Fully-coupled 3D modelling of magmatic dike Propagation – finite pulse release from a point source

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- When does a finite pulse release transition into a dike propagation?
- What is the 3D shape of the buoyant fracture?





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Large time solution

 $t/t_s \approx 1.21 \cdot 10^{11}$

 z/b_*

0.96

 w/W_*

 $1.15 \cdot 10^{-8}$

 x/b_*

 t_{s}^{I}

 At large time we approach the limiting solution of Germanovich *et al.*, (2014) for a finger-like dike propagation. The stable breadth

 $b_* \approx 2^{-8/3} L_b$

is approached in our simulations to about 10%.

 The stable breadth is reached at times significantly larger than a characteristic timescale

$$\frac{[V]}{stab} \approx \frac{2^{15/2}}{3} \left(\frac{V_o E'}{\pi} - K' b_*^{5/2} \right) \frac{\mu' E'^2}{b_* K'^4}$$

Our simulations last up to $t \approx t_{stab}^{[V]} \cdot 10^3$.



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Additional slides and Bibliography





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Further analysis

- Analysing the pressure profile (pressure gradient) and fluid flow inside the fracture to find the solutions of equilibrium shapes (e.g. analytical definition of the birth of dike propagation).
- Arrest is defined geometrically for now. We seek another definition in function of fluid flow.



Dimensionless net pressure profile inside the fracture. The profile is constant along the breadth (along x). The head has a linear gradient along the vertical direction (z) as described in Germanovich et al., (2014). The normalized pressure gradient in the head found was approximately 0.25, which corresponds to a static solution inside the head. We recover this factor in our simulations up to 2% for dike propagation and exactly for fractures without buoyant propagation.



Normalized net pressure inside the fracture. For the black Simulations propagation stopped because equilibrium was reached. For the blue simulation some fluid flow remained allowing for buoyant propagation. Inset is a zoom on the not fully stabilized part.

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Extension of the current work

- Focus on non-viscous shut-in.
- We expect a family of solutions to emerge in function of three dimensionless parameters

 $L_b/R_s, \ \mathcal{K}_s, \ L_b/R_a$

with R_s the radius at shut-in and \mathcal{K}_s the dimensionless toughness at shut-in.

 Different combinations of those parameters may lead to a complicated parametric space.



Material parameters

 Alternative material parameters are defined following Detournay, (2016) (prime parameters) and Germanovich et al., (2014) (bar parameters)

$$E' = \frac{E}{1 - \nu^2}, \quad K' = 4\sqrt{\frac{2}{\pi}}K_{Ic}, \quad \mu' = 12\mu$$
$$\bar{K} = \frac{1}{4}K', \ \bar{E} = \frac{1}{\pi}E', \ \bar{\mu} = \frac{\pi^2}{12}\mu'$$

The scales used are the ones defined in Germanovich et al., (2014)

$$b_* \approx 2^{-8/3} L_b, \ W = \frac{\bar{K}\sqrt{b_*}}{\bar{E}}, \ P = \frac{\bar{K}}{\sqrt{b_*}}$$



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