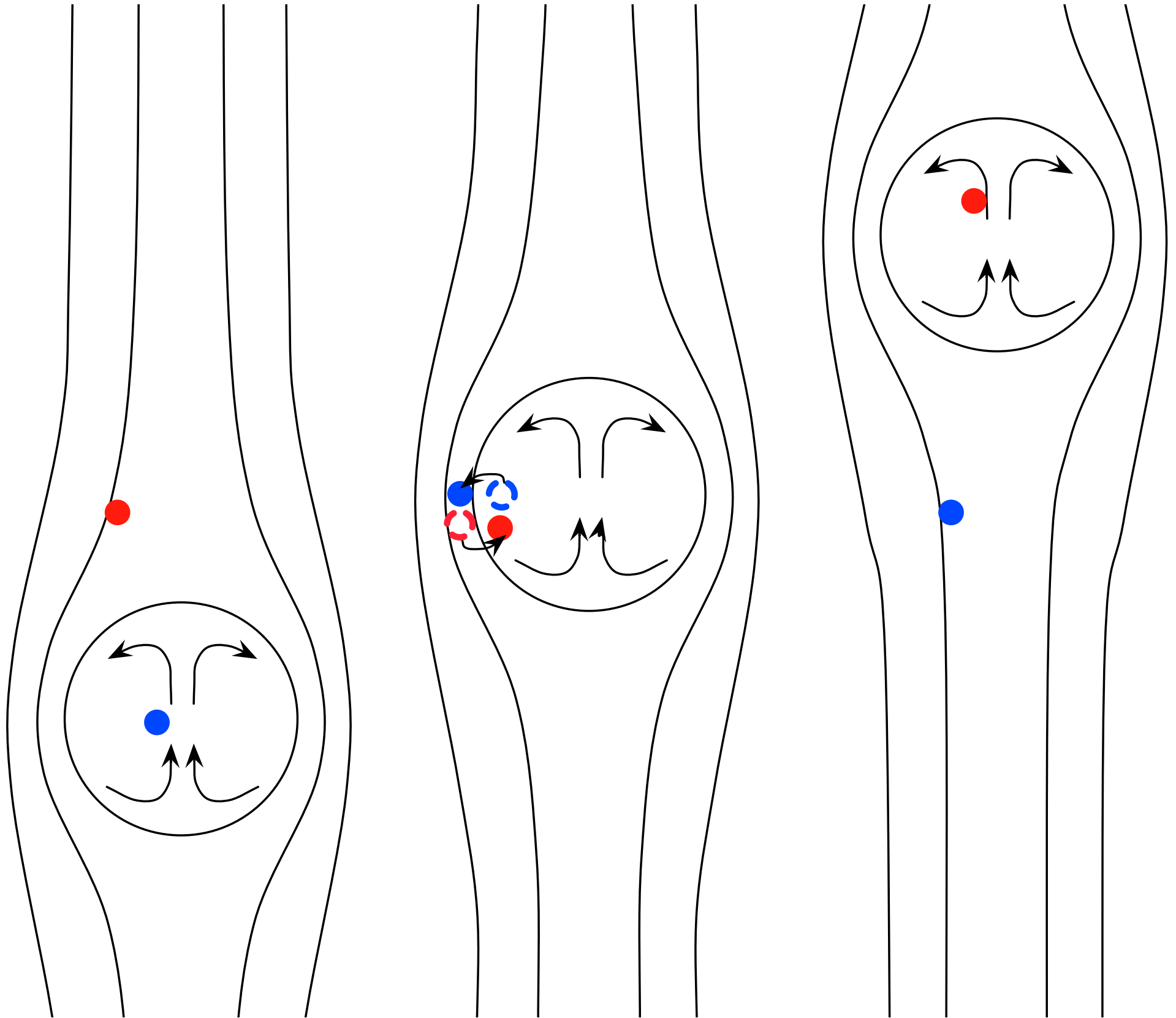


Moving frame



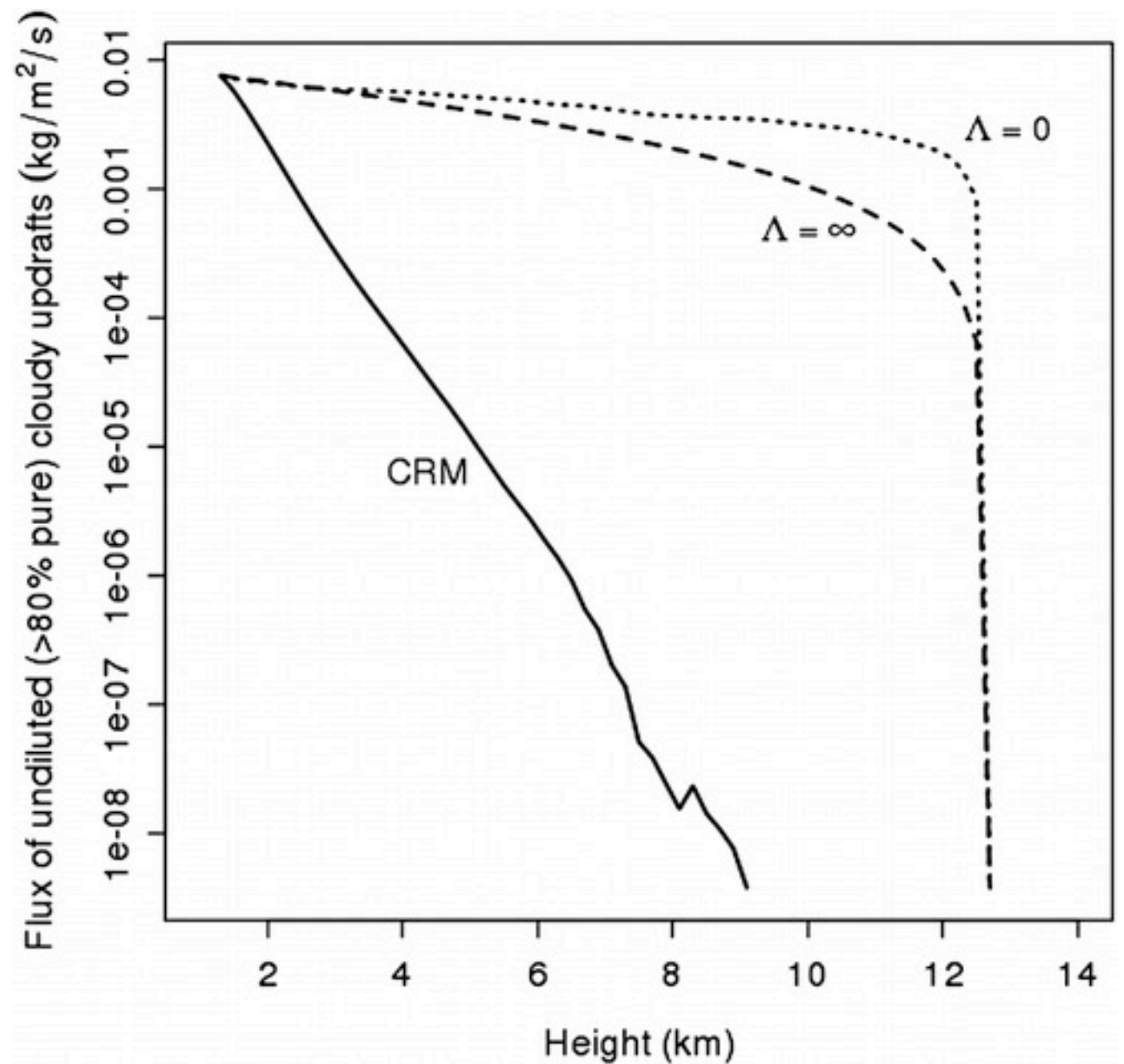
Why?

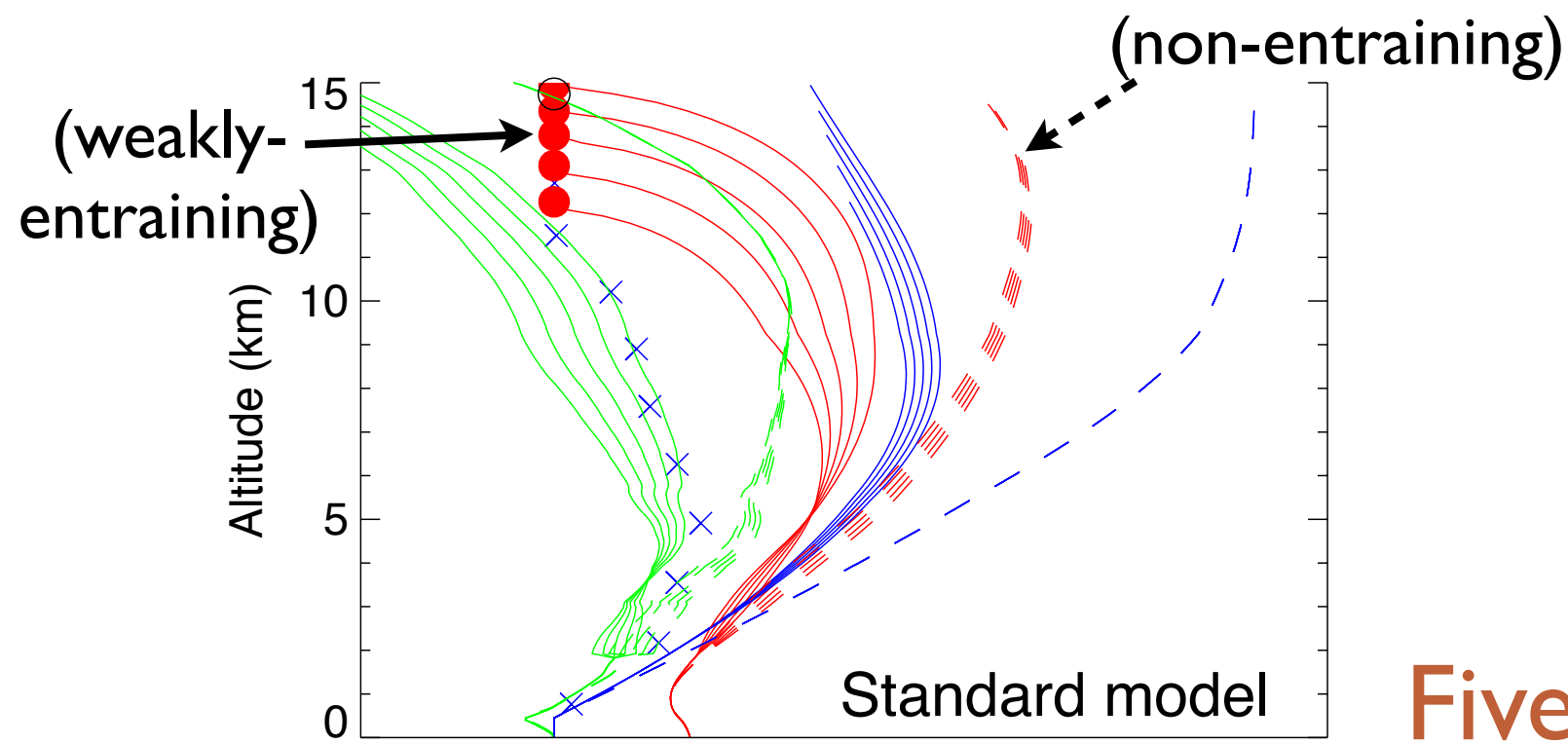
Fluid
exchange
at sides of
thermal
does not
alter the
momentum
budget



Entrainment paradox

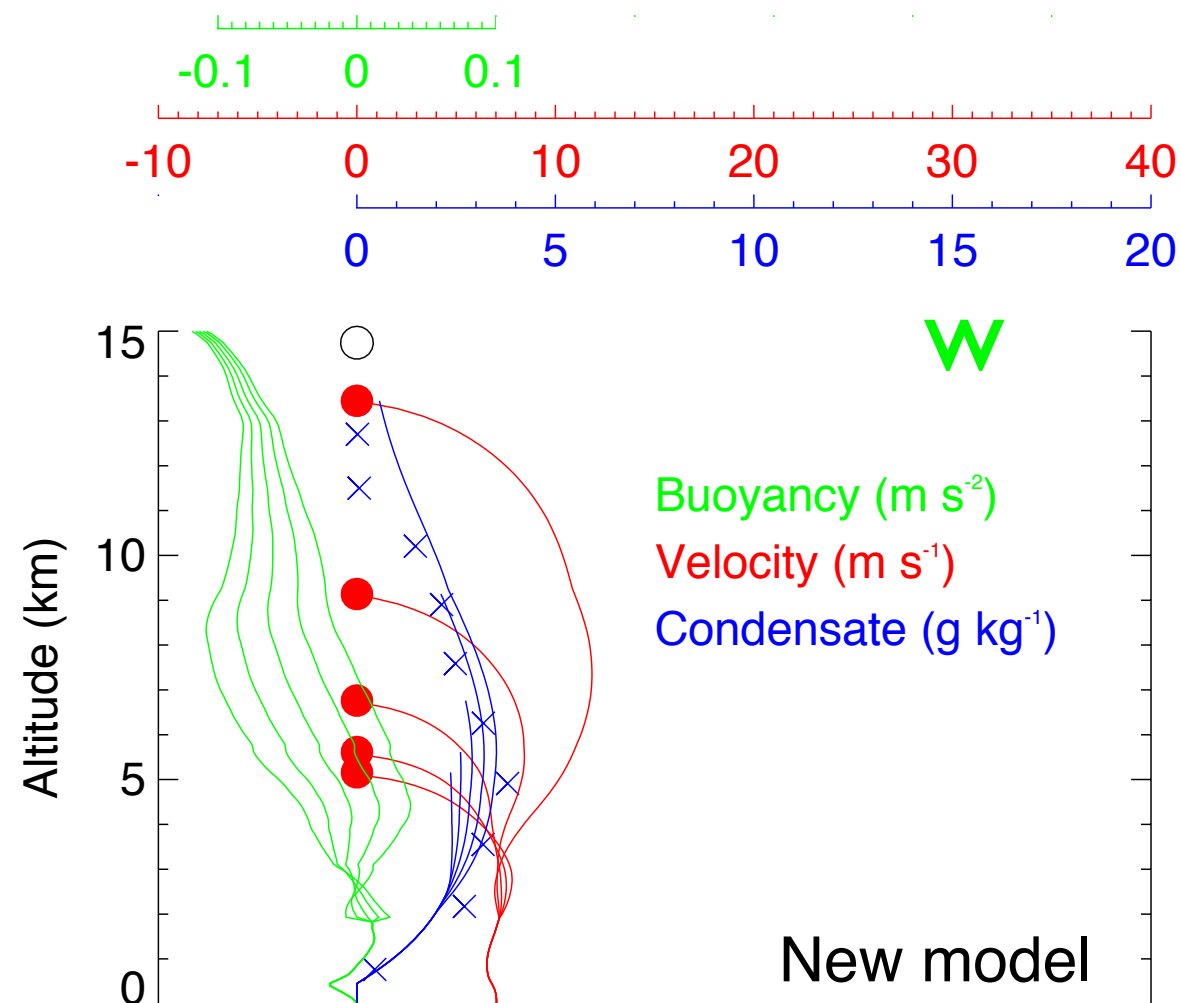
- CRM studies show entrainment rates $\sim (2 \text{ km})^{-1}$ (Khairoutdinov and Randall 2006, Romps and Kuang 2010)
- Highly inconsistent with cumulus parameterizations (Romps and Kuang 2010)





I-D parcel calculations.

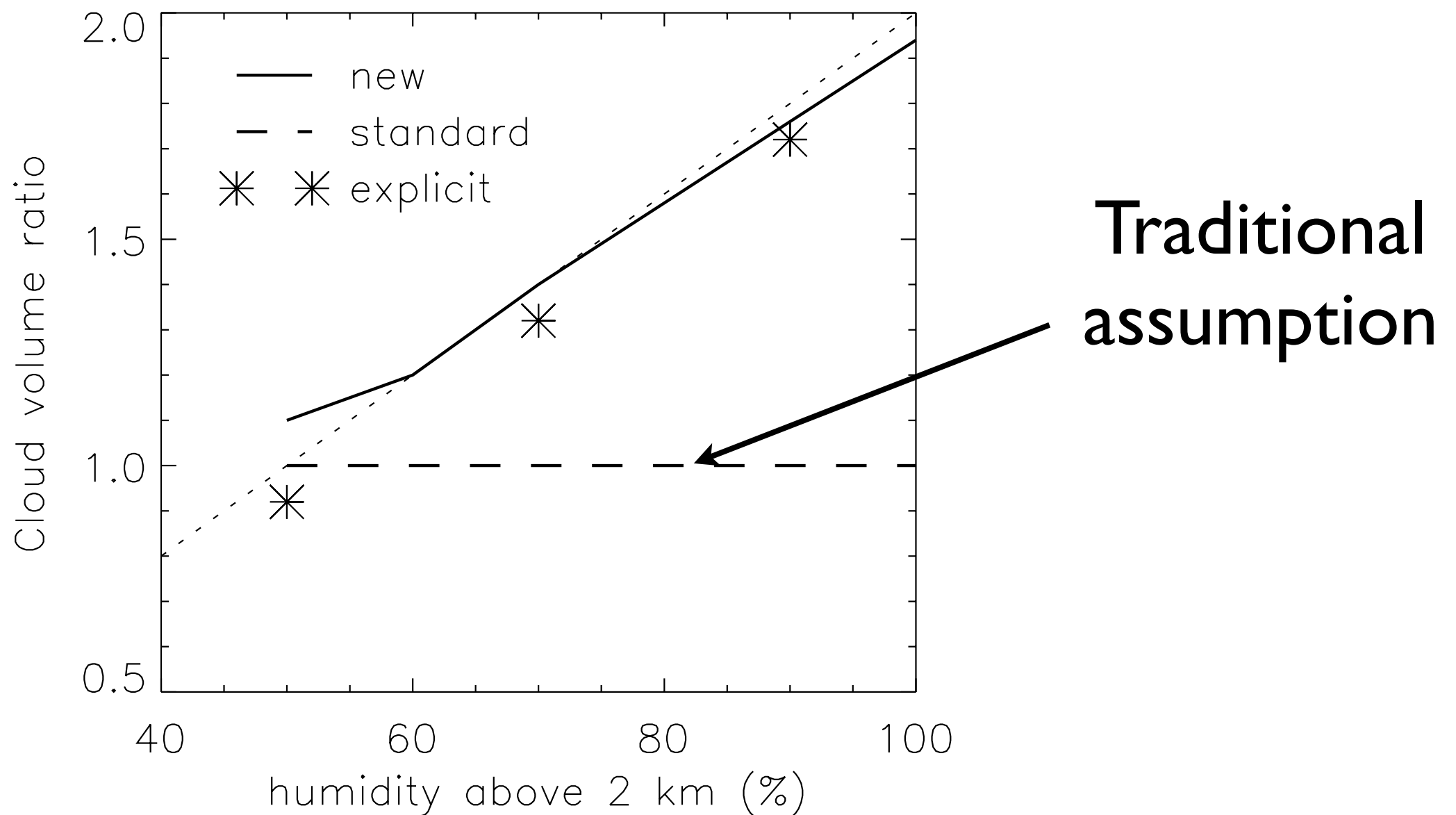
Five values of RH above 2 km: 60-100%.



(Highly entraining;
“slippery”)

x = CRM cloud water

Predicted ratio of cloud volume to updraft volume



Conclusions

- Thermal vortex: a more consistent “parcel”
- Their motion in growing cumulus is primarily inertial, determined by initial kick. Friction and bouyancy relatively weak; entrainment rapid but accompanied by detrainment of zero-w fluid.
- This appears contradictory to common assumptions.
- Initial stages of deep cumulus may be more like shallow convection.

Slippery thermals may:

- Allow highly-entraining clouds to reach upper troposphere.
- Allow more realistic spread of cloud heights?
- Resolve problem of insensitivity to mid-level humidity (cf. *Derbyshire et al 2004*)
- Accurately predict cloud water content and trends in cloud amount
- Predict strong role for boundary layer processes, gusts, etc.--boost continental convection