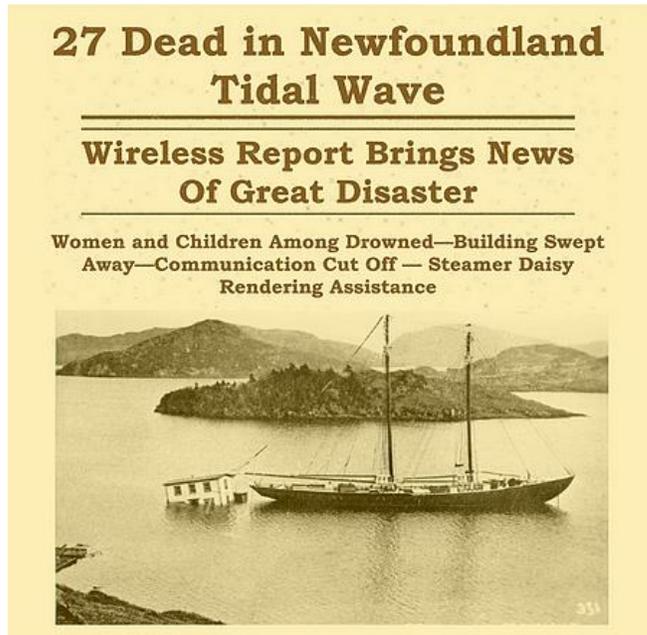


Sediment failure of St. Pierre Slope: new insights of failure mechanisms and slope instability due to the 1929 Grand Banks Earthquake

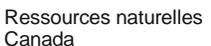
Schulten, I.¹, Mosher D. C.², Piper, D. J. W.²,
Krastel, S.³ and MacKillop, K.²



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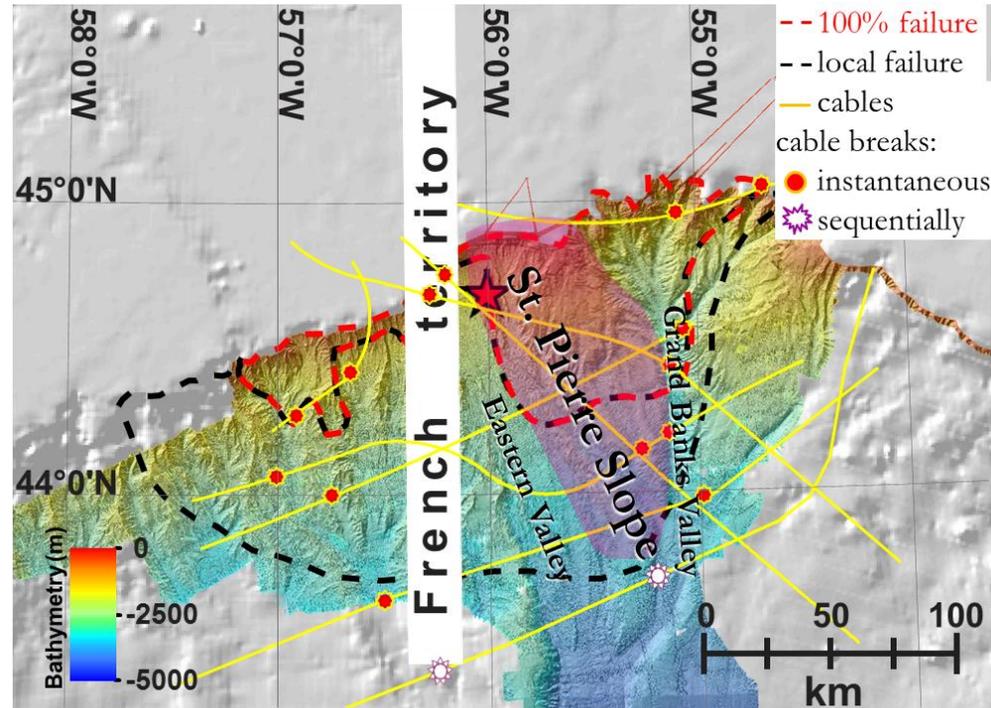


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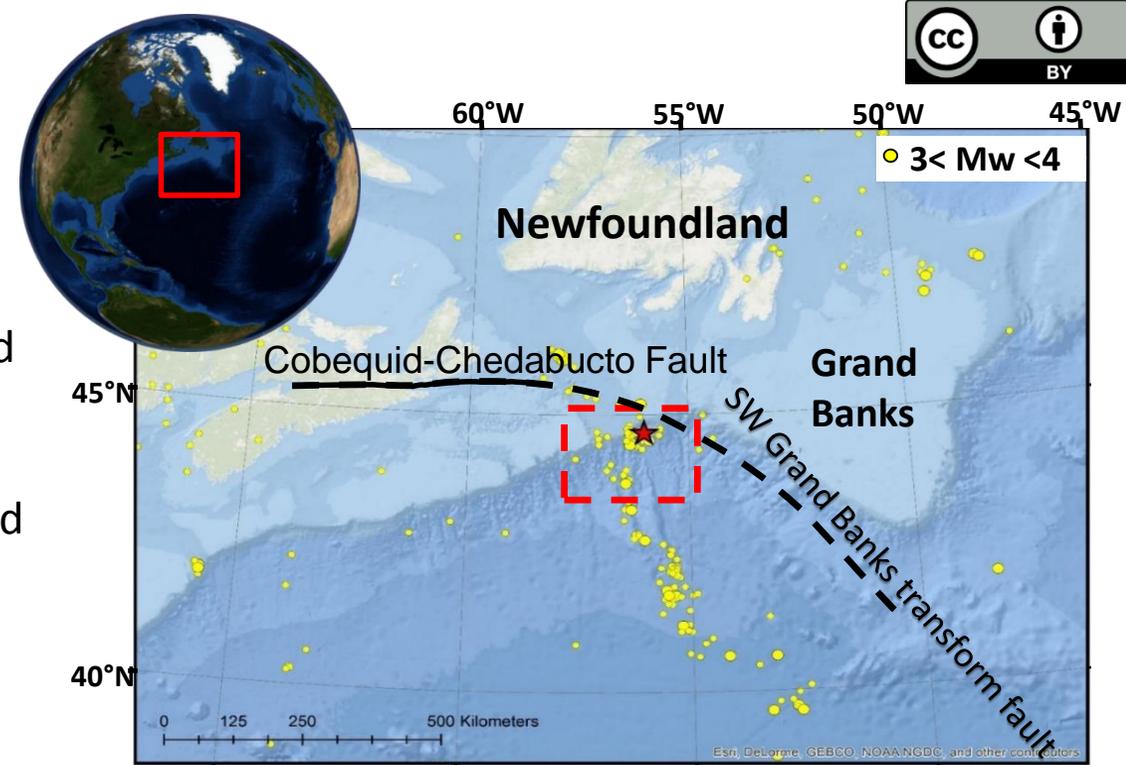


The 1929 event & the St. Pierre Slope

On November 18th 1929 a M_w 7.2 strike-slip earthquake (★; <20 cm of vertical displacement) occurred in ~20 km depth underneath the Laurentian Fan of the southwestern Grand Banks of Newfoundland (Bent, 1995). This earthquake caused a submarine landslide, which led to the first observation of naturally occurring turbidity currents and is one of the few landslides known to have caused a tsunami. The turbidity current broke 12 transatlantic tele-communication cables and the tsunami killed 28 people and destroyed onshore infrastructure, especially on Burin Peninsula of Newfoundland.



Modified from Piper, 2009



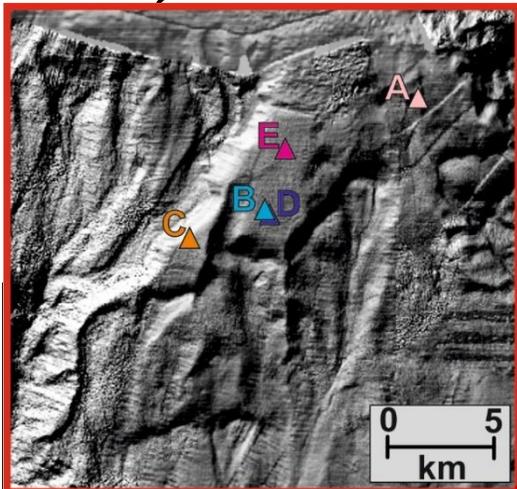
The 1929 submarine landslide is described as follow:

- **widespread, translational + retrogressive sediment failure = <25 m-thick** (Piper et al., 1999; Mosher & Piper, 2007; Schulten et al., 2018)
- **rapid flow transformation** into turbidity currents (Piper et al., 1999)
- **volume estimate: ~100 km³, ~40% entered the turbidity currents** (Piper & Aksu, 1987; McCall, 2006; Schulten et al., 2018)
- **main failure area = St. Pierre Slope (Piper et al., 1999)**
 - numerous shallow escarpments in >730 m water depth (mwd)
 - numerous incised valleys & canyon systems

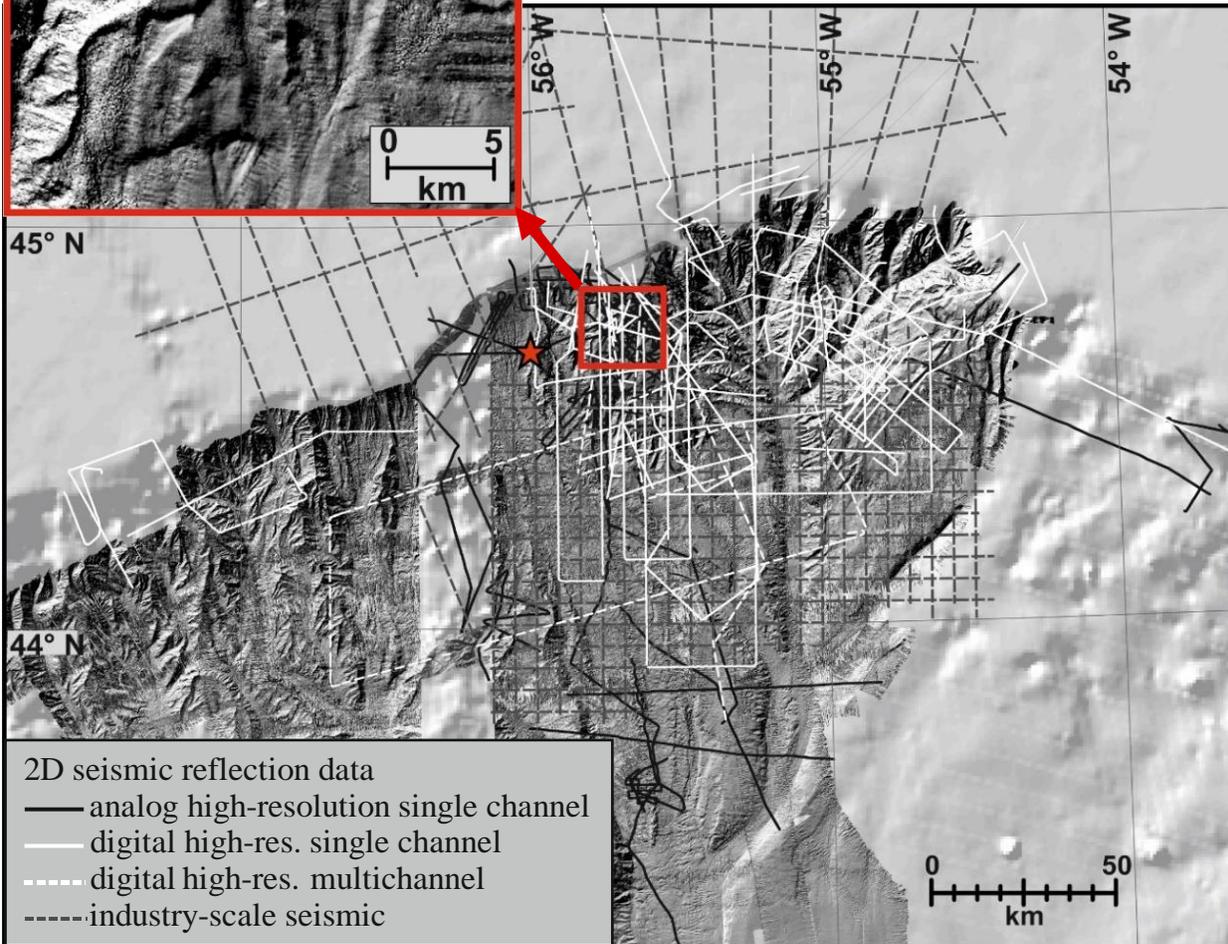
Objective & Methods

Open question: water depth of surficial failure, their thin nature and rapid flow transition contradict what might be expected for a tsunamigenic event

Objective: Need to understand characteristics of initial sediment failure = failure dimensions, kinematics, slope stability



Core locations (A-E), upper St. Pierre Slope



Data source = legacy + newly acquired data (1985-2015):

- multibeam swath bathymetry
- ultra high-resolution seismic data
- 2D seismic reflection data (high-resolution & industry-scale)
- 5 x marine gravity cores from the unfailed part of the slope (~500-730 mwd)

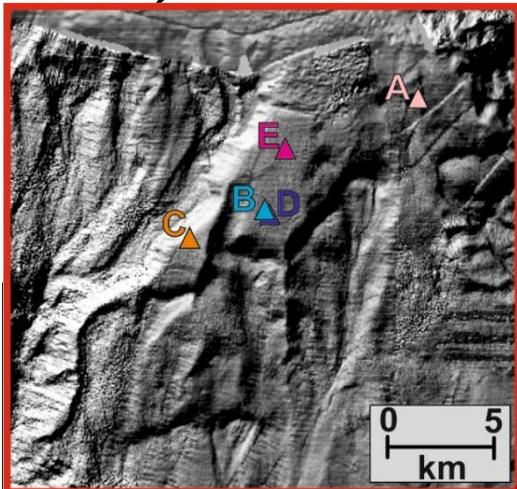
I. Seismic reflection data and multibeam data analysis; published in Schulten et al. (2019)

- establishing a full stratigraphy St. Pierre Slope using results of previous publications
- identification of previously unrecognized sub-bottom structures

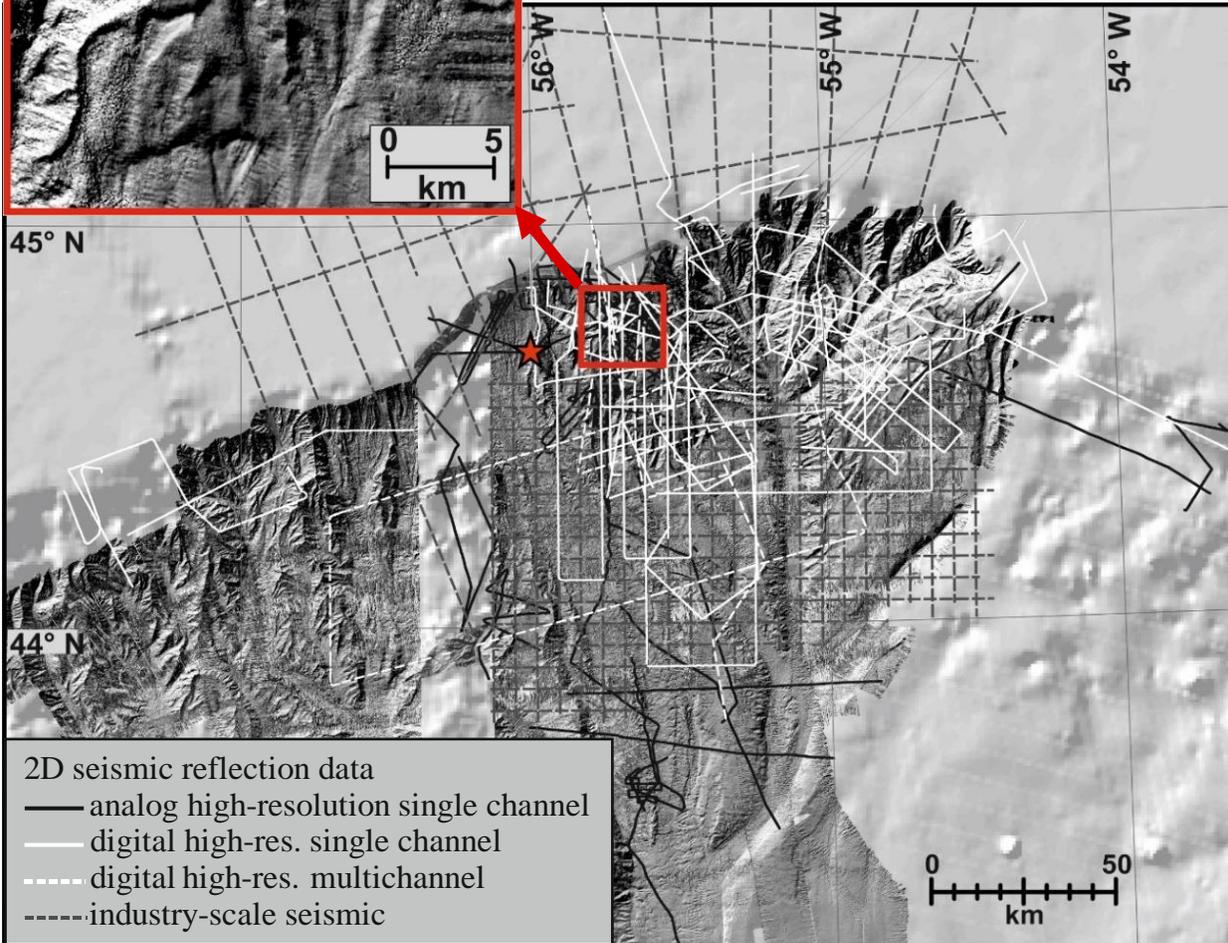
Objective & Methods

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Core locations (A-E), upper St. Pierre Slope



2D seismic reflection data
 — analog high-resolution single channel
 — digital high-res. single channel
 - - - digital high-res. multichannel
 - - - industry-scale seismic

Data source = legacy + newly acquired data (1985-2015):

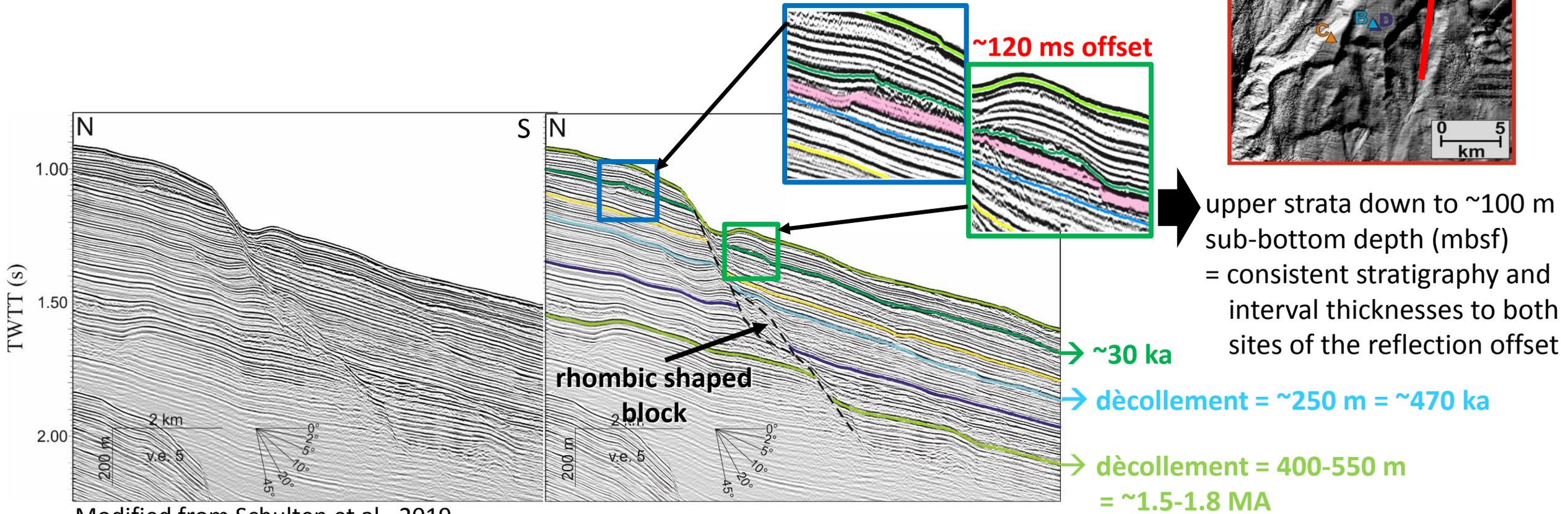
- multibeam swath bathymetry
- ultra high-resolution seismic data
- 2D seismic reflection data (high-resolution & industry-scale)
- 5 x marine gravity cores from the unfailed part of the slope (~500-730 mwd)

II. Geotechnical (consolidation, triaxial, shear strength testing) & static and pseudo-static infinite slope stability analysis

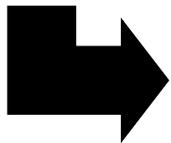
- = sediment cores + sediment slabs (2-550 m-thick)
- FOS for sediment slabs = from normalized shear strength (Su_{NSP} ; triaxial results) + effective stress ($P'_{vo\ trend}$) calculated using an equation of Kominz et al. (2011)
 - PGA to magnitude-distance conversion = equations from Atkinson and Boore (2006, AB2006) and Campbell and Bozorgnia (2008; CB2008)

Results + Interpretation

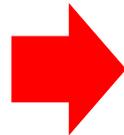
I. Seismic reflection data & multibeam swath bathymetry (Schulten et al., 2019)



Modified from Schulten et al., 2019



at St. Pierre Slope reflection offsets (black dashed line) are evident underneath modern seafloor escarpments down to a depth of ~700 ms or 400-550 m (near the green reflector) (Schulten et al., 2019)

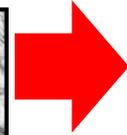
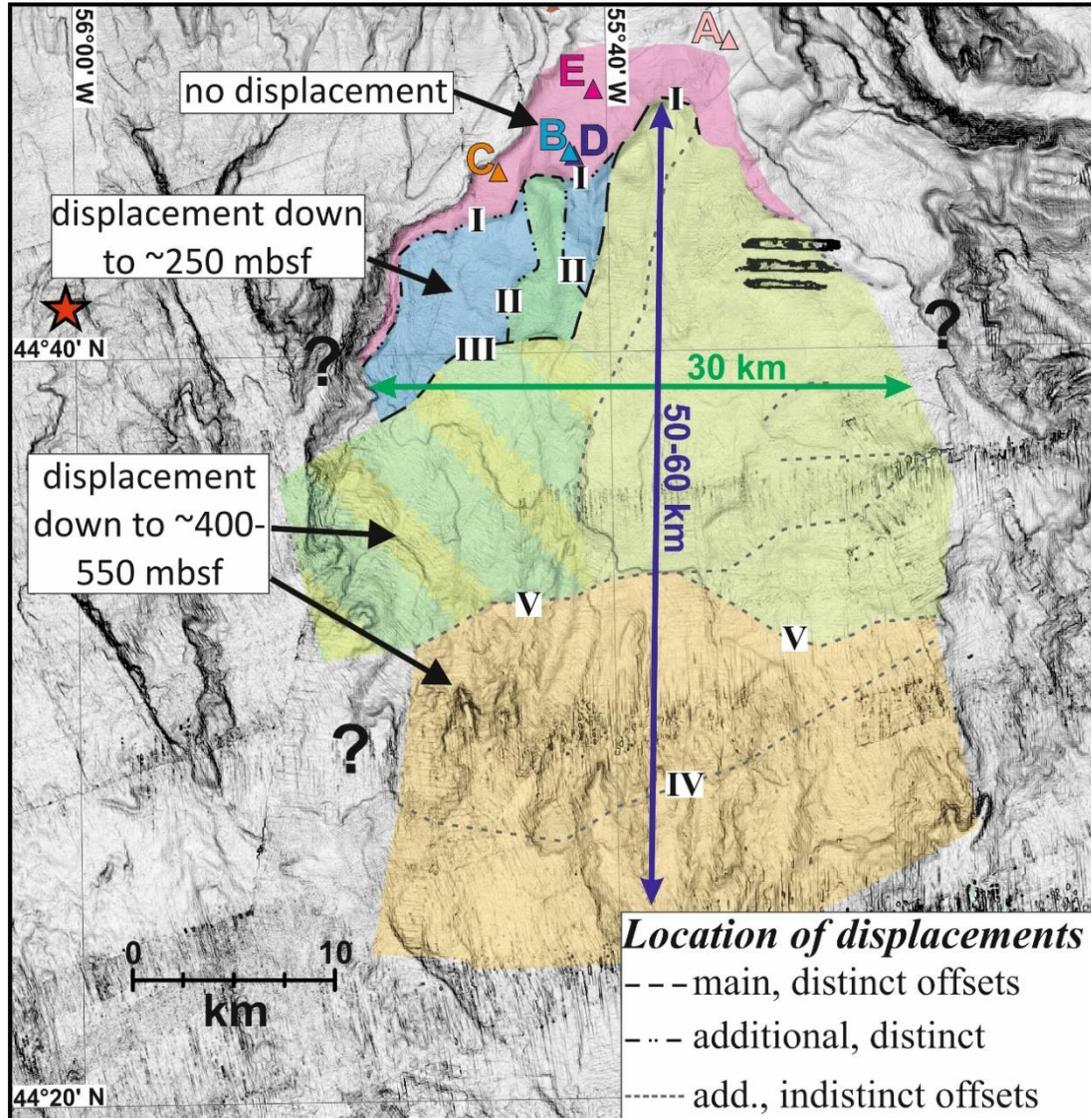


low angle (~17°), normal faults (Schulten et al., 2019):

- ~100 m vertical displacement (Schulten et al., 2019)
- rupture the modern seafloor (Schulten et al., 2018)
- down to different depths within the Quaternary section of the slope (Schulten et al., 2019)

Results + Interpretation

I. Seismic reflection data & multibeam swath bathymetry (Schulten et al., 2019)



faults are part of a massive (~560 km³), complex slump with multiple décollements (250 mbsf & 400-550 mbsf) and slumping towards S & SW (Schulten et al., 2019)



~250 mbsf décollement (light blue horizon) = ~470 ka (MIS 12; Piper et al., 2005)

- regional unconformity = denotes a change in depositional characteristic as a result of shelf-crossing glaciers + increased sedimentation rate
- overlies thick (30-40 m) mass transport deposits (MTD's) (Schulten et al., 2019)

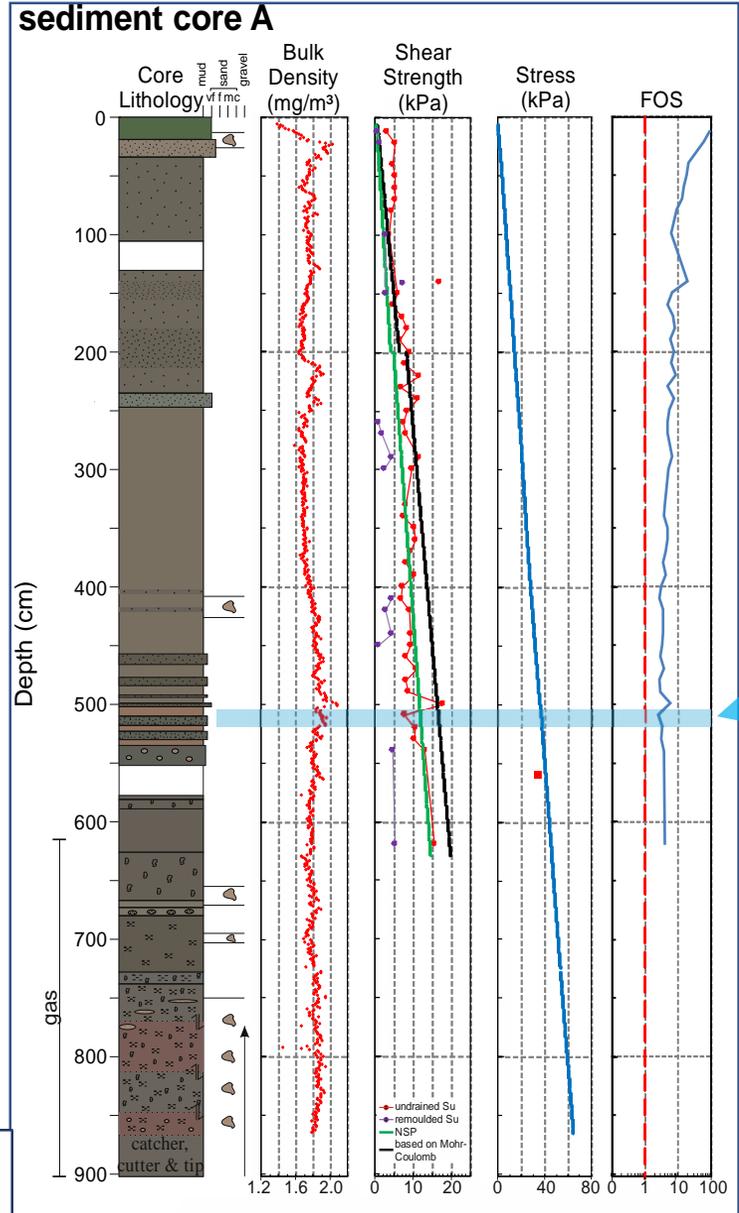
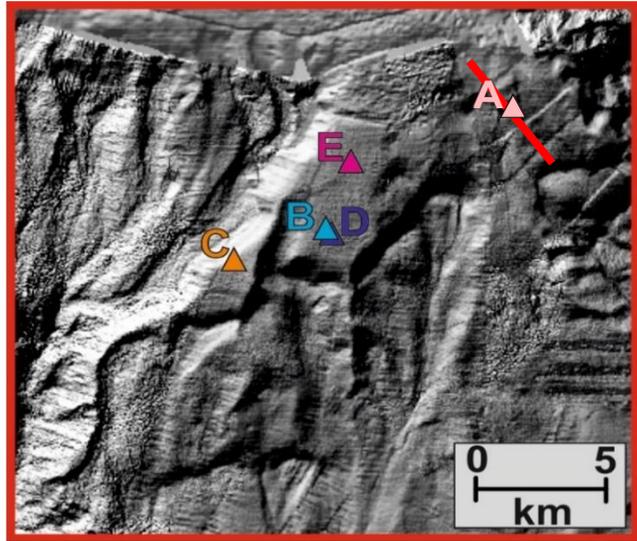


400-550 mbsf décollement (light green to yellow horizon) = ~1.5-1.8 Ma (early Pleistocene; Piper & Normark, 1982)

- overlain by ~40 m-thick MTDs in the shallower part of the slope (Schulten et al., 2019)
- underlain by sediment waves further downslope (Piper et al., 2005; Schulten et al., 2019)

Results + Interpretation

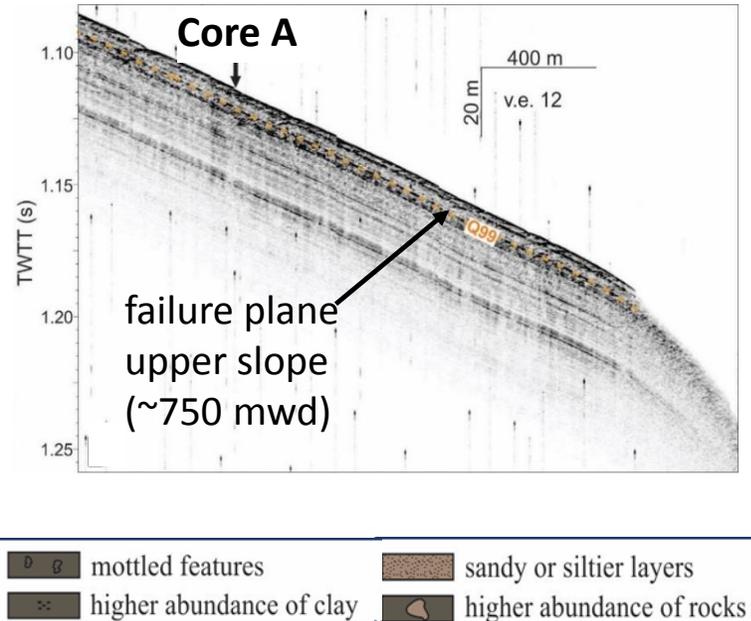
II. Geotechnical analysis & infinite slope stability analysis



- mainly bioturbated, muddy (silt + clay) sediment
 → interbedded sandier or siltier layers are abundant in 400 to 600 cm core depth = MTD's or sandy turbidites
 → gas expansion cracks are evident in >600 cm, capped by the overlying MTD's
- FOS minima = lithological changes between MTD's or sandy turbidites and clay-rich mud that show different shear strengths
- failure plane at the upper St. Pierre Slope in ~10 m depth = core section with gas expansion cracks
- OCR = 0.76-0.89 from 3 to 9 m = normal (NC) to slight underconsolidation (UC)

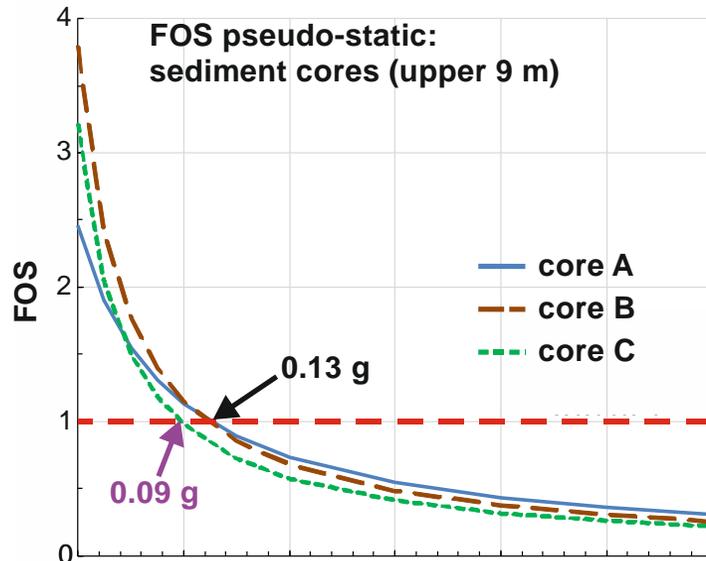
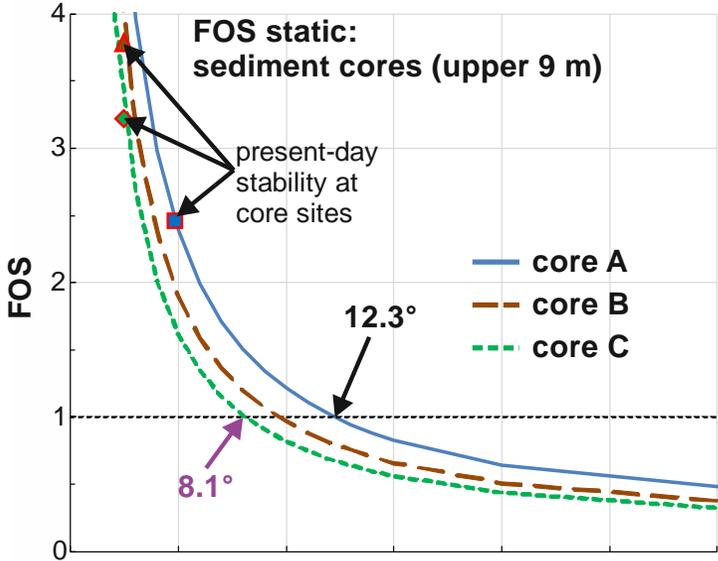
UC as result of excess pore pressure + formation of weak layers due to:

- 1) high sedimentation rates
- 2) rapidly deposited MTD's or sandy turbidites
- 3) presence of gas



Results + Interpretation

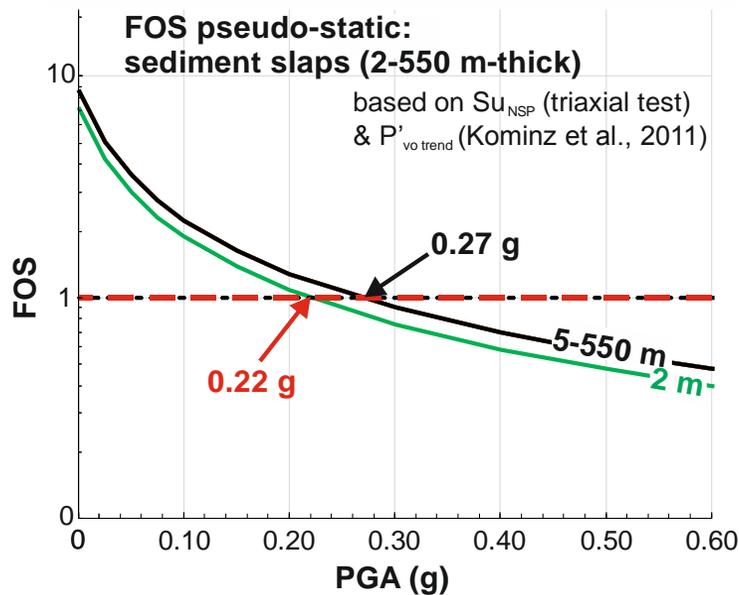
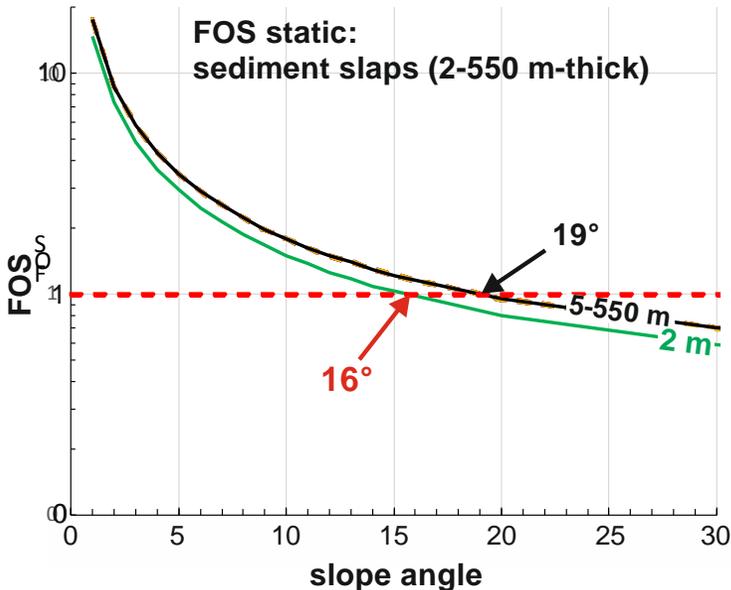
II. Geotechnical analysis & infinite slope stability analysis



➔ **FOS of sediment cores = 8.1° = 0.09 g**

➔ present-day slope angle at St. Pierre Slope = 2-5°, steeper only on canyon walls

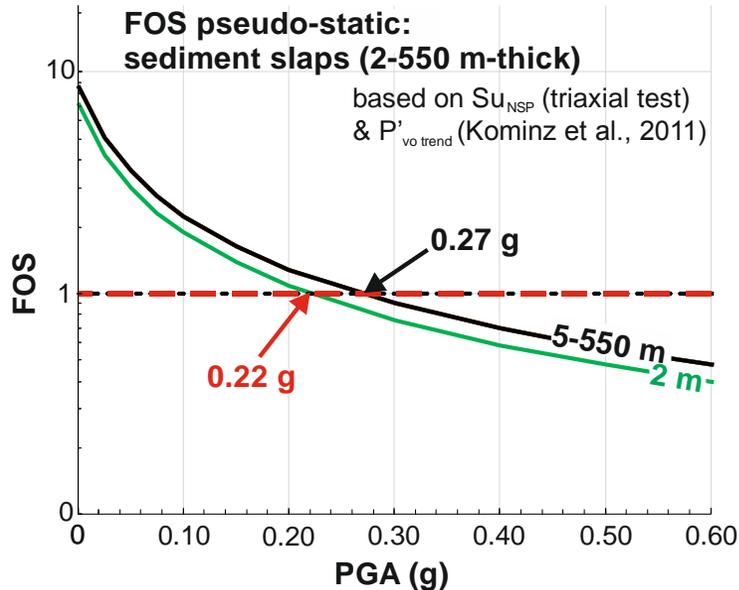
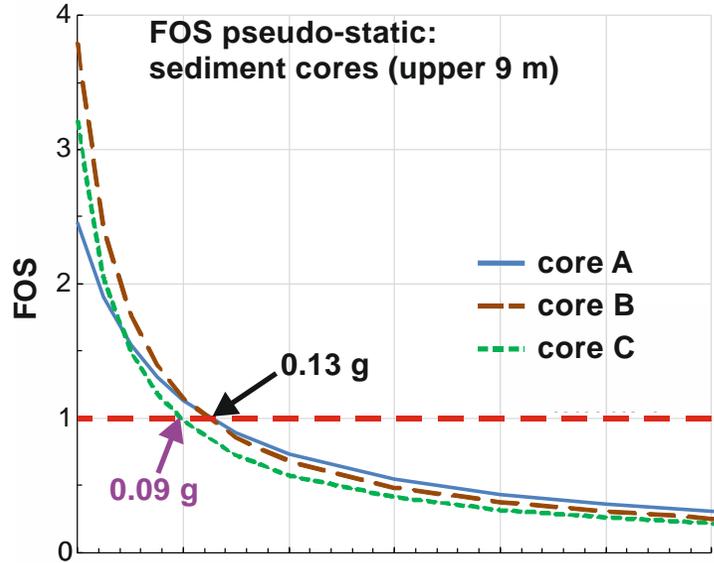
➔ **slope is stable under static and present-day conditions**



➔ **FOS of sediment slabs (2-550 m-thick) = 16° = 0.22 g for a 2 m & 0.27 g for 5-550 m-thick slabs**

Results + Interpretation

II. Geotechnical analysis & infinite slope stability analysis



➔ **PGA of 0.09 g = $M_w > 4.8$, < 5 km distance**
= minimum earthquake loading required to cause slope instability under present-day conditions
= earthquakes past 30 yrs = $M_w < 4$, > 5 km distance

➔ **1929 earthquake = M_w 7.2, ~26 km distance = 0.2 g AB2006 or 0.13 g CB2008:**

sed. cores = failure

core data include shear strength reductions, additional factors are present (e.g. weak layers)

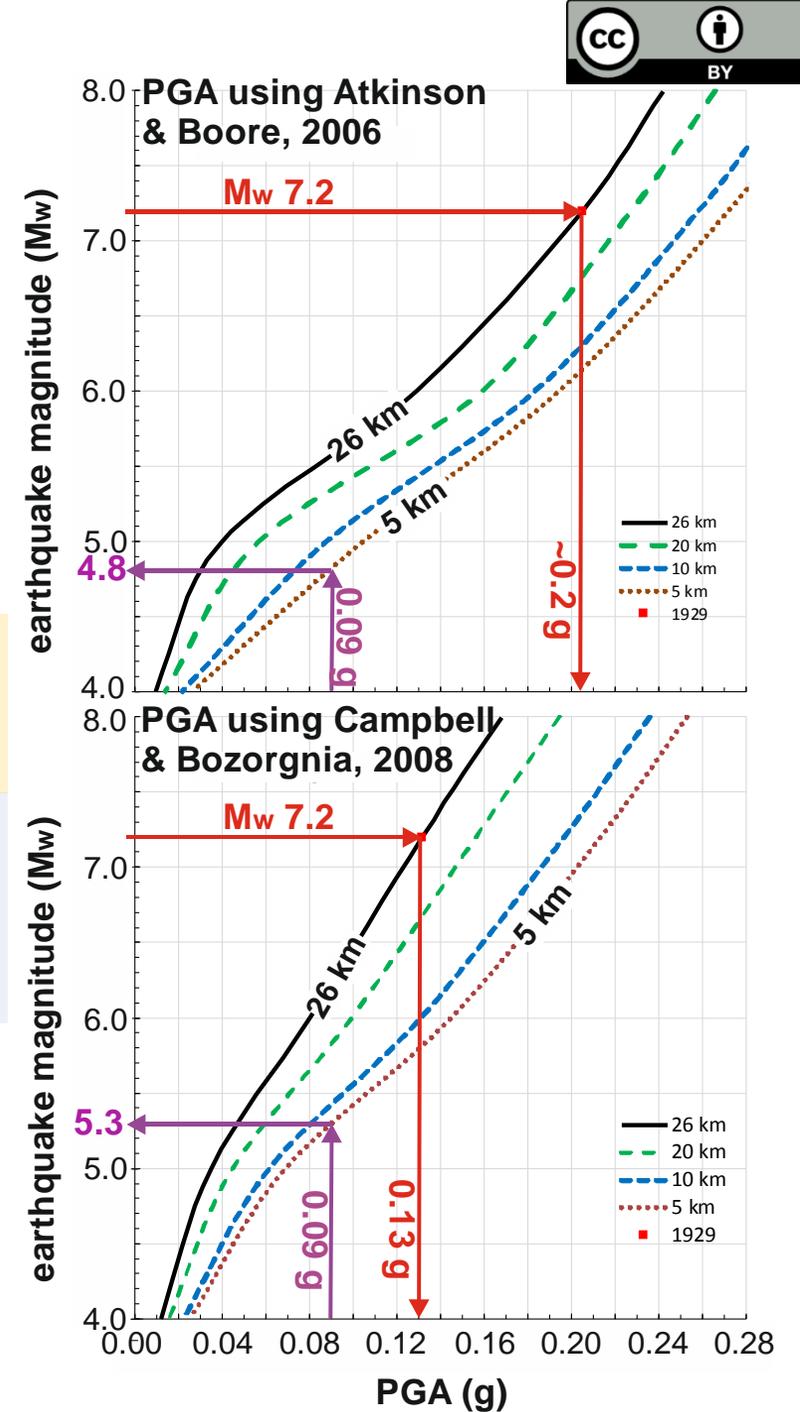
slabs > 10 m = stable

$S_{U_{NSP}} + P'_{vo\ trend}$ (corr. for diagenesis) → slope stability in response to earthquake loading, no additional factors (e.g. weak layers, cyclic loading)



**1929 earthquake: ≠ slump
≠ surficial failures > 10 m**

➔ **additional factors are needed to explain failure in 1929 = presence of weak layers**



Conclusions

- at St. Pierre Slope planar-normal faults occur down to ~550 mbsf and are part of a complex, massive (~560 km³) slump = recent activity, as faults rupture the modern seafloor & height of seafloor escarpments matches the total vertical displacement along the faults (Schulten et al., 2019)
- combination of earthquake loading & pre-conditioning factors is necessary to cause slope instability at St. Pierre Slope
- geomechanical weak layers are a consequence of UC in connection with excess pore pressure
 - ➔ décollements of the slump (250 mbsf & 400-550 mbsf) are associated with MTD's and sediment waves that likely form weak layers susceptible to excess pore pressure development in response to earthquake loading
- 1929 earthquake = displacement of the slump (550 m-thick block) + surficial (<25 m-thick) failures
 - = potential liquifaction within sediment waves + UC in connection with mass deposition and development of excess pore pressure in response to earthquake loading is necessary to explain failure
 - ➔ likely a more effective source for tsunami generation than the translational, shallow (<25 m) failures = tsunami simulation by Løvholt et al. (2018) supports hypothesis that slumping + surficial failures occurred in 1929



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