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Profile

Background and objective

- Proper sets of soil hydraulic properties are indispensable as input for hydrological models which especially use a numerical solution of the Richards' equation to predict and describe water flow.
- The field tension disc infiltrometer (TI) and laboratory undisturbed soil cores are standard methods to measure soil hydraulic properties (HP).
- Objectives: i) comparing the results of in situ and laboratory measurements of soil HP; and ii) evaluating the relevance and the influence of differently calculated/estimated HP on hydrological model performance (to find a proper parameter set).

Methodology

A. The study site:

- Field: potato, typical sandy Podzol.
- Location: the border between Belgium and The Netherlands.
- Equipment at A and B: a weather station, a Diver water level logger, soilwater content sensor probe (at 10, 20, 30, 40, 50 and 60 cm) and tensiometer at 10 and 50 cm (hourly recorded).



B. Measurements:

- In-situ TI experiments (2 replications) at five depths for two profiles (A and B) at consecutive negative pressure heads of 12, 6, 3 and 0.1 cm.
- Lab constant head and sandbox-pressure plate methods on undisturbed soil cores (3 replications) sampled at the same locations/depths of in-situ method.

C. Assessment of hydraulic parameters:

- Method 1- Analytical Wooding's solution using the nonlinear regression method of Logsdon and Jaynes (1993) to determine K_{fs} and α_{G} .
- Method 2- Inverse modeling, performing Hydrus-2D/3D⁽⁴⁾ to determine $K_{f,\sigma}$, α and *n* using initial values from method 1.
- Method 3- Mualem-van Genuchten (MVG) model using RETC software to determine θ_s , α and *n*. K_{ls} was determined directly by applying Darcy's law.

D. Simulation of water flow and root water uptake:

- Numerical model: Hydrus-1D
- Profile geometry: 150 cm with 3 layers
- Study period: growing season 2014 (12 Apr. 22 Sep.)
- Hydraulic model: MVG without air entry value and hysteresis
- Root water uptake model: Feddes model without solute stress
- Upper boundary condition: atmospheric (precipitation, LAI and ETp,)
- Bottom boundary condition: variable pressure head (GWL)
- Input hydraulic parameters: field (Method 2) and lab (method 3) dataset.
- Evaluation: root-mean-square deviation (RMSE), coefficient of determination (r^2) , and Nash-Sutcliffe coefficient of efficiency (C_e)



Sensitivity of soil water simulation using different soil hydraulic parameter characterization as initial input values

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Results and discussion



- Lab hydraulic parameters \succ K_{ls} and *n* increase and θ_s and α_{vG} decrease with increasing depth.
- > Significant differences of K_{ls} values of profiles.

Spatial variability in horizontal and
vertical dimensions.



probability.

Field infiltration, Wooding's solution and inverse optimization





Water retention curves

- MVG differences Significant parameters θ_s , *n* and α_{vG} values between lab and field measurements.
- > Significant correlation between the slope of the WRC of both methods (r = 0.81).
- > The underestimation of saturated water content results from the matrix not being fully saturated.



θ_r^A	θ_s cm ³ cm ⁻³	α_{vG} cm ⁻¹	n	<i>K</i> _b cm h ⁻¹
0.053 ^{ab}	0.525 ^a	0.05733 ^a	1.567 ^c	0.881 ^c
0.055 ^{ab}	0.509 ^a	0.05037 ^a	1.584 ^c	10.01 ^c
0.075 ^a	0.403 ^b	0.04029 ^{ab}	1.449 ^c	2.840 ^c
0.03 ^b	0.35 ^b	0.014 ^c	2.213 ^b	34.046 ^b
0.003 ^{bc}	0.38.3 ^b	0.02038 ^b	2.885 ^a	60.423 ^a
0.069 ^a	0.545 ^a	0.07172 ^a	1.456 ^{ab}	1.483 ^b
0.072 ^a	0.530 ^a	0.05924 ^a	1.508 ^{ab}	3.365 ^{ab}
0.084 ^a	0.367 ^b	0.02448 ^b	1.444 ^b	0.761 ^b
0.013 ^b	0.361 ^b	0.02922 ^b	1.879 ^a	5.752 ^a

^A Not estimated (measured at 15,000 cm). Means followed by the same letter do not differ across depths (in each profile) by the LSD test at the level of 5%

Significant differences $(p \le 0.05)$ of K_s values for lab and field (optimization and Wooding approaches).

> A significant correlation between lab and field $K_{\rm s}$ (r = 0.75).

Relevance of hydraulic parameter set on model performance

- > The model over and under predicted soil-water content using lab and field experiments data sets.
- > Small sample volume, tempo-spatial variability and underestimation hydraulic parameters, especially θ_r , using field methods could be possible reasons for the under prediction of soil-water content.

Node (cm)			Profile /	4				
		Field			Lab			
	RMSE ^a	C _e ^a	1 ^{2a}	RMSE ^a	C _e ^a			
Water conten	t							
10	0.044	0.11	0.42	0.063	-0.85			
20	0.053	-1.06	0.29	0.050	-0.78			
30	0.072	-2.87	0.37	0.034	0.10			
40	0.070	-4.58	0.27	0.043	-1.13			
50	0.051	-3.64	0.39	0.045	-2.65			
60								
Water potential								
10	217.7	-0.35	0.16	197.1	-0.10			
50	99.0	0.05	0.30	156.4	-1.38			
			Profile E	3				
Water content								
10	0.052	-3.0	0.38	0.056	-3.55			
20	0.046	-3.6	0.26	0.054	-5.33			
30	0.055	-19.3	0.40	0.037	-7.99			
40	0.043	-25.4	0.37	0.024	-7.29			
50	0.101	-391.2	0.29	0.062	-144.8			
60	0.156	-121.6	0.38	0.122	-73.1			
^a PMSE C and r^2 are the root mean square deviation (cm and cm ³ cm ⁻³) the								

oefficient of efficiency and the coefficient of determination

results (30 - 50 cm depths).

Conclusions and perspectives

- infiltration rates using Hydrus-2D/3D.
- water potential in the subsoil.
- profile.

Further reading

- Geophysics, 126: 35-41.
- Earth Syst. Sci., 20(1): 487-503.

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 \geq According to the C_e and RMSE criteria the lab method yielded slightly better

> Inverse optimization resulted in excellent matched between observed and fitted

> Field experiment parameter sets, which were achieved fast and simple, resulted in slightly better soil-water content simulation performance in the topsoil and soil-

 \geq It is not possible to judge whether laboratory or field methods should be preferred and most appropriate data set to predict soil water fluctuations in a complete soil

> The reasons behind the deviations should be further unraveled.

> Parameter optimization over long time such as a growing season in combination with independent soil-water content and soil-water potential data is necessary.

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