

On the energy balance behind frictional ruptures

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Motivation





- Earthquake ruptures are driven by the dynamic weakening of frictional strength along crustal faults
- "Lab-earthquake" experiments revealed the crack-like properties of frictional ruptures.

(e.g Xia *et al.,* Science, 2004 Passelègue *et al.,* Science, 2013 Svetlizky *et al.,* Nature, 2014 Rubino *et al.,* Nature Comm., 2017)

This work investigates the rupture energy controlling the propagation of frictional ruptures by analogy with fracture mechanics

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Context

- Shear stress does not drop to zero in the wake of frictional ruptures (unlike shear cracks)
- The energy controlling the rupture dynamics (≡ the **rupture energy** *G_c*) is only a subpart of the frictional dissipation
- Slip-weakening friction model predicts that G_c corresponds to the **breakdown energy** E_{BD} (\equiv excess of frictional dissipation on top of the minimum stress)



> What is the rupture energy for more sophisticated friction models?

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Approach: dynamic simulation of frictional ruptures

• Elastodynamics boundary integral method

Geubelle and Rice, JMPS, 1995 Breitenfeld and Geubelle, IJF, 1998



• Friction law at the interface: two examples (model variables are written in red)

Rate-and-state friction

Dieterich, JGR, 1979 Bar Sinai *et al.*, JGR, 2012 Ruina, JGR, 1983

•
$$\tau(x) = \left(f_0 + A \ln(1 + \frac{v(x)}{v^*}) + B \ln(1 + \frac{\phi(x)}{\phi^*})\right) \sigma_n$$

- φ[s] can be related to the microcontacts area (Baumberger and Caroli, Adv. In Phys., 2006)
- Empirical law representative of rock friction experiments

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Thermal pressurization across a layer of
gouge at the interfaceRice et al., JGR, 2014
Platt et al., JGR, 2014

•
$$\tau(x) = \left(f_0 + A \ln \frac{\dot{\gamma}(x,y)}{\dot{\gamma}^*}\right) (\sigma_n - p(x,y))$$

- *γ* strain rate profile through the layer depending on fluid press. *p* and temp. *T*
- Mature fault zone with a core filled with fluid-saturated gouge

Approach: dynamic simulation of frictional rupture

• Elastodynamics boundary integral method

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- Friction law at the interface: two examples
- Study the near-tip elastic fields to compute the energy released by the rupture
- Compare it to the energy dissipation at the interface during the rupture

Shear-fracture: a well-defined benchmark

- Demonstrate the approach for a shear crack simulated by slip-weakening cohesive law:
- The near-tip singularity can be studied using fracture mechanics (LEFM) predictions for stress *τ* and slip velocity *ν*
- *K* can be directly related to the energy release by unit crack advance *G*

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$$G = \frac{K^2}{2\mu\alpha_s}$$

 $\int \frac{\tau/\tau_c}{G_c}$

Shear-fracture: a well-defined benchmark

- Demonstrate the approach for a shear crack simulated by slip-weakening cohesive law:
- The near-tip singularity can be studied using fracture mechanics (LEFM) predictions for stress *t* and slip velocity *v*
- *K* can be directly related to the energy release by unit crack advance *G*
- The fit of τ and ν allows for estimating *G*
- The rupture energy balance is verified $G = G_c$



Let's now study frictional ruptures

Case 1: Rate-and-state friction

- As τ does not drop to zero, the frictional stress drop $\Delta \tau = \tau - \tau_r$ shall be used in the analogy with LEFM (invoking the linearity of the bulk constitutive law) Palmer and Rice, Proc. Roy. Soc., 1973
- Friction reaches a steady value of τ_r which can be predicted theoretically Barras *et al.*, PRX, 2019
- The breakdown energy overestimates *G* !

$$G < E_{BD}(x) = \int (\tau(x) - \tau_{min}) d\delta(x)$$



Let's now study frictional ruptures

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- Friction reaches a steady value of τ_r which can be predicted theoretically Barras *et al.*, PRX, 2019
- The breakdown energy overestimates *G* !
- A better estimate of *G_c* can be obtained by integrating only the near-tip dissipation



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Let's now study frictional ruptures

Case 2: Thermal pressurization

- Crack-like rupture fronts emerge from intense shear-localization across the gouge layer
- The computed energy release rate G is also much smaller than E_{BD} .
- No obvious value for τ_r as friction keeps weakening after the rupture due to pressurization. Its value is also determined during the fit before computing $\Delta \tau = \tau - \tau_r$



Different friction laws, but generic observations

- Rupture energy $(G_c = G)$ is only a fraction of E_{BD}
- Rupture energy is associated to the rapid weakening of friction immediately in the wake of the rupture
- The subsequent long-term evolution of friction after the rupture does not enter the rupture energy budget and significantly differs along the interface
- A critical displacement δ_c can be associated to this transition

Evolution of E_{BD} during the rupture integrated at different locations along the interface





Thermal pressurization



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 δ_c can be rationalized from the physics behind the two friction laws

Rate-and-state

 δ_c arises when ϕ reaches its minimum, i.e. when the area of underlying microcontact reaches a minimum value after the rupture

Thermal pressurization

 δ_c arises when the most intense shear-localization is observed within the gouge





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Summary and outlook

- The energy balance driving the propagation of frictional rupture is studied for two different types of frictional interface:
 - Rate-and-state interface (rock friction experiments)
 - Fluid-saturated granular layer (representative of fault cores filled with gouge)
- The rupture energy G_c is a small fraction of the total breakdown energy observed during the rupture
- *G_c* corresponds to the near-tip dissipation associated with the rapid drop of frictional stress, whose extend is rationalized using the physics behind each friction law
- The energy partition inherited from slip-weakening friction ($G_c = E_{BD}$) appears to be the exception rather than the rule

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Thank you!

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- Eran Bouchbinder, Michael Aldam (Weizmann Institute of Science)
- Efim A. Brener (Forschungszentrum Jülich)
- Nicolas Brantut (UCL, London)

<u>References</u>

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