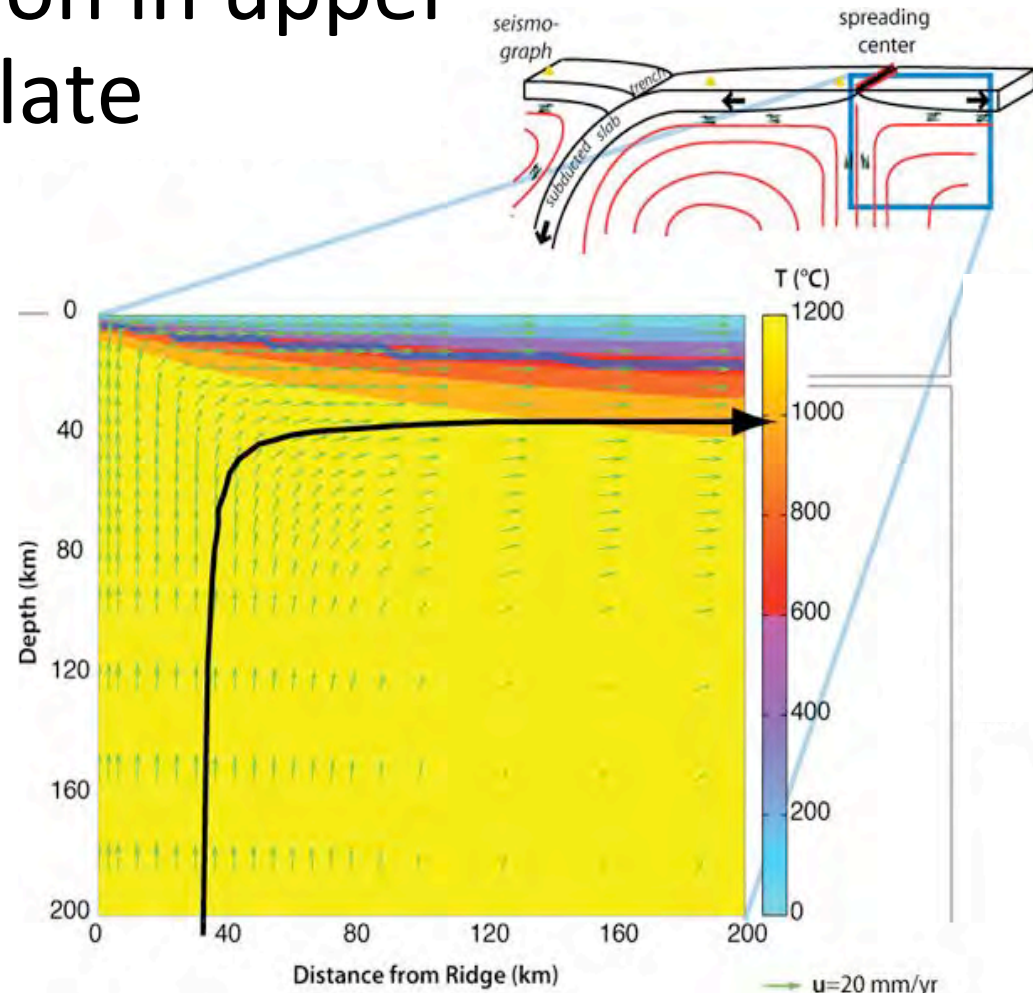


Rheologic effects of Crystal Preferred Orientation in upper mantle flow near plate boundaries

*Donna Blackman, Olivier Castelnau
Don Boyce, Paul Dawson*

Goal- are fully-coupled models of mantle flow & microstructural (CPO) evolution required ?

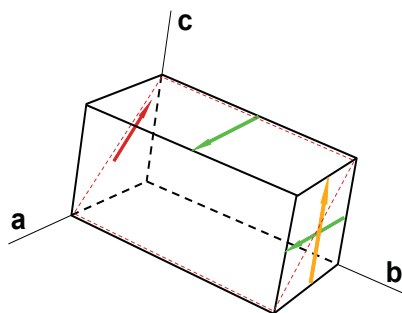
Motivation- understand regional flow patterns and processes
>>> *improve interpretation of seismic anisotropy*



Linked Micro-Macro Numerical Modeling

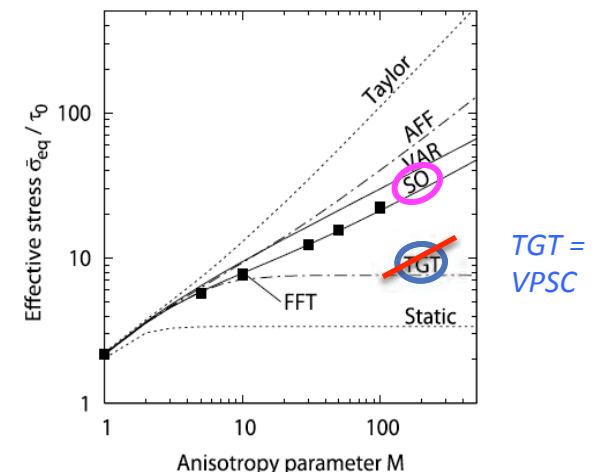
- Compute regional mantle flow field using **Isaiah**
Cornell 3D parallel FEM: deformation in Eulerian frame, coupled flow & temperature fields
- Calculate velocity gradient tensor along streamlines ending at all elements
- Calculate CPO at each element using Second Order Self Consistent scheme
Castelnau et al. (JGR 2008; GRL 2009); 1000-grain polycrystals, dislocation glide dominant
- Determine effective viscosity tensor for polycrystal at each element
specify stress:strain-rate behavior of polycrystal (linear vs power law $n=2-3$)
- Re-compute flow field using updated anisotropic viscosity tensor (V_{ijkl})
- Iterate (flow, V_{ijkl} stabilize) , compute seismic anisotropy

Dislocation slip systems for Olivine crystals



Slip system	Reference stress MPa
● (010)[100]	5.5×10^{-4}
● (001)[100]	5.5×10^{-4}
● (010)[001]	5.5×10^{-3}
● {101} <101>	5.5×10^{-2}

4th 'hard' system allows general deformation



Flow-Induced Crystal Preferred Orientation

B-1, $n=1$, intermediate coupling (it1)
Pole Figures (100)

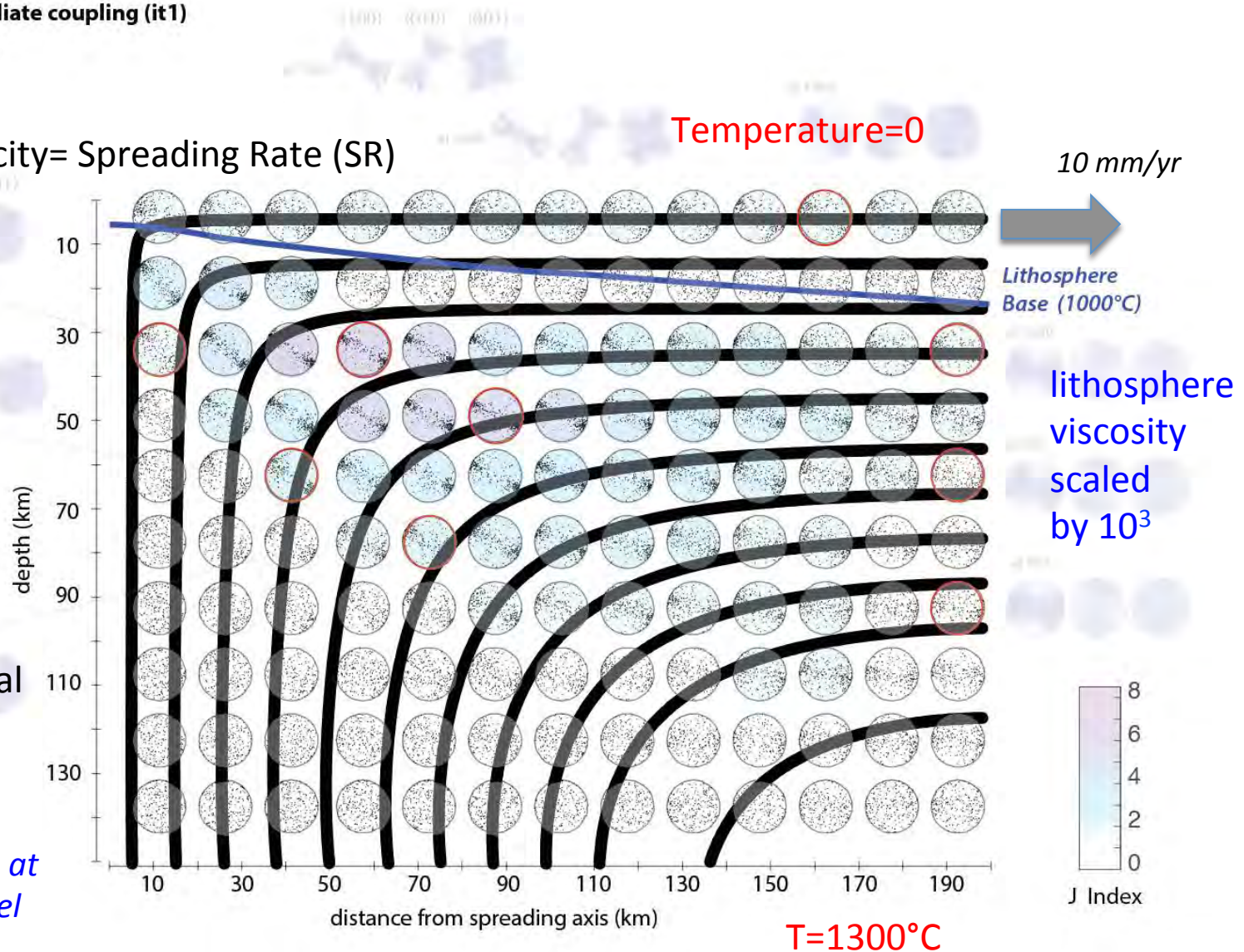
BCs: top velocity= Spreading Rate (SR)

horizontal
gradients
zero at
spreading
axis

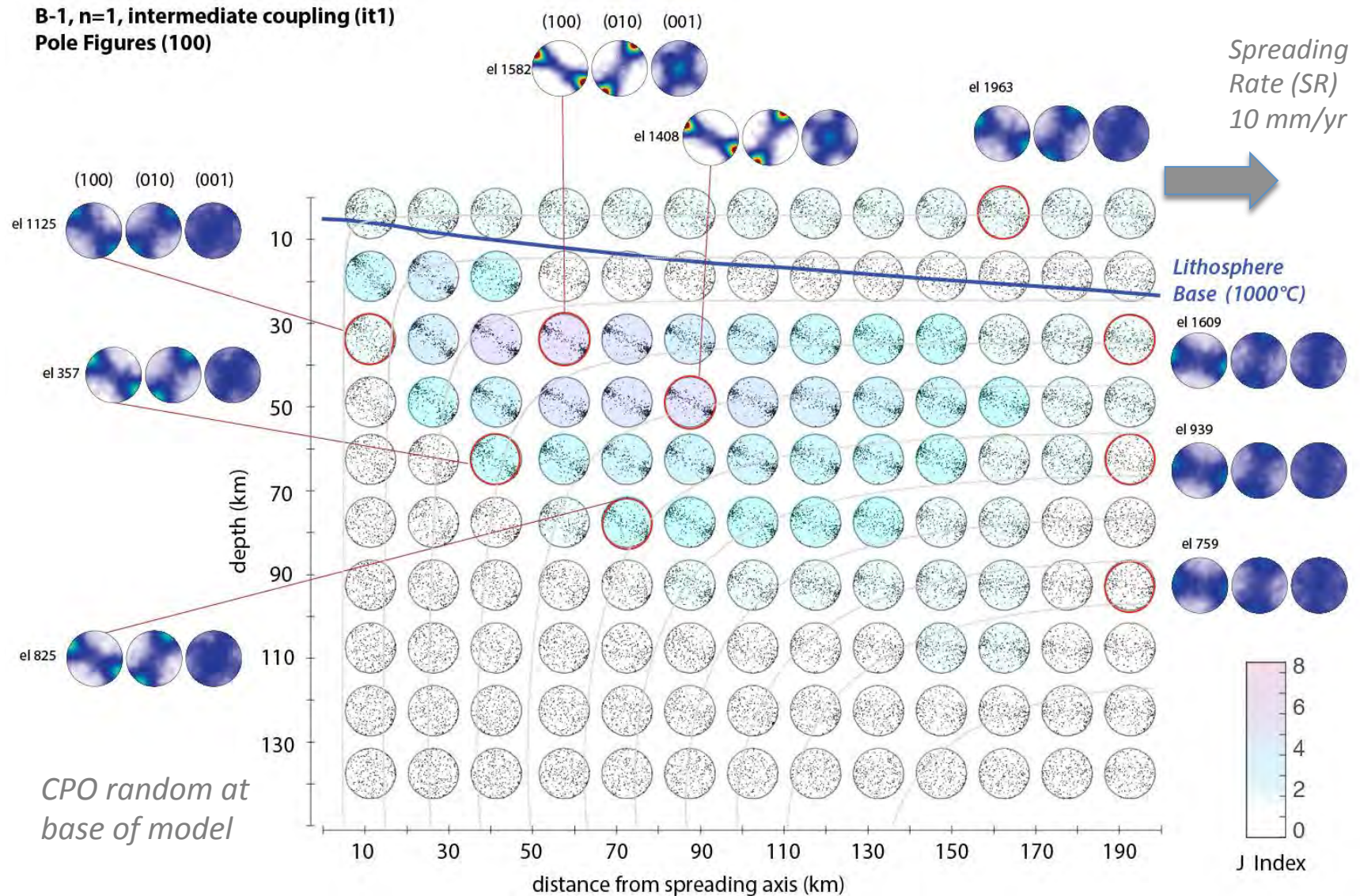
stress-free
base

only horizontal
flow out of
right side

*CPO random at
base of model*



Flow-Induced Crystal Preferred Orientation



Viscosity Tensor

$$\begin{bmatrix} \sigma_{11} \\ \sigma_{22} \\ \sigma_{33} \\ \sigma_{23} \\ \sigma_{13} \\ \sigma_{12} \end{bmatrix} = \begin{bmatrix} V_{1111} & V_{1122} & V_{1133} & V_{1123} & V_{1113} & V_{1112} \\ V_{2211} & V_{2222} & V_{2233} & V_{2223} & V_{2213} & V_{2212} \\ V_{3311} & V_{3322} & V_{3333} & V_{3323} & V_{3313} & V_{3312} \\ V_{2311} & V_{2322} & V_{2333} & V_{2323} & V_{2313} & V_{2312} \\ V_{1311} & V_{1322} & V_{1333} & V_{1323} & V_{1313} & V_{1312} \\ V_{1211} & V_{1222} & V_{1233} & V_{1223} & V_{1213} & V_{1212} \end{bmatrix} \begin{bmatrix} \dot{\epsilon}_{11} \\ \dot{\epsilon}_{22} \\ \dot{\epsilon}_{33} \\ 2\dot{\epsilon}_{23} \\ 2\dot{\epsilon}_{13} \\ 2\dot{\epsilon}_{12} \end{bmatrix}$$

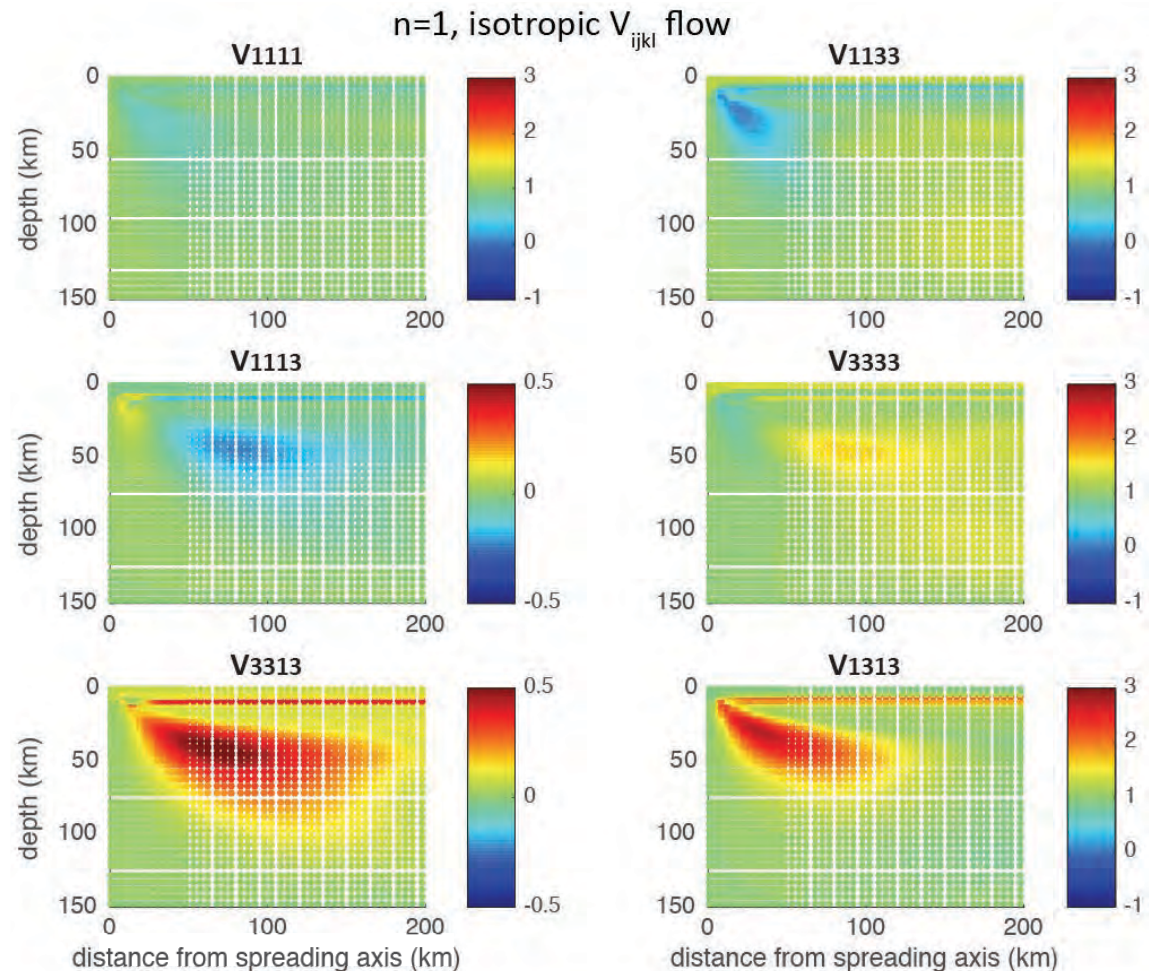
calculate polycrystal
strain rate ($\dot{\epsilon}$) response
to applied stress (σ)

polycrystal has CPO that
evolved along flowline to
element

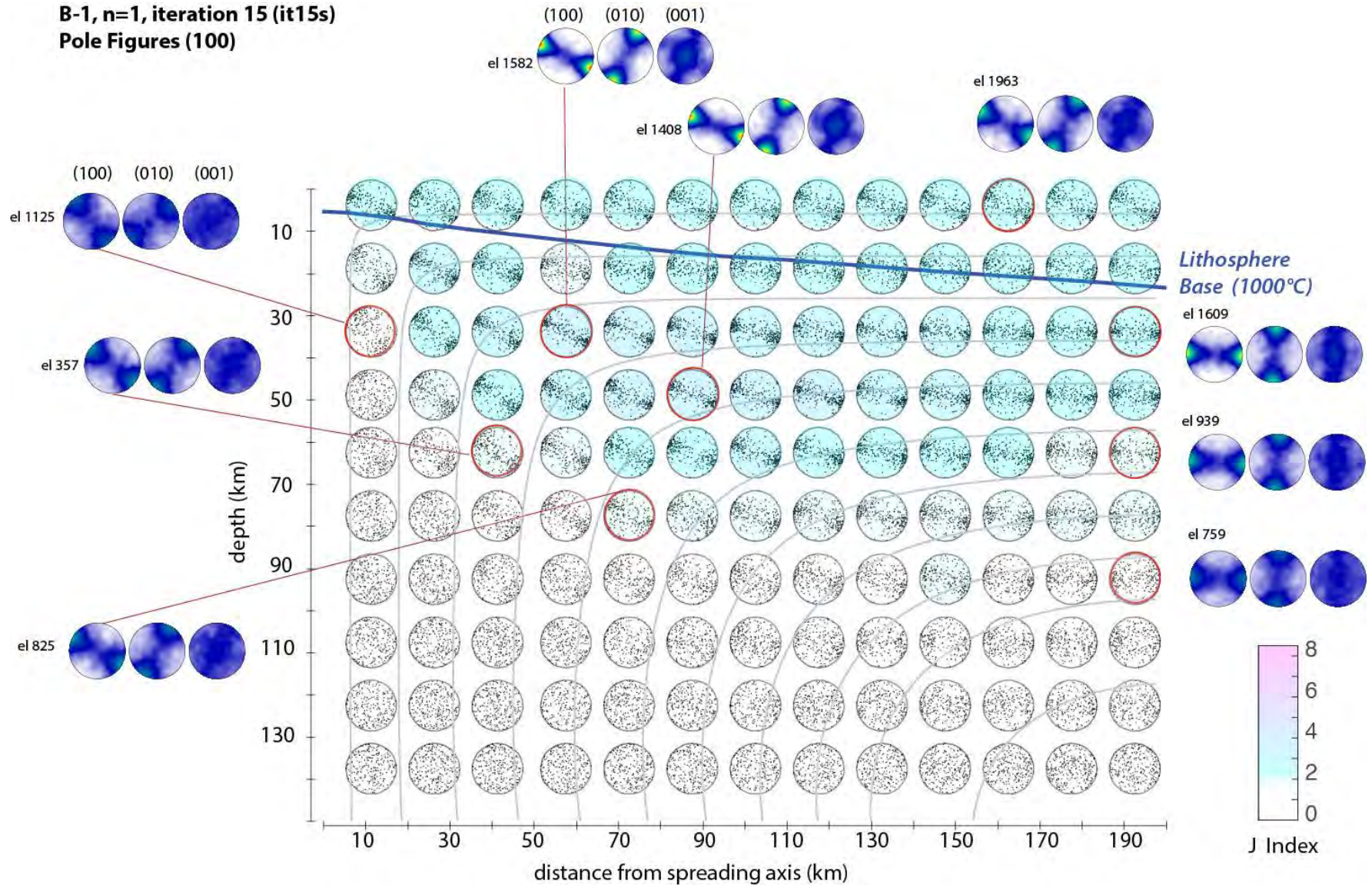
flow is 2-D, although
model & texturing are
calculated in 3-D

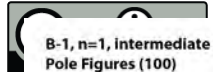
6 independent V_{ijkl}
components

x: spreading direction (1)
z: vertical (3)
y: \perp to plane (2)

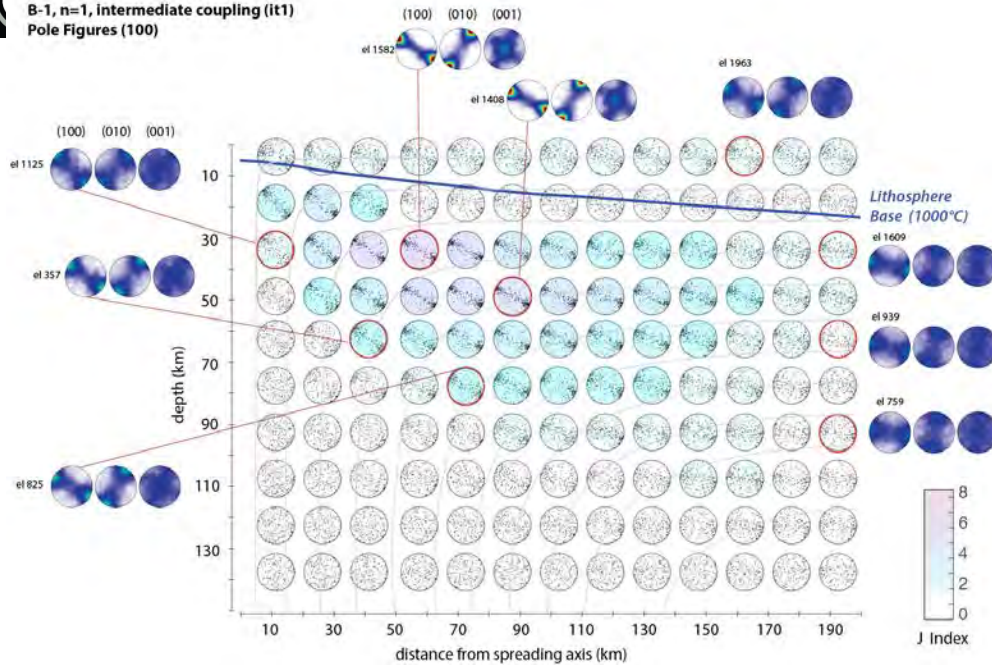


Coupled flow/CPO Result

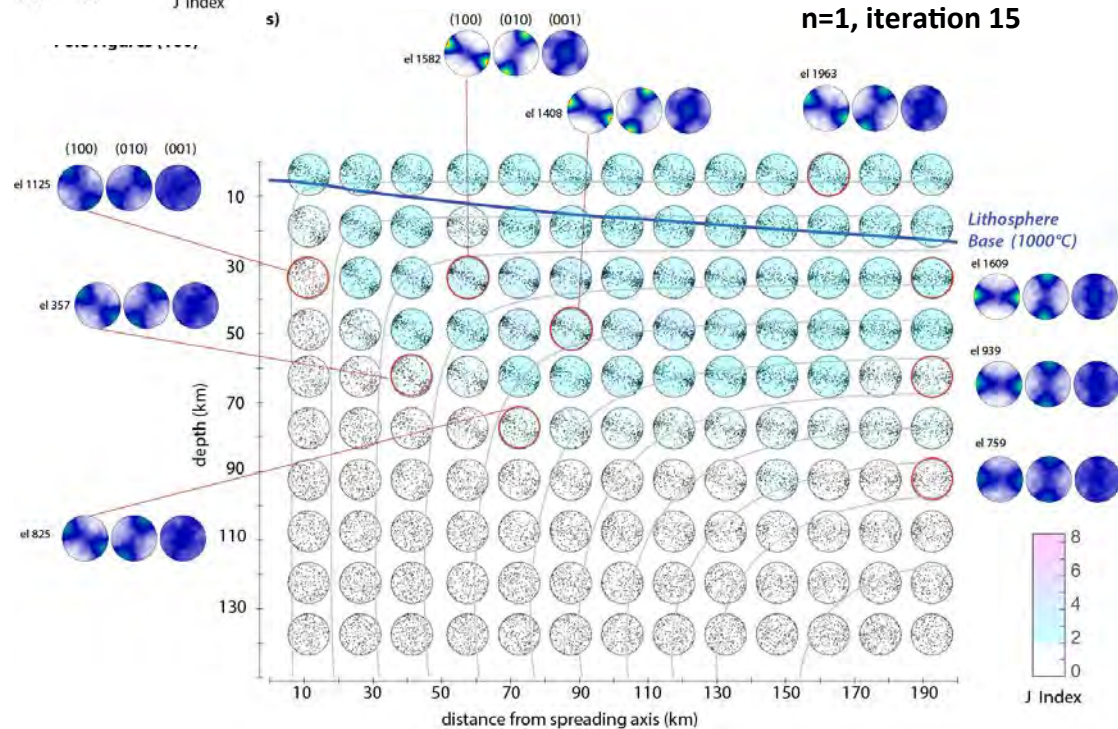
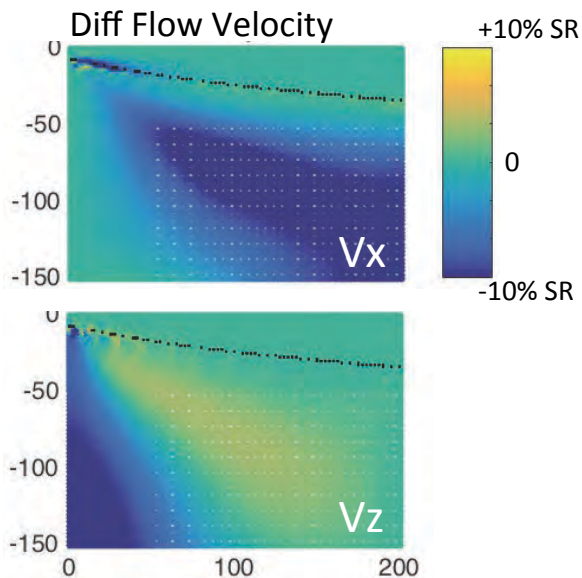




B-1, n=1, intermediate coupling (it1)
Pole Figures (100)

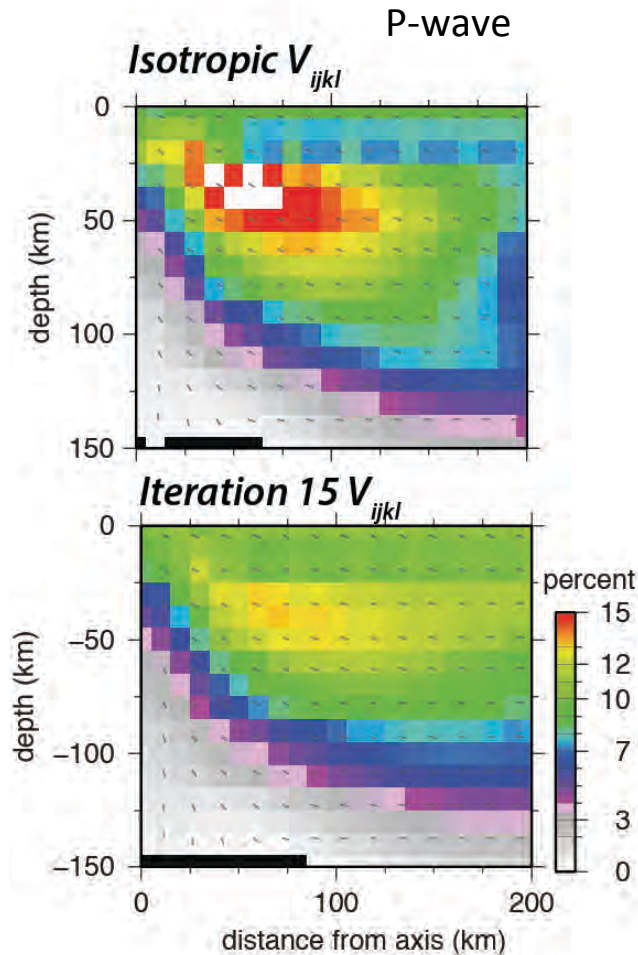


Compare CPO, flowlines & flow velocities

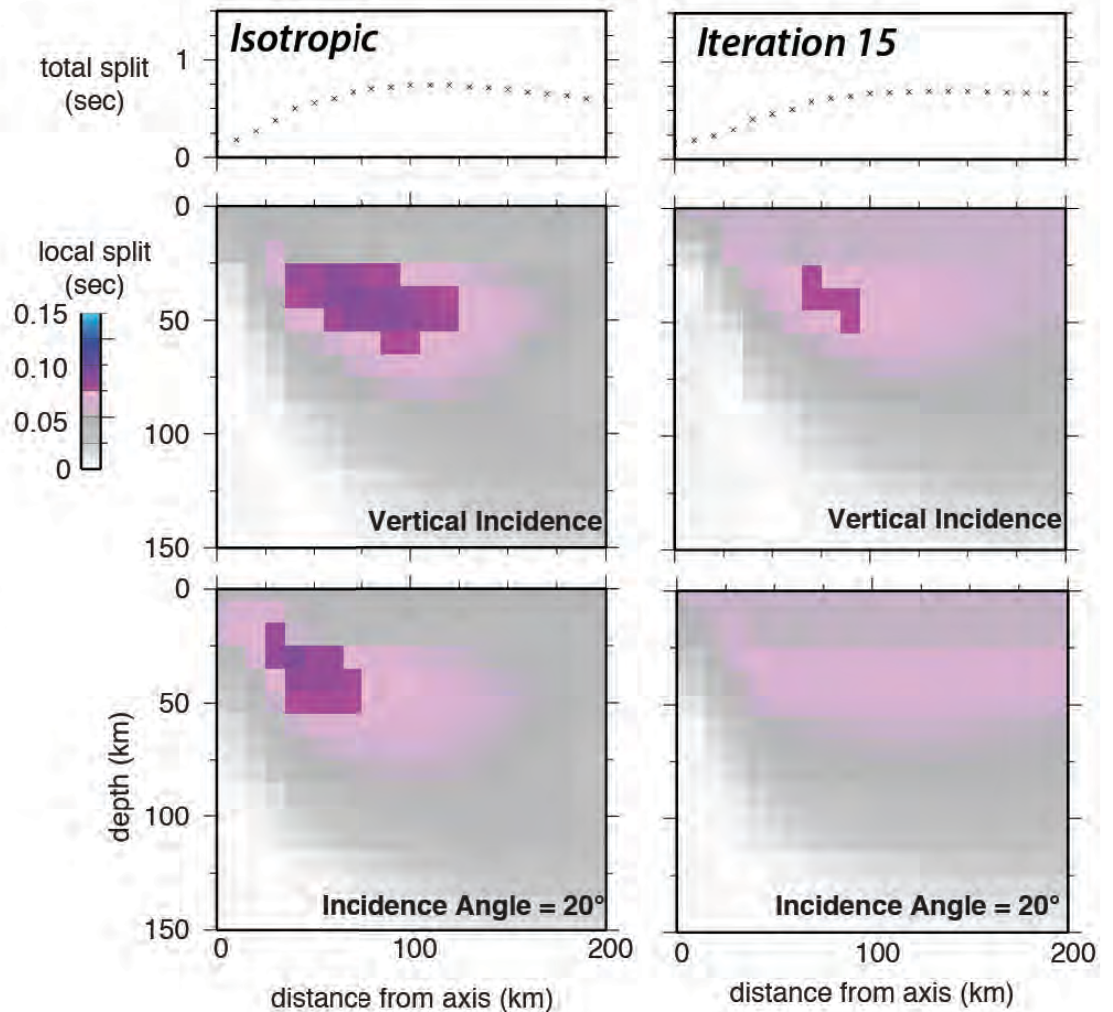


Predicted Seismic Anisotropy

Linear ($n=1$) case



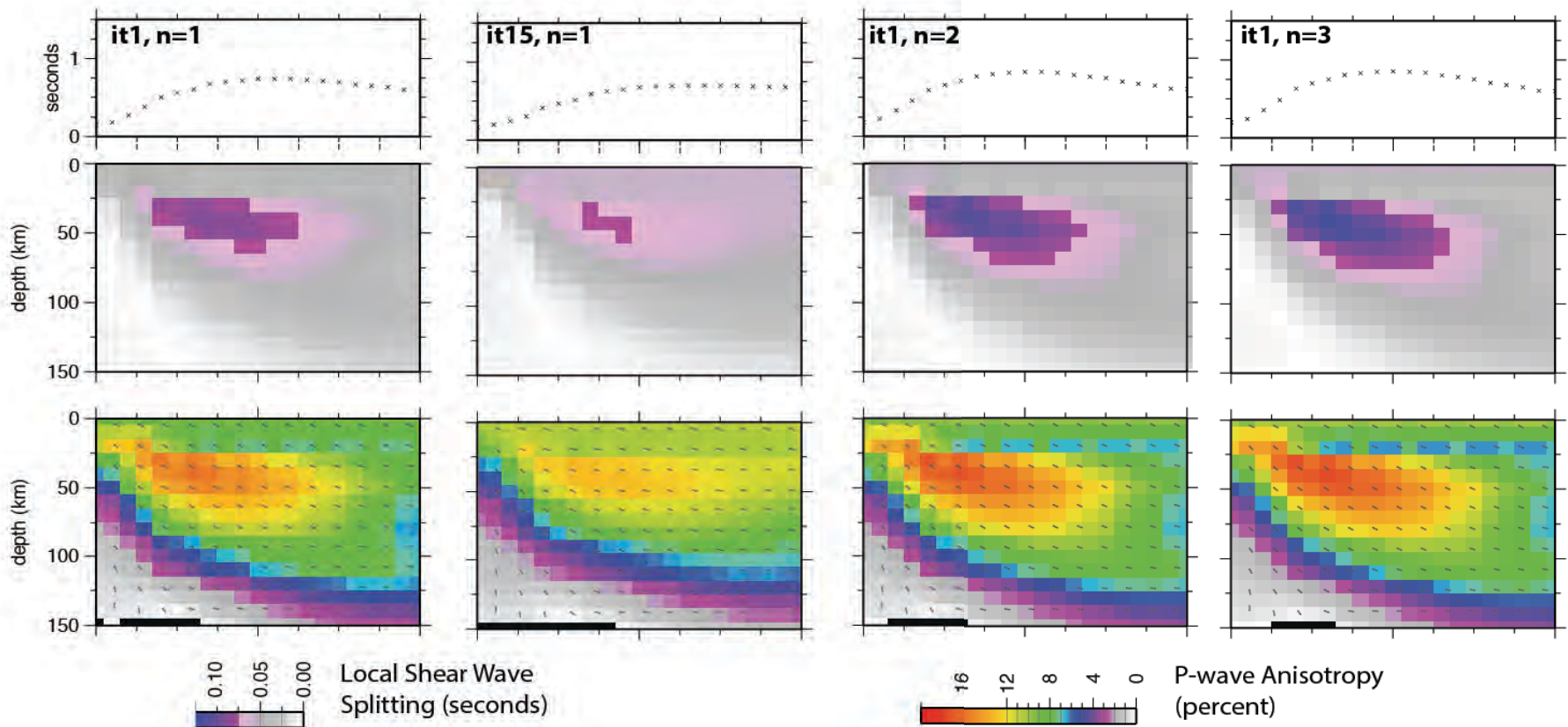
S-wave



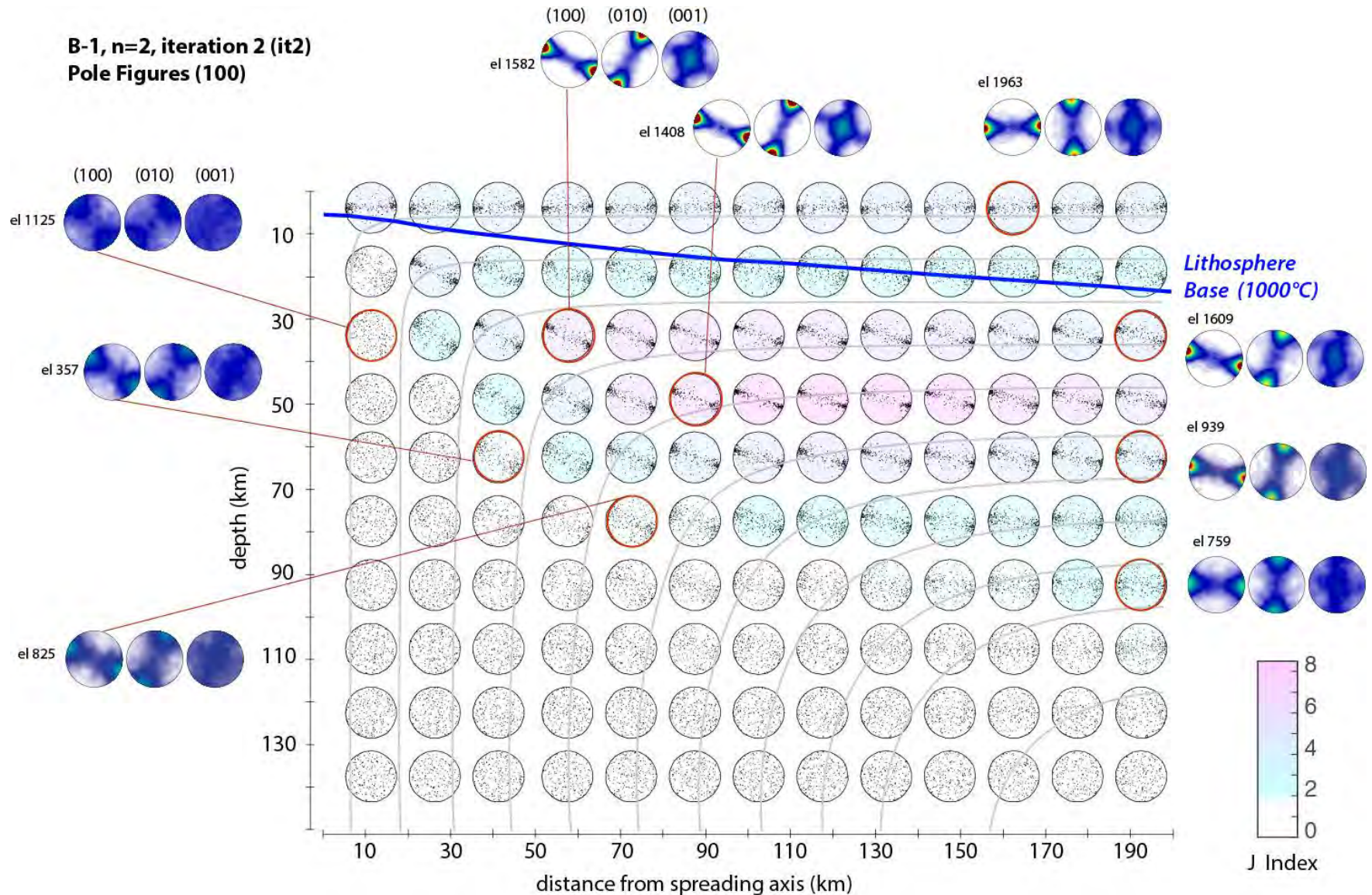
Predicted Seismic Anisotropy

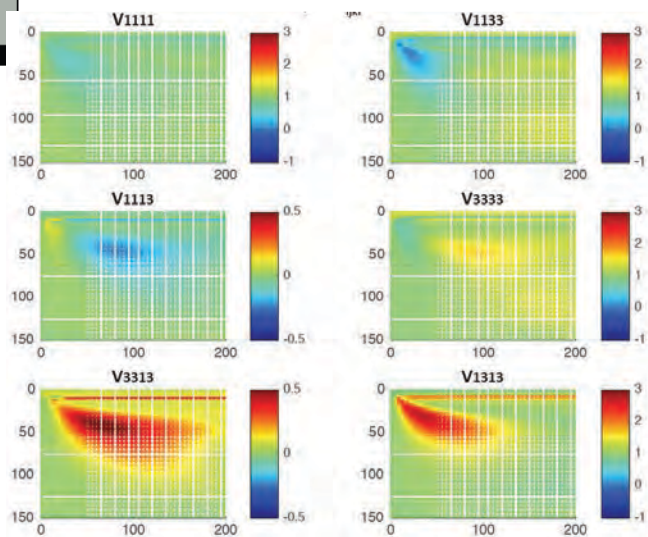
compare linear & power law cases, intermediate coupling

>> anisotropy a few percent stronger in flow 'corner', seismic effects modest



Coupled flow, power law polycrystal

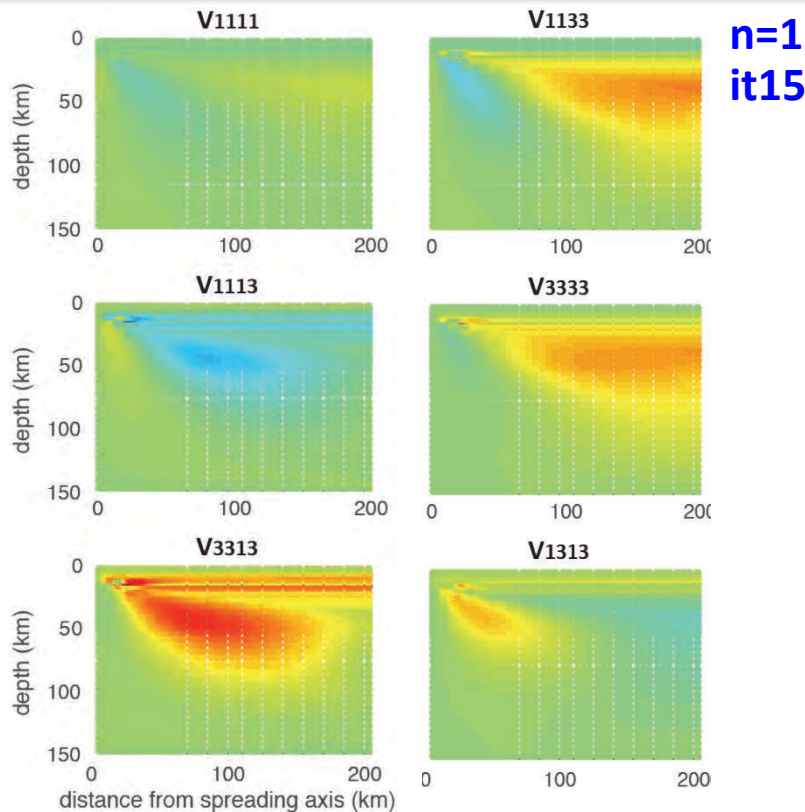




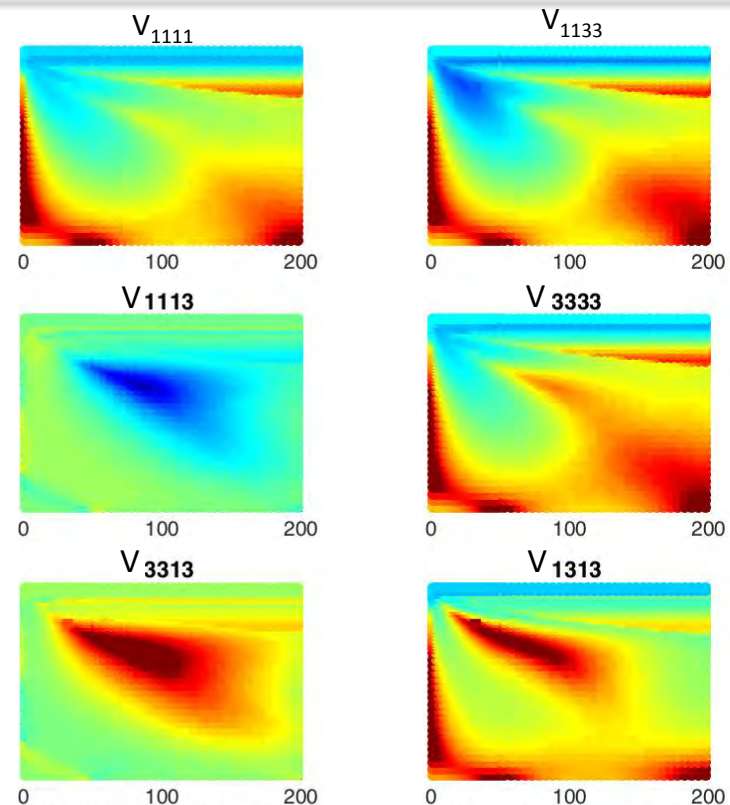
$n=1$
 $it1$

Variation of V_{ijkl} Between Models

*scaled by isotropic value, green \sim isotropic
color scale constant for a given V_{ijkl} component*



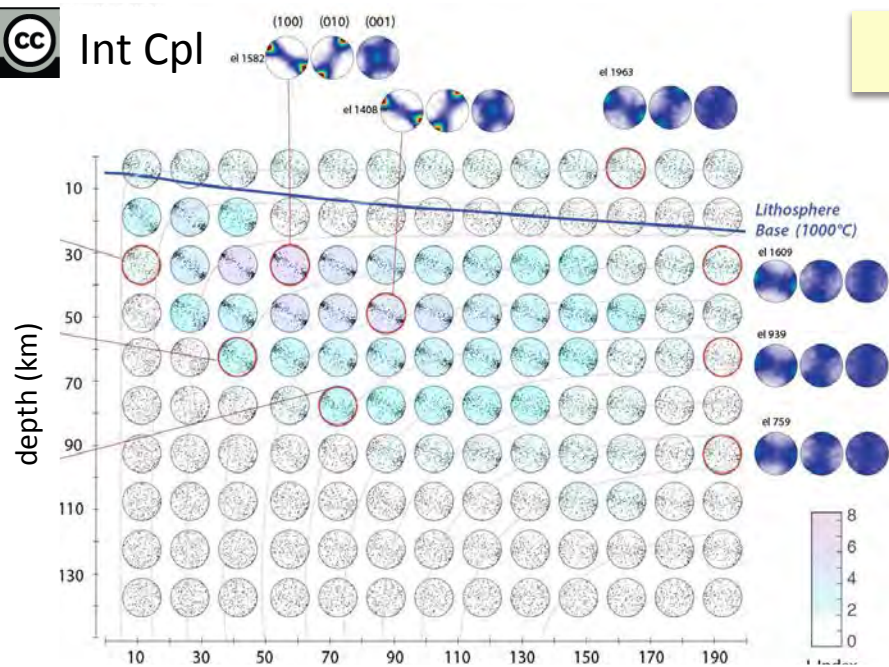
$n=1$
 $it15$



$n=2$
 $it2$

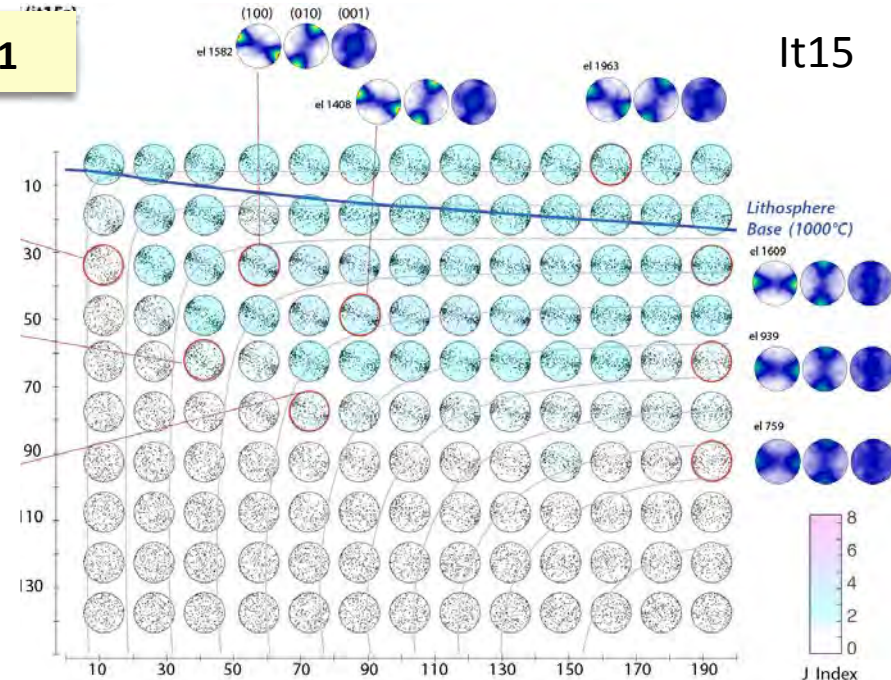


Int Cpl

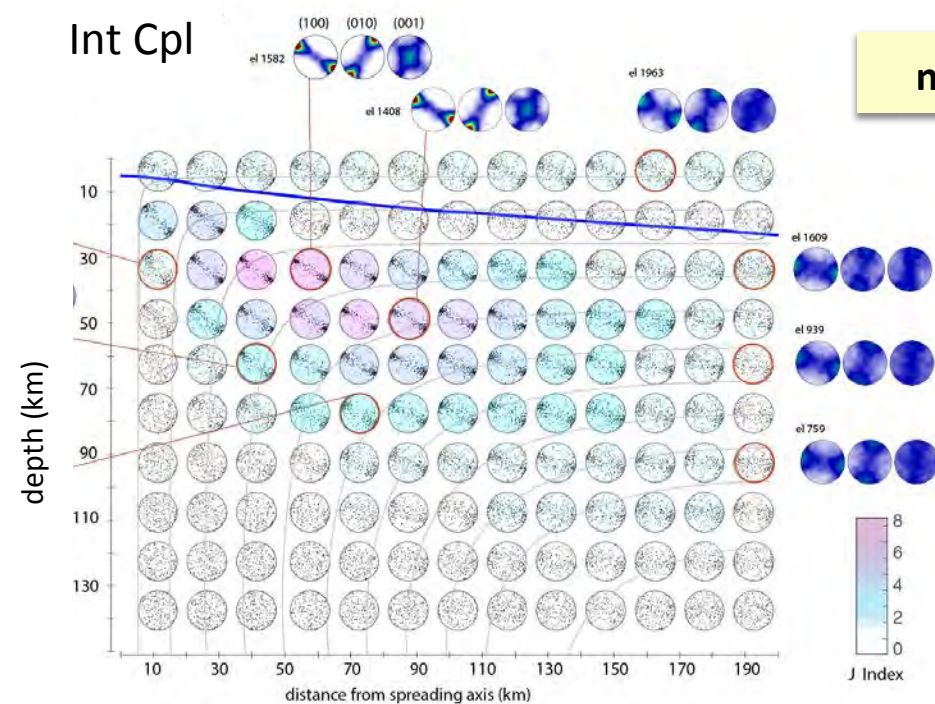


n=1

It15

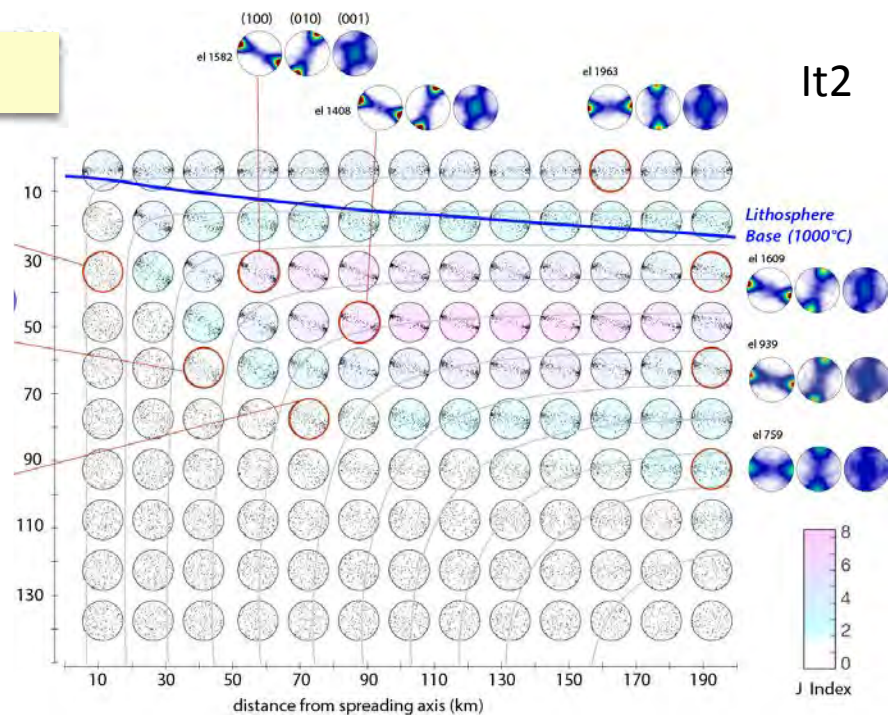


Int Cpl

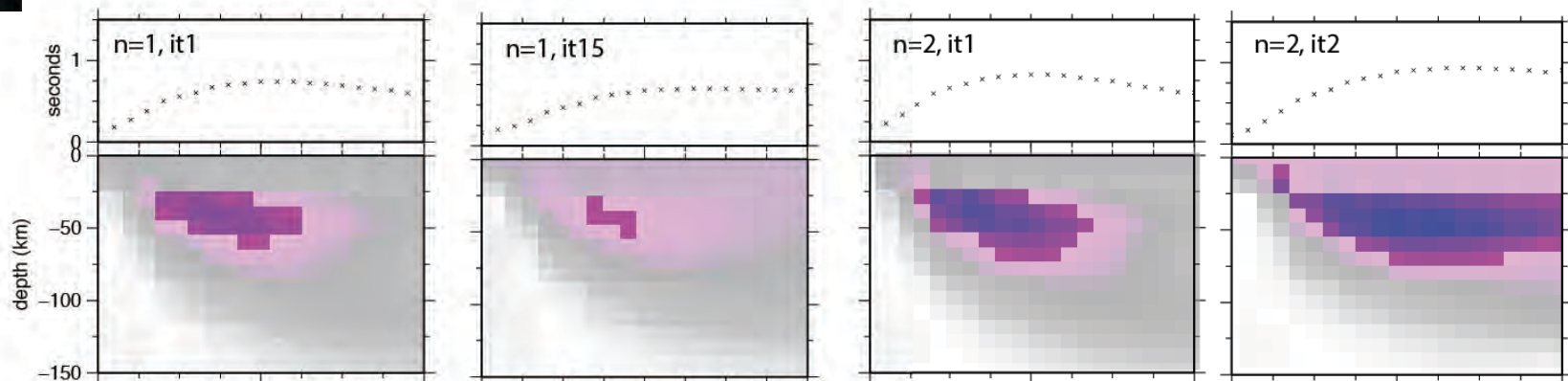


n=2

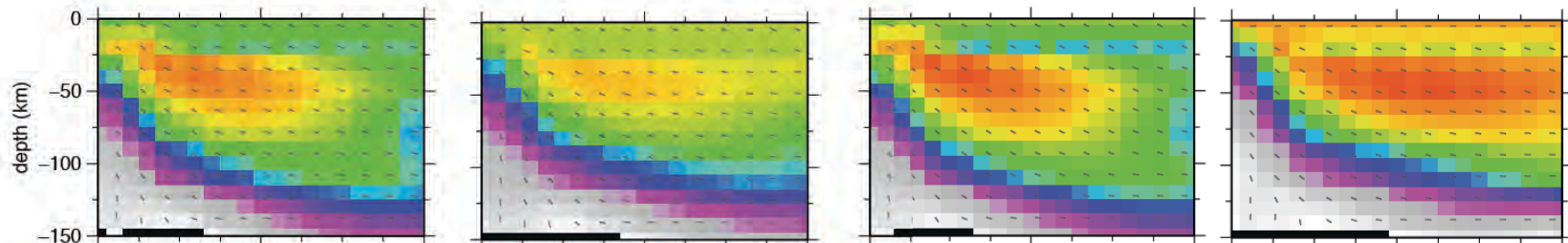
It2



SKS Split

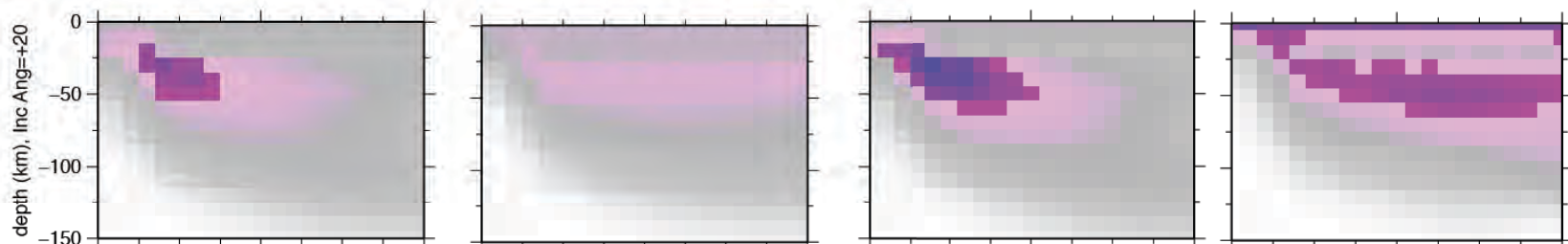


local SKS split

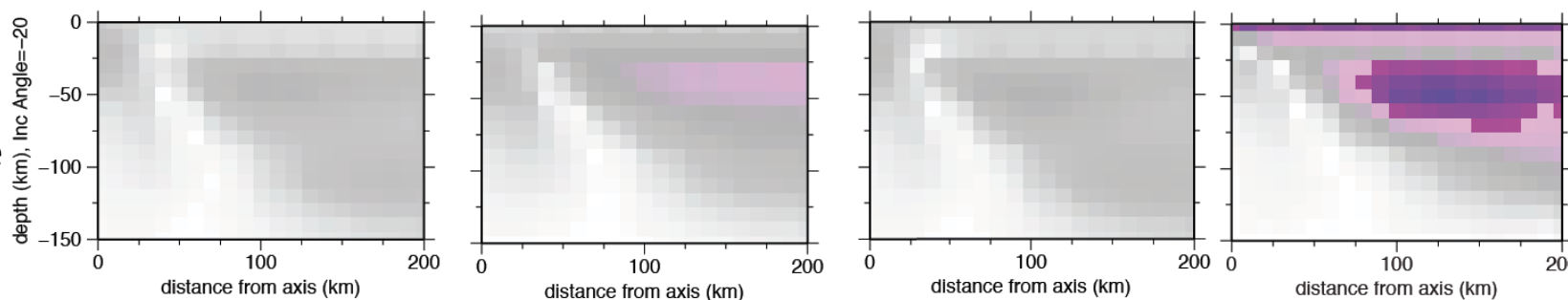


Pwave anisotropy

local split
20° angle
incidence



local split
-20° angle
incidence



Summary

- **Fully-coupled micro-macro scale modeling is possible**

Linear, low resolution runs 10-12 hrs each model iteration— full streamlines (sl), single processor

- **Flow field & anisotropy are affected by CPO rheologic feedback**

Linear case— modest differences relative to isotropic V_{ijkl} intermediate coupling case

Power law case— more notable differences: off axis anisotropy is stronger & extends deeper below lithosphere, increased shallow anisotropy rotates to horizontal, subaxial zone reduction for B-1

Magnitude of difference off axis is seismically detectable (need larger model space to quantify)

- **Computational implications of (more realistic) power law polycrystal behavior**

major increase in convergence time for CPO evolution & viscosity tensor calculation

>> multi-processor, high-speed computing required for further work, update sl from last element

- **Details of axial lithosphere will influence shallow results**

