# Two-sided turbulent boundary layer parameterizations for assessing ocean – atmosphere fluxes

F. Lemarié <sup>1</sup> C. Pelletier <sup>1,2</sup> E. Blayo <sup>1</sup> M.-N. Bouin <sup>3</sup> J.-L. Redelsperger <sup>4</sup>

EGU2020: Sharing Geosciences Online, May 2020

<sup>1</sup>Univ. Grenoble Alpes, Inria, LJK, Grenoble, France

<sup>2</sup>ELIC/TECLIM, UCLouvain, Louvain-la-Neuve, Belgium

<sup>3</sup>Centre de Météo Marine, Météo-France, Brest, France

<sup>4</sup>CNRS, LOPS, IRD, Univ. Brest Occidentale, IFREMER, Brest, France







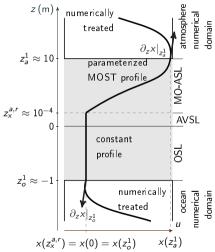






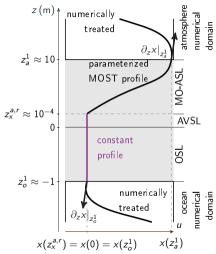






MOST: Monin-Obukhov similarity theory. SL: surface layer. MO-ASL: MOST atmosphere layer. MO-OSL: MOST ocean layer. VSL: viscous sublayer.

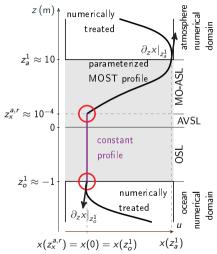
Turbulent air-sea fluxes are determined from atmosphere, MOST-derived bulk formulae, which:



MOST: Monin-Obukhov similarity theory. SL: surface layer. MO-ASL: MOST atmosphere layer. MO-OSL: MOST ocean layer. VSL: viscous sublayer.

Turbulent air-sea fluxes are determined from atmosphere, MOST-derived bulk formulae, which:

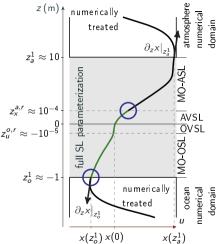
Neglect the ocean and viscous parts of the SL.



MOST: Monin-Obukhov similarity theory. SL: surface layer. MO-ASL: MOST atmosphere layer. MO-OSL: MOST ocean layer. VSL: viscous sublayer.

Turbulent air-sea fluxes are determined from atmosphere, MOST-derived bulk formulae, which:

- Neglect the ocean and viscous parts of the SL.
- ► Lead to numerical irregularities inbetween subparts of the SL.



MOST: Monin-Obukhov similarity theory. SL: surface layer. MO-ASL: MOST atmosphere layer. MO-OSL: MOST ocean layer. VSL: viscous sublayer.

Turbulent air-sea fluxes are determined from atmosphere, MOST-derived bulk formulae, which:

- Neglect the ocean and viscous parts of the SL.
- ► Lead to numerical irregularities inbetween subparts of the SL.

Introducing an idealized framework for extending existing formulae to two-sided versions, ensuring:

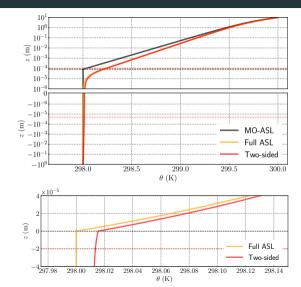
- regularity;
- ► comprehensiveness.

## Comprehensive surface layer parameterization

SL-comprehensive  $\mathbf{u}_h$  and  $\theta_v$  profiles are derived from:

- 1. turbulent flux conservation;
- a choice of roughness length parameterization and viscous profiles;
- 3. transmission conditions (e.g., viscous stress) at z = 0;

Regularity is ensured by design, except at z = 0, which is a physical interface.



Top:  $\theta$  surface layer profiles resulting from different closure types; bottom: zoom around z=0.

Impact on turbulent fluxes via  $(u_a^*, \theta_a^*)$ , from integrating  $u_h$  and  $\theta_v$  profiles on the SL.

$$\frac{\kappa \Delta \theta}{\theta_a^*} = \ln \left( \frac{z_a^1}{z_{\theta}^{a,r}(\mathbf{x}_a^*)} \right) - \psi_h \left( \frac{z_a^1}{L_O^a(\mathbf{x}_a^*)} \right)$$

Analogous for  $\|\mathbf{u_h}\|$ .  $\psi_h$ : stability function;  $L_O^a$ : atm. Obukhov length

Impact on turbulent fluxes via  $(u_a^*, \theta_a^*)$ , from integrating  $\mathbf{u_h}$  and  $\theta_v$  profiles on the SL.

#### New contributions from the viscous sublayers

$$\frac{\kappa \Delta \theta}{\theta_a^*} = \ln \left( \frac{z_a^1}{z_\theta^{a,r}(\mathbf{x}_a^*)} \right) - \psi_h \left( \frac{z_a^1}{L_O^2(\mathbf{x}_a^*)} \right) + (1 + \lambda_\theta) \left( e - 1 \right)$$

Analogous for  $\|\mathbf{u}_{\mathbf{h}}\|$ .  $\psi_{\mathbf{h}}$ : stability function;  $L_O^a$ : atm. Obukhov length;  $\lambda_\theta = \frac{\sqrt{\rho_a}c_p^a}{\sqrt{\rho_o}c_p^o}$ 

Impact on turbulent fluxes via  $(u_a^*, \theta_a^*)$ , from integrating  $\mathbf{u_h}$  and  $\theta_V$  profiles on the SL.

New contributions from the viscous sublayers and the ocean SL:

$$\frac{\kappa \Delta \theta}{\theta_a^*} = \ln \left( \frac{z_a^1}{z_\theta^{a,r}(\mathbf{x}_a^*)} \right) - \psi_h \left( \frac{z_a^1}{L_O^a(\mathbf{x}_a^*)} \right) + (1 + \lambda_\theta) \left( \mathbf{e} - \mathbf{1} \right) + \lambda_\theta \ln \left( \frac{z_o^1}{z_\theta^{o,r}(\mathbf{x}_a^*)} \right) - \lambda_\theta \psi_h \left( \frac{-z_o^1}{L_O^o(\mathbf{x}_o^*)} \right)$$

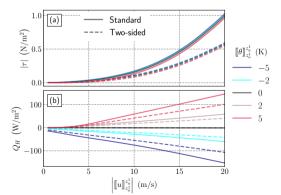
Analogous for  $\|\mathbf{u_h}\|$ .  $\psi_h$ : stability function;  $L_O^a$ : atm. Obukhov length;  $\lambda_\theta = \frac{\sqrt{\rho_a}c_\rho^a}{\sqrt{\rho_o}c_\rho^a}$ ;  $L_O^c$ : ocean Obukhov length.

Impact on turbulent fluxes via  $(u_a^*, \theta_a^*)$ , from integrating  $\mathbf{u_h}$  and  $\theta_V$  profiles on the SL.

New contributions from the viscous sublayers and the ocean SL:

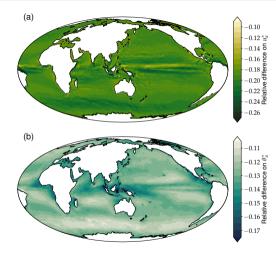
$$\frac{\kappa \Delta \theta}{\theta_a^*} = \ln \left( \frac{z_a^1}{z_\theta^{a,r}(\mathbf{x}_a^*)} \right) - \psi_h \left( \frac{z_a^1}{L_O^a(\mathbf{x}_a^*)} \right) + (1 + \lambda_\theta) \left( \mathbf{e} - \mathbf{1} \right) + \lambda_\theta \ln \left( \frac{z_o^1}{z_\theta^{o,r}(\mathbf{x}_a^*)} \right) - \lambda_\theta \psi_h \left( \frac{-z_o^1}{L_O^o(\mathbf{x}_o^*)} \right)$$

Analogous for  $\|\mathbf{u_h}\|$ .  $\psi_h$ : stability function;  $L_O^a$ : atm. Obukhov length;  $\lambda_{\theta} = \frac{\sqrt{\rho_a c_p^a}}{\sqrt{\rho_O c_p^a}}$ ;  $L_O^o$ : ocean Obukhov length.



- Two-sided closures lead to dampened fluxes.
- ► Results from using one-sided roughness parameterizations in a two-sided context.
- Calls for calibrating bulk formulae anew, taking into account the two-sided closure above.

### **Conclusions**



Time-averaged (year 2006) relative difference on turbulent scales arising from using two-sided bulk closures, using ERA-Interim (atmosphere) and GLORYS2v4 (ocean) near-surface data.

- ► Introduced an idealized framework for extending existing bulk formulae to two-sided versions.
- Adapted to coupled ocean-atmosphere numerical simulations, which use θ(z = −1m) as ocean temperature, yet with bulk closures derived from surface measurements.
- Considerable room for enhancement through retuning and new physics (e.g. radiation penetration, wave-induced surface deformation).