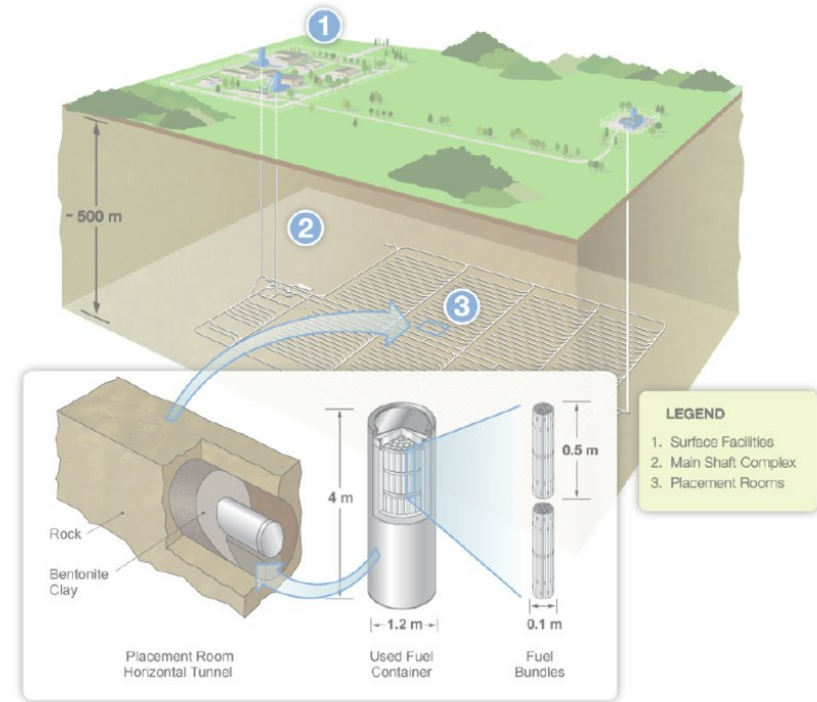


# Near field evolution of a spent fuel repository in an argillaceous rock formation and impact on radionuclide migration

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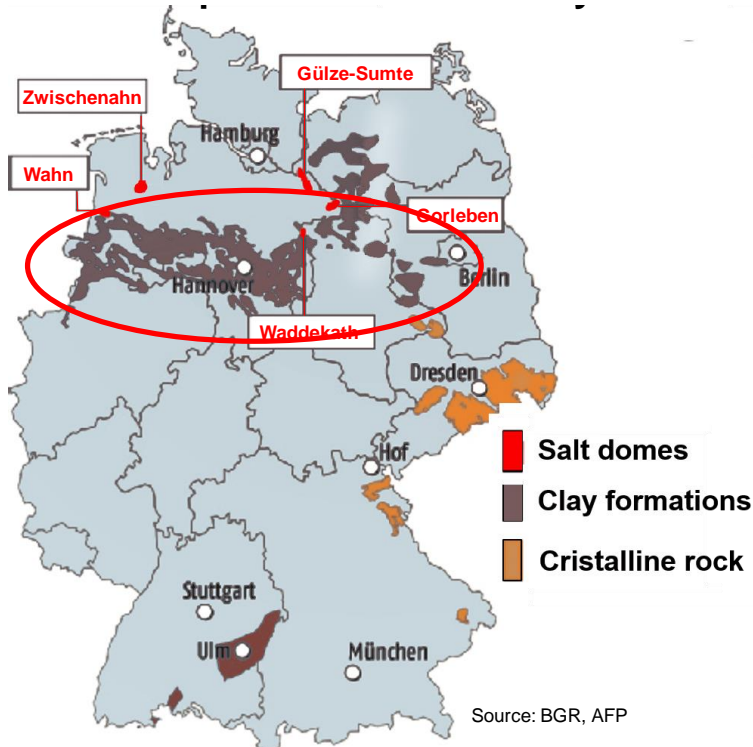
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02.05.2020



# Introduction

## Clay formations in Germany



### North German Basins:

- Risk of deep glacial trench formation
  - ➔ **Emplacement depth ~ 600-700 m**  
(Extended mine construction/lining required)
- Geological formation:  
Lower cretaceous, upper jurassic

# Introduction

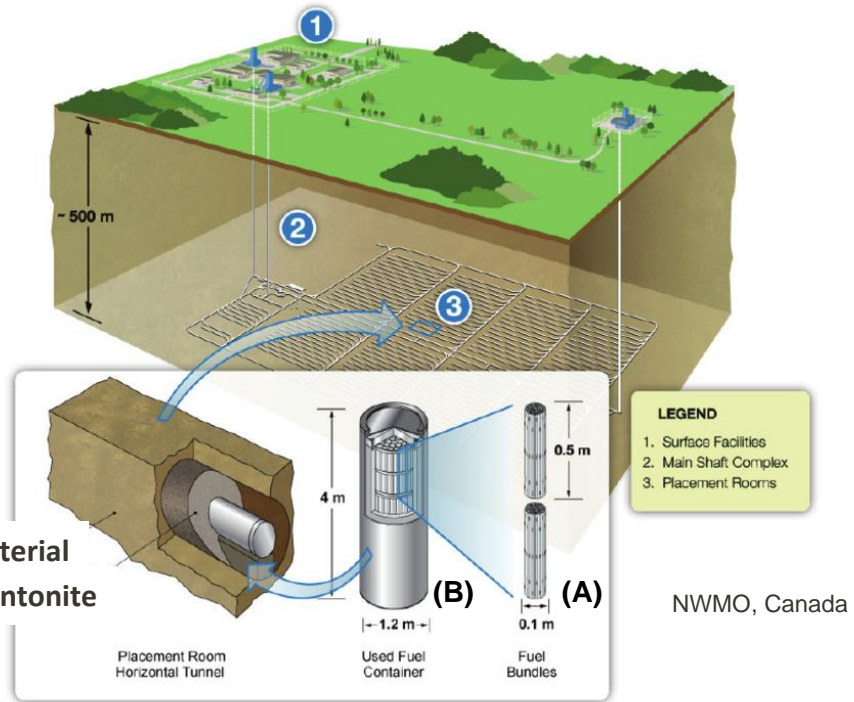
## Repository concept in Clayrock for Spent Nuclear Fuel

### – Multibarrier system

- A) SNF (Spent Nuclear Fuel)
- B) the steel container (Pollux 10)
- C) bentonite (MX-80)
- D) cement plug (Low pH concrete)
- E) cement liner (OPC)
- F) surrounding clay rock (North Germany)



Radionuclide migration



# Reactive solute transport

## Numerical concept

Total mass balance of water and chemical species in variable saturated porous media

$$\omega \frac{\partial c_i}{\partial t} = -\psi \mathbf{q}_l \cdot \nabla c_i + \nabla \cdot (\psi \mathbf{D}_l \cdot \nabla c_i) - c_i \nabla \cdot (\rho_l \mathbf{D}_l \nabla \omega_l^w) - f_{ext}^w c_i + f_{ext}^w c_i^* + \omega r_{eq} + \omega r_{kin}$$

$$\mathbf{q}_l = 0$$

**Diffusion**

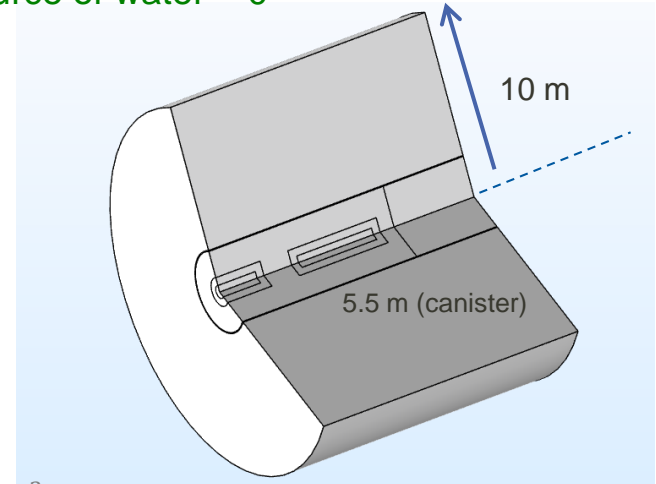
$$\nabla \omega_l^w = 0 \quad \text{Source of water} = 0$$

Advection

$$\mathbf{D}_l = \mathbf{D}_{disp} + \mathbf{D}_{dif} = \phi S_l D_s \tau = \phi D_s \tau = \phi 1 \cdot 10^{-9} \tau$$

$$\omega = \phi S_l \rho_l \omega_l^w = \rho_l \phi$$

$$\psi = \rho_l \omega_l^w$$



$\phi$ : porosity [ $m^3 m^{-3}$ ]  $S_l$ : liquid saturation [ $m^3 m^{-3}$ ]  $\rho_l$ : liquid density [ $kg m^{-3}$ ]

# Geochemistry

## Nuclear waste (Radionuclide inventory)

**55 GWd/tHM** burn-up after **50 years** in PWR (UO<sub>2</sub> + MOX)

(Gigawatts-day /tonnes)

Initially: UO<sub>2</sub> (matrix): Activity:  $7.74 \times 10^{15}$  Bq/tHM

Max. [ ]<sub>aq</sub>

	Half life (a)	Act. (Bq/tHM)	Mass (g/tHM)	Redox state	Key Chem. Parameters	Solub. (mol/Kgw)
<sup>243</sup> Am	7 370	$1.71 \times 10^{12}$	$2.32 \times 10^2$	+III	pH, HCO <sub>3</sub> <sup>-</sup>	$7.88 \times 10^{-6}$
<sup>230</sup> Th	75 380	$1.07 \times 10^9$	1.40	+IV	HCO <sub>3</sub> <sup>-</sup>	$3.50 \times 10^{-9}$
<sup>238</sup> U	$4.468 \times 10^6$	$1.14 \times 10^{10}$	$9.17 \times 10^5$	+IV, +VI	HCO <sub>3</sub> <sup>-</sup> , Eh	$3.79 \times 10^{-9}$
<sup>237</sup> Np	$2.144 \times 10^6$	$6.18 \times 10^{10}$	$2.37 \times 10^3$	+IV,	HCO <sub>3</sub> <sup>-</sup>	$1.01 \times 10^{-9}$
<sup>242</sup> Pu	373 300	$1.49 \times 10^{11}$	$1.02 \times 10^3$	+III, +IV, +V	pH, HCO <sub>3</sub> <sup>-</sup> , Eh	$1.91 \times 10^{-9}$
<sup>99</sup> Tc	211 000	$8.01 \times 10^{11}$	$1.27 \times 10^3$	+IV, +VII	Eh	?

# Geochemistry

## Pore water compositions

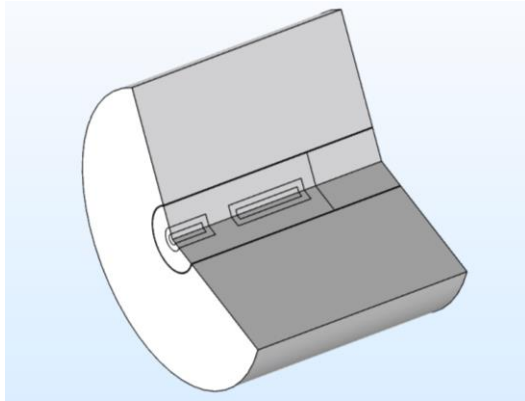
	Host rock	Bentonite	OPC Cement	Low pH concrete	Processes
Na	3.70	2.12	$5.45 \times 10^{-10}$	$1.91 \times 10^{-2}$	Exchange
K	$5.44 \times 10^{-3}$	$8.91 \times 10^{-2}$	$1.25 \times 10^{-9}$	$3.42 \times 10^{-2}$	Exchange
Ca	0.23	0.93	$2.76 \times 10^{-7}$	$5.24 \times 10^{-3}$	Exchange/precip/dissolu
Cl	4.22	4.22	$1.00 \times 10^{-9}$	$1.00 \times 10^{-10}$	--
SO <sub>4</sub>	$2.59 \times 10^{-2}$	$1.89 \times 10^{-2}$	$5.01 \times 10^{-10}$	$3.05 \times 10^{-2}$	Precipitation/dissolu
Si	$1.80 \times 10^{-4}$	$1.80 \times 10^{-4}$	$2.02 \times 10^{-3}$	$2.02 \times 10^{-3}$	Precipitation/dissolu
Al	$4.99 \times 10^{-9}$	$4.99 \times 10^{-9}$	$1.44 \times 10^{-4}$	$1.44 \times 10^{-4}$	Precipitation/dissolu
Fe <sub>Total</sub>	$4.98 \times 10^{-5}$	$4.98 \times 10^{-5}$	$5.45 \times 10^{-8}$	$5.45 \times 10^{-8}$	Precipitation/dissolu
Mg	0.114	0.114	$3.73 \times 10^{-7}$	$3.73 \times 10^{-7}$	Exchange/precip/dissolu
CO <sub>3</sub>	$8.92 \times 10^{-5}$	$4.34 \times 10^{-5}$	$1.50 \times 10^{-5}$	$1.50 \times 10^{-5}$	Precipitation/dissolu
Eh (mV)	-111 (Fe(II)/Fe(III))	-111 (Fe(II)/Fe(III))	-27 mV	-27 mV	Precipitation/dissolu
pH	7.77	8.1	13.31	10.68	Precipitation/dissolu/surf

# Modelling results

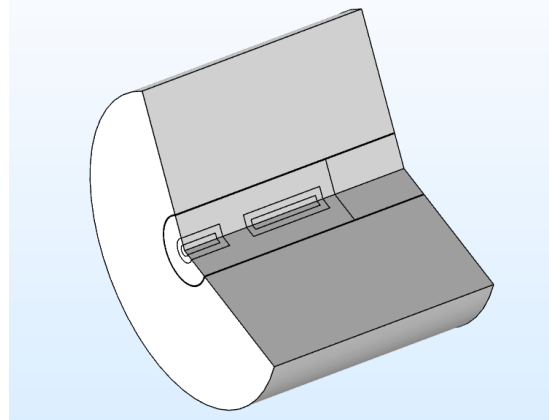
## Canister Corrosion



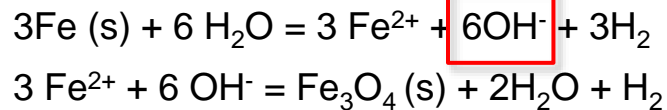
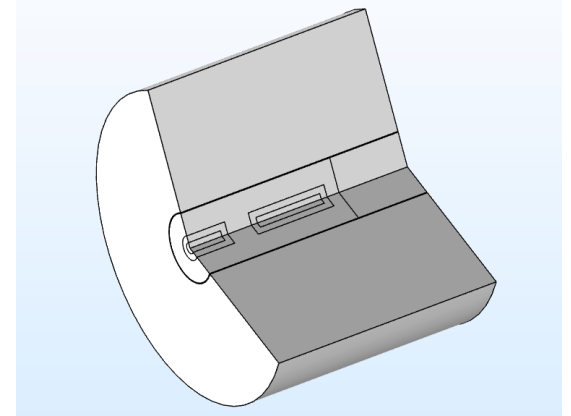
100 years



1 000 years



10 000 years



$$r_n = M_w m k_n A$$

0.005  $\mu\text{m yr}^{-1}$

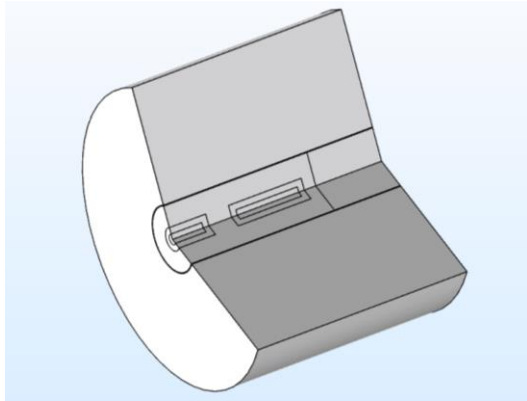
$r_n$ : reaction rate [ $\text{mol s}^{-1}$ ]

# Modelling results

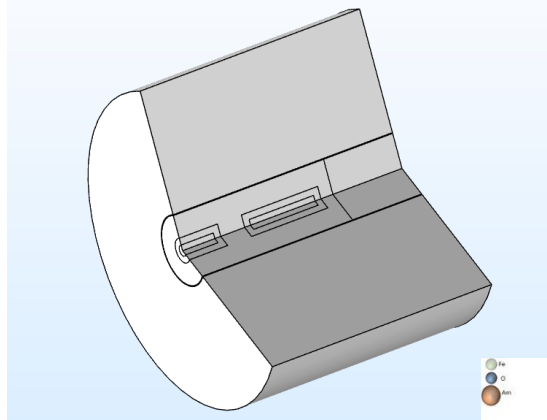
## Transport of a reactive tracer ( $^{243}\text{Am}$ )



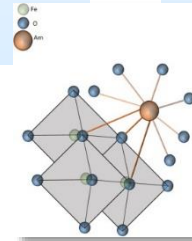
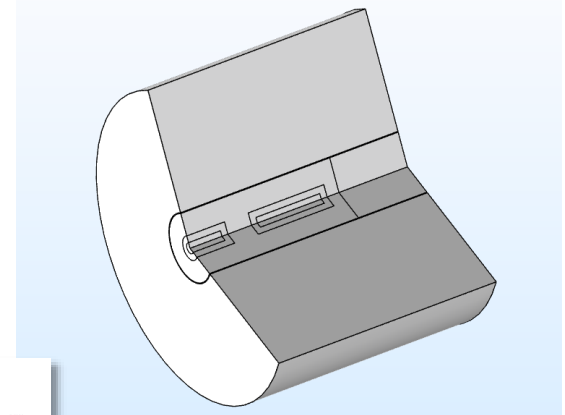
100 years



1 000 years



10 000 years



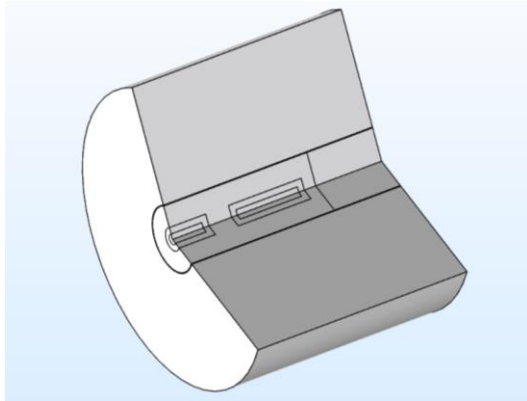


# Modelling results

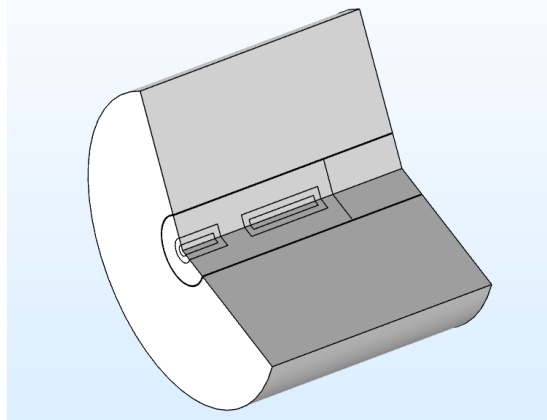
## Transport of a non-reactive tracer ( $^{36}\text{Cl}^-$ )

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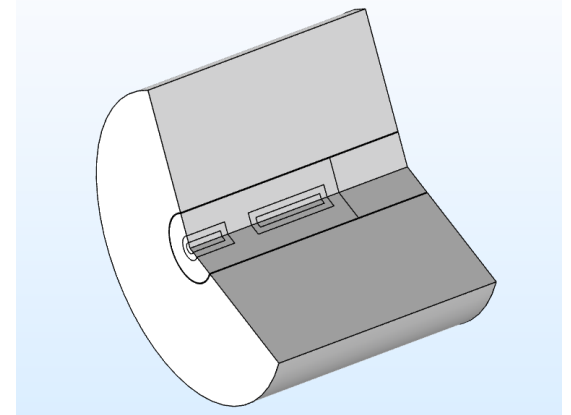
100 years



1 000 years



10 000 year

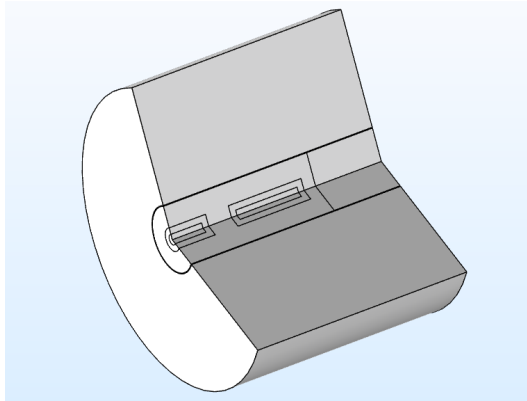


# Modelling results

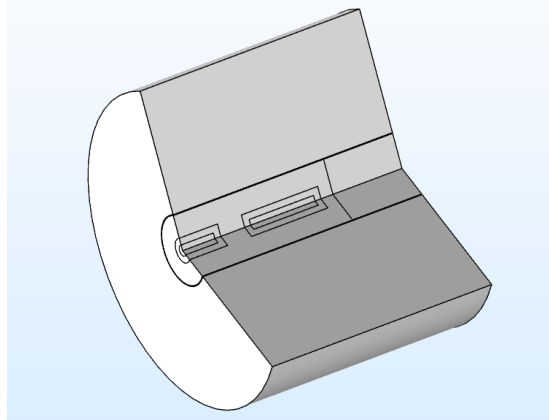
## Processes at the bentonite barrier

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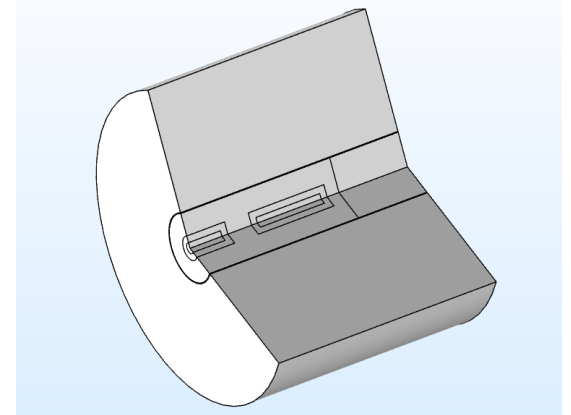
100 years



1 000 years



10 000 year



# Conclusions

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- **Numerical tools need to be improved** in order to handle coupled mass transport with reactions in long term simulations (10 000 years) and big domains (9000 mesh elements, 5000 nodes)
- Geochemical processes happening next to the **canister/bentonite** interface are the most relevant for most of the radionuclides present in the waste inventory
- Processes happening in the cement liner seems to be less relevant for radionuclide migration, but important for barrier integrity studies.

# Thank you for your attention!

Acknowledgement:

German Federal Ministry of Education and Research (Grant 02NUK053A) and the Initiative and Networking Fund of the Helmholtz Association (Grant SO-093) within the iCross project.

02.05.2020