



# MODELING THE SEA SURFACE WAVES IN HURRICANE BASING ON SELF- SIMILARITY CONCEPT

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- ▣ TC parameterization
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# Motivation

- ▣ Observation (satellites, buoy, aircraft) and modeling (e.g. WAVEWATCH III) of waves in TC is critical for forecasting and fundamental study
- ▣ Classical self-similar theory of wave development (Kitaigorodskii, 1962) demonstrated practical capabilities to reproduce surface wave characteristics, even under extreme wind conditions (e.g. Young, 1988, Young, 2013, Kudryavtsev et al., 2015).
- ▣ However, fields of surface waves under these extremes can rapidly become complex and characterized by multiple wave systems, limiting the direct use of the 1D self-similar fetch-laws (e.g. Hwang et al., 2017, Hwang and Walsh, 2018).
- ▣ In moving TC surface waves in the right sector obtain “unlimited” fetch (group velocity resonance) and can be “trapped” by TC
- ▣ It leads to typical asymmetry - appearance of waves, much larger than ones predicted by a “standard” fetch-law estimates using TC wind speed and its radius as a fetch
- ▣ Angular wave distributions in different TC parts are complicated : multimodal wave systems, some waves are moving windward



The **aim** of this work is to develop a 2D parametric model for wave evolution in non-uniform wind field, based on

- 1) energy and momentum conservation laws (Hasselmann et al., 1976)  
and
- 2) self-similarity concept relating non-dimensional wave frequency, wave energy and fetch (Kitaigorodskii, 1962)

and to apply this model to TC conditions



# Governing Equations

Energy and momentum conservation  
(Hasselmann et al., 1976; Phillips, 1977):

$$\partial E / \partial t + c_{gj} \partial E / \partial x_j = S^E$$

$$\partial M_i / \partial t + c_{gj} \partial M_i / \partial x_j = S_i^M$$

$E(\omega, \varphi) = A(\varphi - \varphi_p)F(\omega)$  - energy spectral density

$M_i = k_i E / \omega = \kappa_i \omega E / g$  - momentum spectral density

$$\kappa_i = [\cos \varphi, \sin \varphi]$$

$S^E = S_W - S_D + S_N$  - energy source

$S_i^M = \kappa_i \omega S^E / g$  - momentum source

$c_{gj}$  - group velocity

## Wind input:

$$S_W = \beta \omega A(\varphi - \varphi_p)F(\omega),$$

(Miles, 1957)

$\beta = c_\beta (u_*/c)^2 \cos^2(\varphi - \varphi_W)$  - growth rate  
 $c_\beta = (2 \div 6) \times 10^{-2}$  (Plant, 1982; Meirlink et al. 2003)  
 $u_*$  - friction velocity

If wind projection is smaller than wave phase velocity ( $u_k \cos(\varphi - \varphi_W) - c < 0$ )  $\rightarrow S_W = 0$ :

$$\beta = c_\beta (u_*/c)^2 \cos^2(\varphi - \varphi_W) H_\beta(\varphi - \varphi_W, u_{10}/c)$$

$$H_\beta(\varphi - \varphi_W, u_{10}/c) = \frac{1}{2} \left[ 1 + \tanh \left( p \left( \cos(\varphi - \varphi_W) \frac{u_{10}}{c} - 1 \right) \right) \right]$$

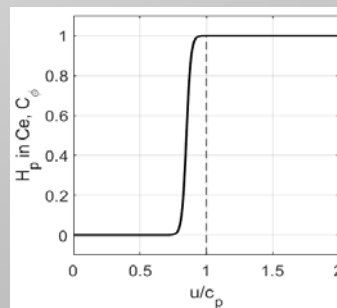
## Dissipation:

Wave breaking  
(Longuet-Higgins, 1969)

$$D = \omega_p e (k_p^2 e / \varepsilon_T^2)^n$$

$$D = \int S_D d\varphi d\omega$$

$$e = \int E d\varphi d\omega$$



## Non-linear interactions:

Four-wave interactions  
(Hasselmann, 1962)

Energy transfer towards low frequencies:

$$\partial S_N / \partial \omega < 0$$

$$\langle S_N \rangle \sim E^3$$

(Zakharov, 2010;  
Badulin et al., 2007)

# Governing Equations

$$\begin{aligned} \partial E / \partial t + c_{gj} \partial E / \partial x_j &= S^E \\ \partial M_i / \partial t + c_{gj} \partial M_i / \partial x_j &= S_i^M \end{aligned} \quad \left| \begin{aligned} &\iint d\varphi d\omega \\ &\text{and some algebra...} \end{aligned} \right.$$



$$\begin{aligned} e &= \int E d\varphi d\omega \\ \bar{c}_g &= \int c_g F(\omega) d\omega / e \\ \bar{\omega} &= \int \omega F(\omega) d\omega / e \\ \kappa_j^p &= [\cos \varphi_p, \sin \varphi_p] \\ \omega_p / \bar{\omega} &= \bar{c}_g / c_{gp} = r_g \end{aligned}$$

$$\left\{ \begin{aligned} \frac{\partial e}{\partial t} + \kappa_j^p \bar{c}_g \frac{\partial e}{\partial x_j} + e \partial(\kappa_j^p \bar{c}_g) / \partial x_j &= \iint S^E d\varphi d\omega \\ &\approx \iint (S_W - S_D) d\varphi d\omega \quad - \text{energy growth rate (wind+dissipation)} \\ \frac{\partial}{\partial t} \omega_p + \kappa_j^p \bar{c}_g \frac{\partial}{\partial x_j} \omega_p &= \frac{r_g}{e} \int (\omega - \bar{\omega}) S_O^E d\omega \quad - \text{peak frequency (non-linear interactions)} \\ \frac{\partial}{\partial t} \varphi_p + \kappa_j^p \bar{c}_g \frac{\partial}{\partial x_j} \varphi_p &= \frac{1}{\bar{\omega} e} \iint \sin(\varphi - \varphi_p) \omega S^E d\varphi d\omega \quad - \text{peak direction (wind)} \end{aligned} \right.$$

**Parameters in the right-hand side are derived using  
1D equations (uniform wind:  $\partial / \partial t = 0, \varphi_p = \varphi_w$ ),  
together with fetch-limited laws (Kitaigorodskii, 1962)  
and then generalized to 2D equations**



# Energy

## Link to self-similarity

$$\left\{ \begin{array}{l} \tilde{x} = xg / u^2 \\ \tilde{e} = eg^2 / u^4 \\ \tilde{\omega}_p = \omega_p u / g \\ \alpha = u / c_p \end{array} \right.$$

$$\partial e / \partial t + \kappa_j^p \bar{c}_g \partial e / \partial x_j + e \partial (\kappa_j^p \bar{c}_g) / \partial x_j = \iint S^E d\varphi d\omega$$

Right hand side:

$$\approx \iint (S_w - S_D) d\varphi d\omega$$

$$\iint (S_w - S_D) d\varphi d\omega = I_w - D$$

Model assumption:

Dissipation is proportional to the wind input:

$$D/I_w = \gamma \Rightarrow (k_p^2 e)^n \propto \alpha^2$$

$$\Rightarrow n = \frac{2q}{p+4q}$$

$$I_w - D = \omega_p e (\tilde{I}_w - \tilde{D})$$

$$\tilde{I}_w - \tilde{D} = C_e H_p \alpha^2 \cos^2(\varphi_p - \varphi_w) - (ek_p^2 / \varepsilon_T^2)^n$$

$$H_p = 1/2 \cdot \left\{ 1 + \tanh \left[ p (\cos(\varphi_p - \varphi_w) \alpha - 1) \right] \right\}$$

Fetch laws:

(Kitaigorodskii, 1962)

$$\tilde{\omega}_p \equiv \alpha = c_\alpha \tilde{x}^q, \quad \tilde{e} = c_e \tilde{x}^p$$

**For the case of uniform wind:**

$$\partial e / \partial t = 0, \varphi_p = \varphi_w$$

$$\partial (\bar{c}_g e) / \partial x \propto (g/u) \alpha^3 e$$

$$q = -1/4$$

$C_e$  and  $\varepsilon_T$  are constants calibrated on fetch-laws

# Link to self-similarity

## Peak frequency

$$\frac{\partial}{\partial t} \omega_p + \kappa_j^p \bar{c}_g \frac{\partial}{\partial x_j} \omega_p = \frac{r_g}{e} \int (\omega - \bar{\omega}) S_o^E d\omega$$

Right hand side (NL interactions):

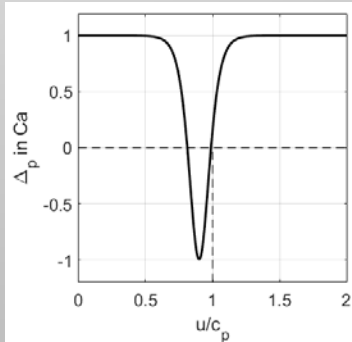
$$e^{-1} \int (\omega - \bar{\omega}) S_o^N d\omega \approx$$

$$\begin{aligned} \delta\omega \propto \omega_p \quad \left| \begin{array}{l} \langle S_N \rangle \sim e^3 \end{array} \right. & \rightarrow \approx e^{-1} \partial S_o^N / \partial \omega \int (\omega - \bar{\omega})^2 d\omega \\ & \propto -e^{-1} \delta\omega^2 \langle S_o^N \rangle \\ & \propto -\omega_p^2 k_p^4 e^2 \propto -g^{-4} \omega_p^{10} e^2 \end{aligned}$$

$$\begin{aligned} e^{-1} \int (\omega - \bar{\omega}) S_o^N d\omega &= C_\alpha g^{-4} \omega_p^{10} e^2 \\ &= C_\alpha \omega_p^2 (k_p^2 e)^2 \end{aligned}$$

Restriction for fully developed waves:

$$\begin{aligned} C_a &= C_a \Delta_p \\ \Delta_p &= 1 - 2 \operatorname{sech}^2(10(\alpha - 0.9)) \\ C_e &\text{ calibrated on fetch-laws} \end{aligned}$$



Fetch laws:

(Kitaigorodskii, 1962)

$$\tilde{\omega}_p \equiv \alpha = c_\alpha \tilde{x}^q, \quad \tilde{e} = c_e \tilde{x}^p$$

**For the case of uniform wind:**

$$\partial e / \partial t = 0, \varphi_p = \varphi_w$$

$$c_{gp} \partial \omega_p / \partial x \propto g^{-4} \omega_p^{10} e^2$$

$$2p + 10q + 1 = 0 \quad \text{-- "magic relations"}$$

(Badulin et al., 2007;  
Zakharov, 2010)

$$p = 3/4$$

$$n = 2$$

$$\begin{aligned} q &= -1/4 \\ n &= \frac{2q}{p + 4q} \end{aligned}$$



# Spectral peak direction

$$\frac{\partial}{\partial t} \varphi_p + \kappa_j^p \bar{c}_g \frac{\partial}{\partial x_j} \varphi_p = \frac{1}{\bar{\omega} e} \iint \sin(\varphi - \varphi_p) \omega S^E d\varphi d\omega$$



Taylor series around  $\varphi = \varphi_p$



Dissipation and four-wave interactions  
are functions of wave spectrum,  
while wind input is also a function of  
wave direction



Integral over azimuth vanishes for  $S_D$  and  $S_N$ .  
Change of wave direction is caused by wind

$$\frac{\partial}{\partial t} \varphi_p + \kappa_j^p \bar{c}_g \frac{\partial}{\partial x_j} \varphi_p = -C_\varphi \alpha^2 \omega_p H_p \sin[2(\varphi_p - \varphi_w)]$$

$$C_\varphi = c_\beta c_D \delta \varphi^2 \frac{\int \omega^4 F(\omega) d\omega}{\omega_p^3 \int \omega F(\omega) d\omega} = 1.8 \times 10^{-5} \text{ for JONSWAP spectrum}$$

# Effect of Group Velocity Divergence (Ray Focusing)

Energy growth rate in ray  
characteristic form:

$$\frac{de}{dt} = -e \left( \overbrace{\partial \bar{c}_g / \partial l + \bar{c}_g \partial \varphi_p / \partial n}^{c_g \text{ divergence}} \right) + \omega_p e (\tilde{I}_w - \tilde{D}) \quad | / e$$

$$\partial \bar{c}_g / \partial l \approx \Delta \bar{c}_g / (\bar{c}_g \Delta t) = \bar{c}_g^{-1} d\bar{c}_g / dt$$

$$\bar{c}_g \partial \varphi_p / \partial n \approx \bar{c}_g \Delta \varphi_p / \Delta n = \bar{c}_g G_n$$

$\Delta n$  - distance between neighbor characteristics

$\Delta \varphi_p$  - direction difference between them

$G_n, G_w$  - peak/wind direction gradient in cross-ray direction,  $\Delta \varphi / \Delta n$

*ray focusing/defocusing*

$$\frac{d}{dt} \ln(\bar{c}_g e) = -\bar{c}_g G_n + \omega_p (\tilde{I}_w - \tilde{D})$$

**Caustic:**  $\Delta n \rightarrow 0$

Restriction for  $G_n$   
(wave is not monochromatic):

$$G_n = \frac{\Delta \varphi_p}{\Delta n_0} \left[ \frac{\Delta n / \Delta n_0}{(\Delta n / \Delta n_0)^2 + (1/2 \cdot \Delta c_g / \bar{c}_g)^2} \right]$$

$$(\Delta c_g / \bar{c}_g)^2 = 4.6 \times 10^{-2} \text{ - JONSWAP}$$

from eq. for  $\varphi_p$  :

$$\frac{d\Delta \varphi_p}{dt} \approx T^{-1} (\Delta \varphi_w - \Delta \varphi_p) \quad | / \Delta n$$

$$T^{-1} = 2C_\varphi H_p \alpha^2 \omega_p \cos(2(\varphi_p - \varphi_w))$$

$$d\Delta n / dt = \Delta \varphi_p \bar{c}_g$$

$$dG_n / dt + G_n / T + \bar{c}_g G_n^2 = G_w^n / T$$

$$G_n = \Delta \varphi_p / \Delta n$$

# Complete System of Equations

$$\frac{d}{dt} x_j = \kappa_j^p \bar{c}_g \quad - \text{wave train } \underline{\text{position}}$$

$$\frac{d}{dt} \ln(\bar{c}_g e) = -\bar{c}_g G_n + \omega_p (\tilde{I}_w - \tilde{D}) \quad - \text{modified } \underline{\text{energy}}$$

$$\frac{d}{dt} c_{gp} = -\frac{r_g C_\alpha}{2} \Delta_p g (k_p^2 e)^2 \quad - \text{spectral peak } \underline{\text{group velocity}} \text{ (from eq. for frequency)}$$

$$\frac{d}{dt} \varphi_p = C_\varphi \alpha^2 \omega_p H_p \sin[2(\varphi_p - \varphi_w)] \quad - \text{spectral peak } \underline{\text{direction}}$$

$$dG_n/dt + G_n/T + \bar{c}_g G_n^2 = G_w^n/T \quad - \text{peak direction gradient (} \underline{\text{focusing}} \text{ term), } G_n = \Delta\varphi_p/\Delta n$$

(or two eq. instead: for  $\Delta\varphi_p$  and  $\Delta n$ )

System describes the development of surface waves under a varying wind field in both space and time, as well as the evolution of swell propagation in the absence of wind forcing

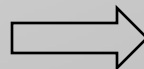
Wave breaking of dominant waves:

(Phillips, 1985)

$$Q_p = \varepsilon k_p^{-1} L_p \quad D = b g^{-1} c^5 L$$

$$\Downarrow$$

$$D = \omega_p e (k_p^2 e / \varepsilon_T^2)^n$$



$$Q_p \propto \varepsilon_T^2 (e k_p^2 / \varepsilon_T^2)^3$$

# Method to solve the equations

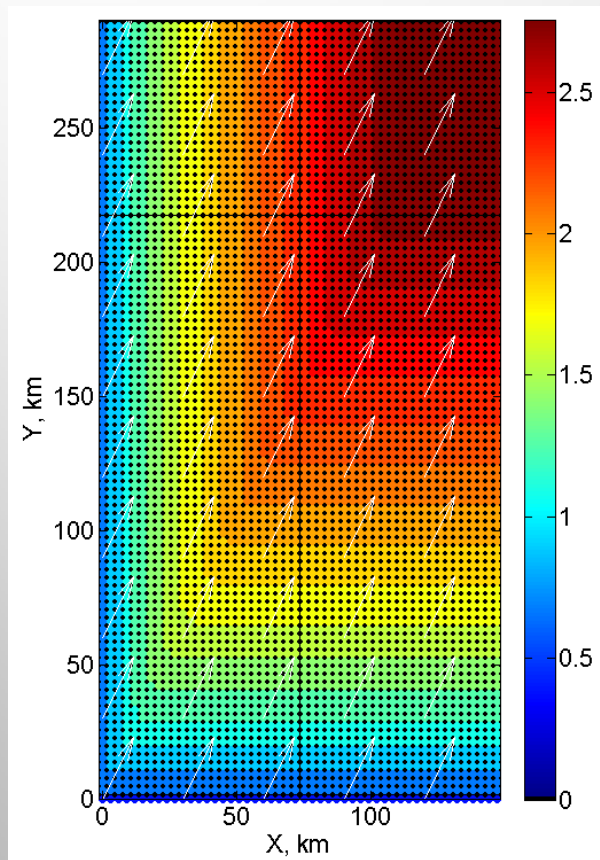
- ▣ A wind field on a uniform grid and a initial locations of wave trains are set
- ▣ Wave characteristics at  $t=0$ :  $\omega_0 = 3$ ,  $\varphi_0 = \varphi_w$ ,  $\Delta\varphi_p = 0$ ,  $e_0 = U^4/g^2 c_e (a/c_a)^{p/q}$
- ▣ Right-hand sides of every equation are calculated
- ▣ Wave train coordinates and other parameters at  $t_{i+1}=t_i+dt$  are obtained with the use of 4<sup>th</sup> order Runge-Kutta scheme
- ▣ Starting  $dt \sim 1s$  slowly increases to 30 min to reduce calculation time and data amount



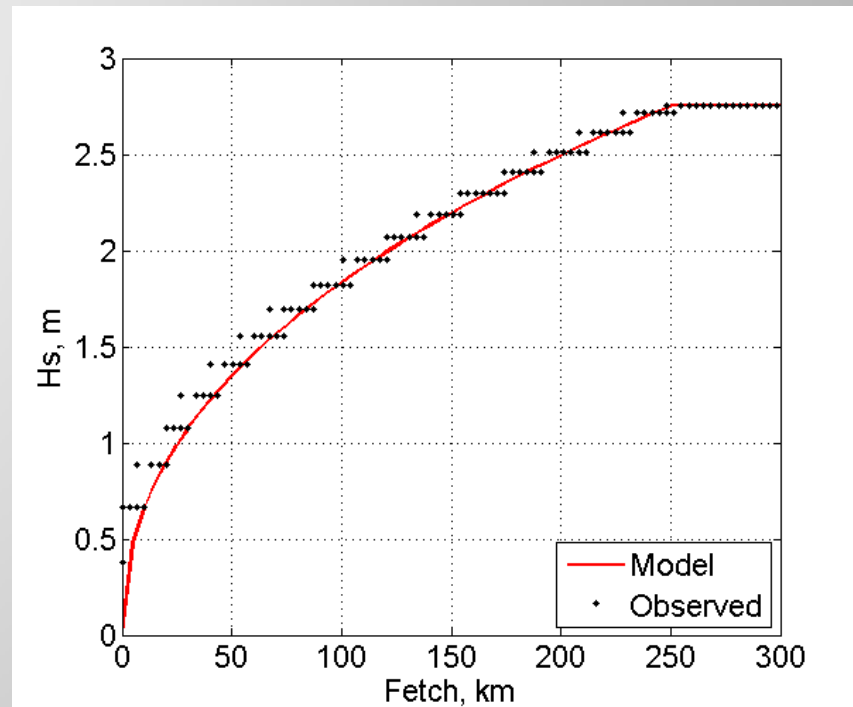
**An array of wave train coordinates, peak frequency, energy, direction, wave age, distance between “neighbor” characteristics (focusing effect) at every discrete time point**

# Model Simulations: Uniform Wind

Constant wind from the shore.  
Effective fetch:  $U \cos(a)$



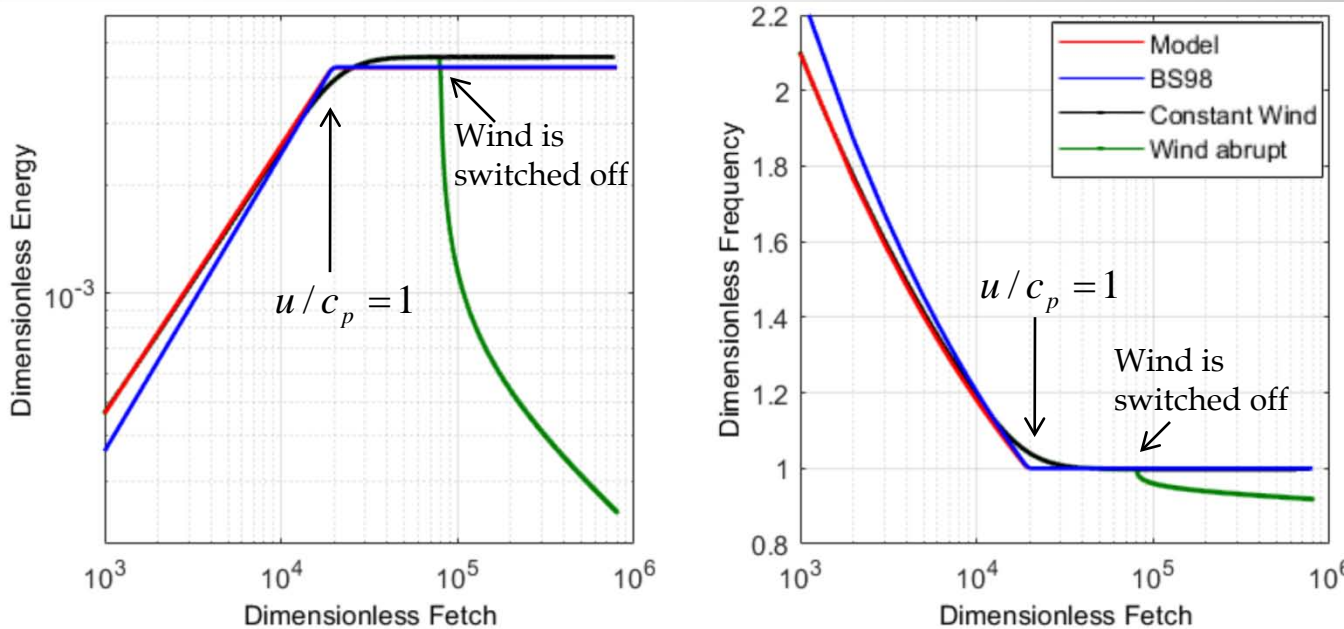
Hs field



Max Hs inside areas around grid points vs  
effective fetch in comparison with fetch law  
model,  $\tilde{e} = c_e \tilde{x}^p$   
( $p=0.83$ ,  $c_e=5.88e-7$ , Babanin&Soloviev, 1998)



# Model Simulations: Uniform Wind



$$\tilde{x} = xg / u^2$$

$$\tilde{e} = eg^2 / u^4$$

$$\tilde{\omega}_p = \omega_p u / g$$

Fetch laws:

$$\tilde{\omega}_p \equiv \alpha = c_\alpha \tilde{x}^q, \quad \tilde{e} = c_e \tilde{x}^p$$

Dimensionless energy and peak frequency vs dimensionless fetch.

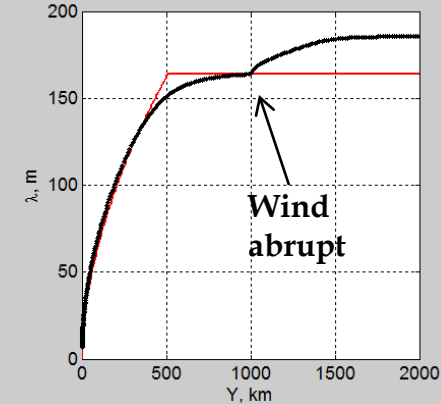
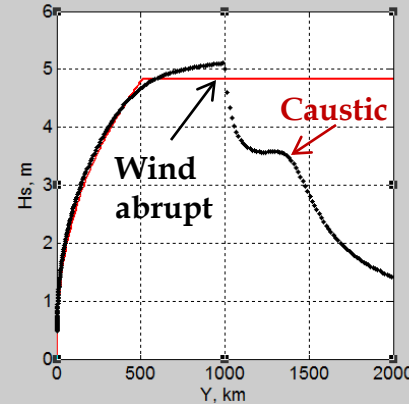
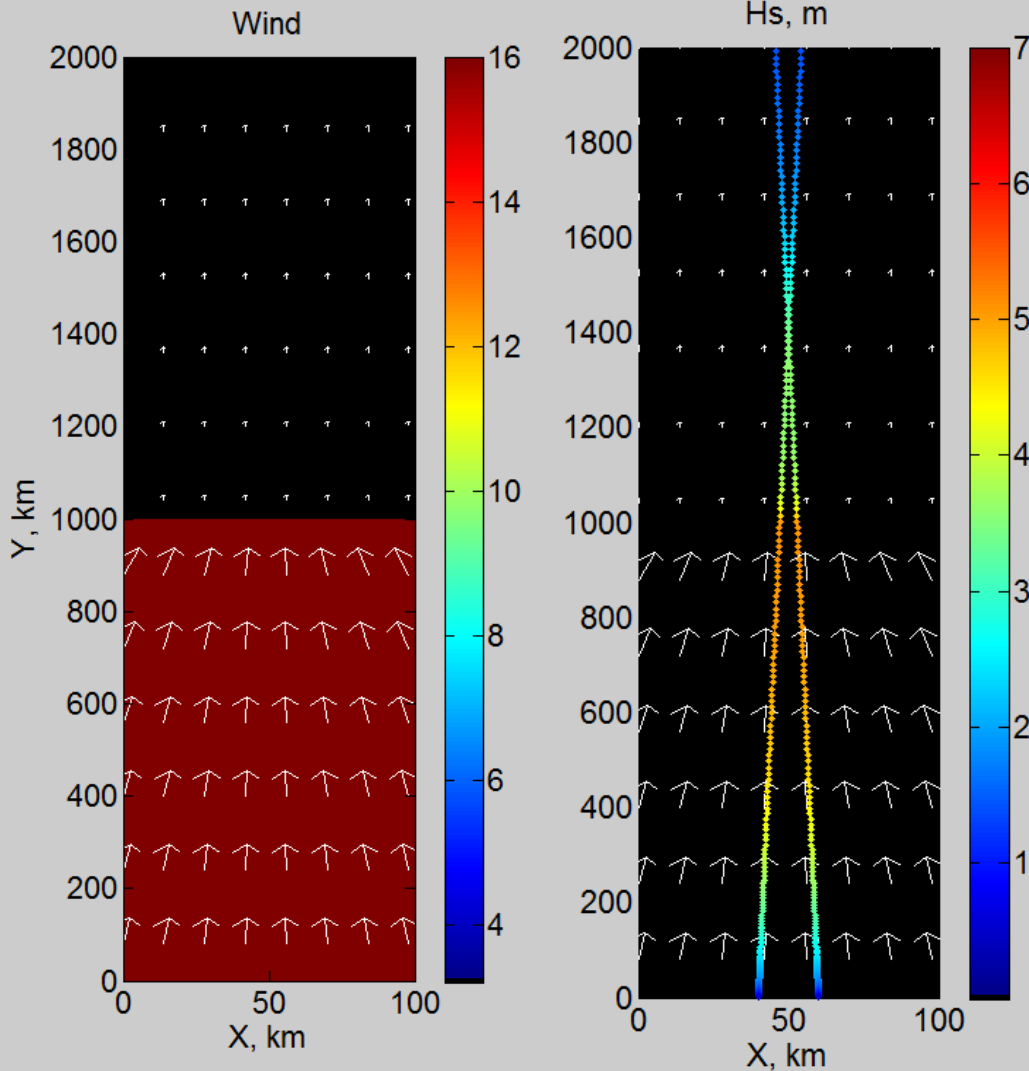
Our model (red/black), Babanin&Soloviev, 1998 (blue).

Green line shows model evolution of energy and frequency after the wind suddenly drops at fetch  $\tilde{x} = 8 \cdot 10^4$

1. The model provides a smooth transition from developing to fully developed waves.
2. Swell: a rapid decay of the wave energy (much stronger than predicted by Zakharov and Badulin, 2017) under the weakly turbulent theory,  $\tilde{x}^{-1/12}$ )
3. Swell: a moderate downshift of the peak frequency

# Convergent Wind Field. Caustic

## Hs and wavelength profiles



1. Wind (16 m/s) abruptly decreases to 3m/s at fetch 1000 km
2. Fully developed waves turn to decaying focusing swell
3. Rays cross at fetch ~1300 km
4. In caustic point energy temporarily grows, than rays diverge with additional energy lose
5. Caustic effects are weakly/not manifested in wavelength

# Convergent/Divergent Wind Effects

Wind is uniform in the main direction, but varying in the perpendicular direction,  $V \ll U$

Gradient of wind direction

$$|G_w| = 10^{-4} \text{ rad/m:}$$

negative – divergence (**blue**),

positive – convergence (**red**)

zero – **black**

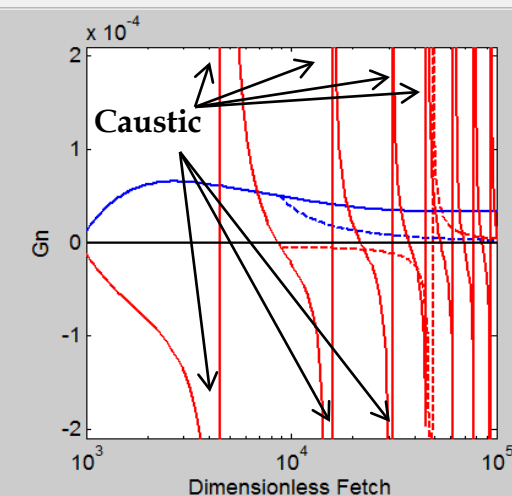
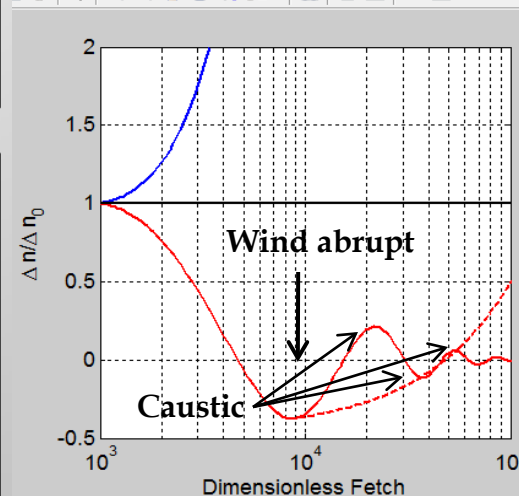
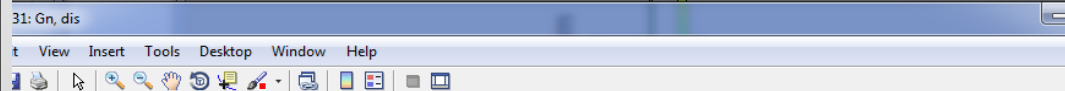
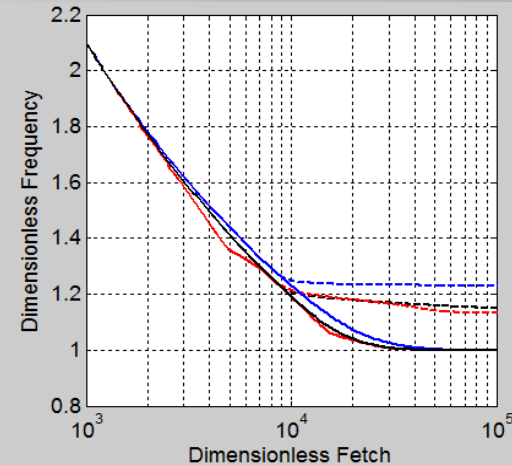
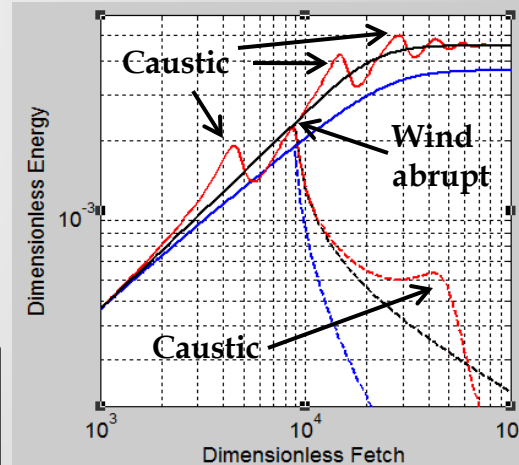
dashed line ---- wind abrupt (swell)

Divergence of the wind velocity forces the wave rays to widen – additional energy sink (decrease ~30%, and deceleration of the frequency downshift)

**Swell:** rapid attenuation and shorter peak wavelength

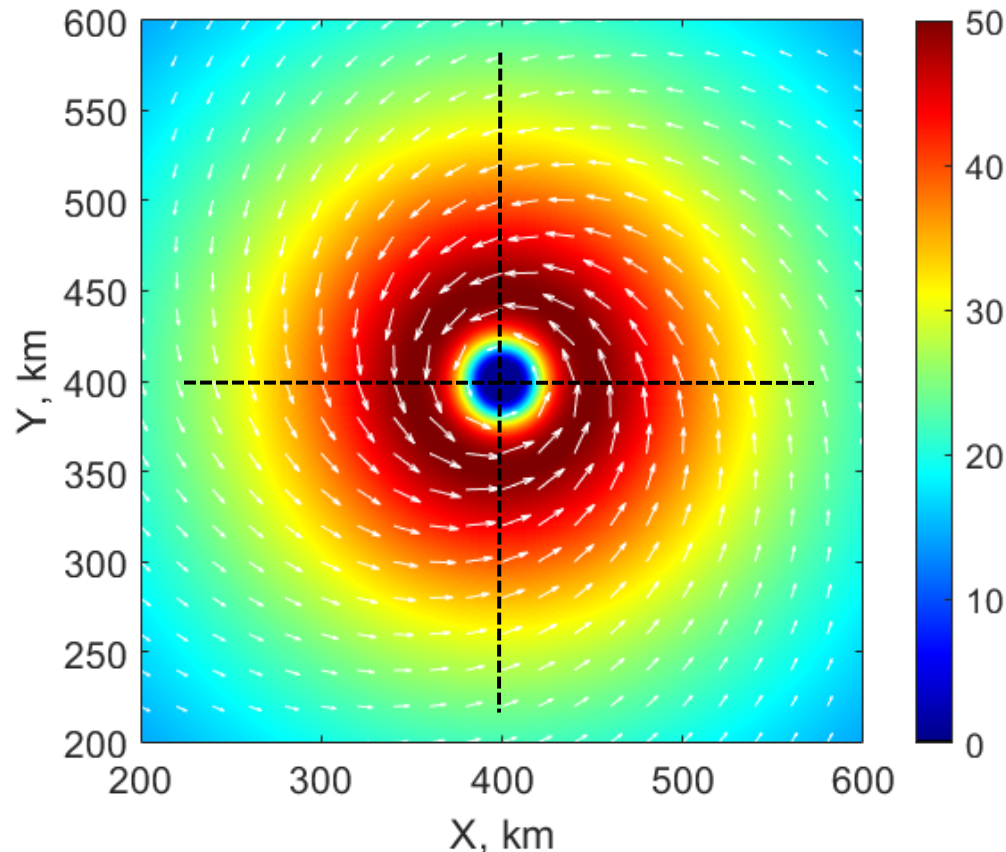
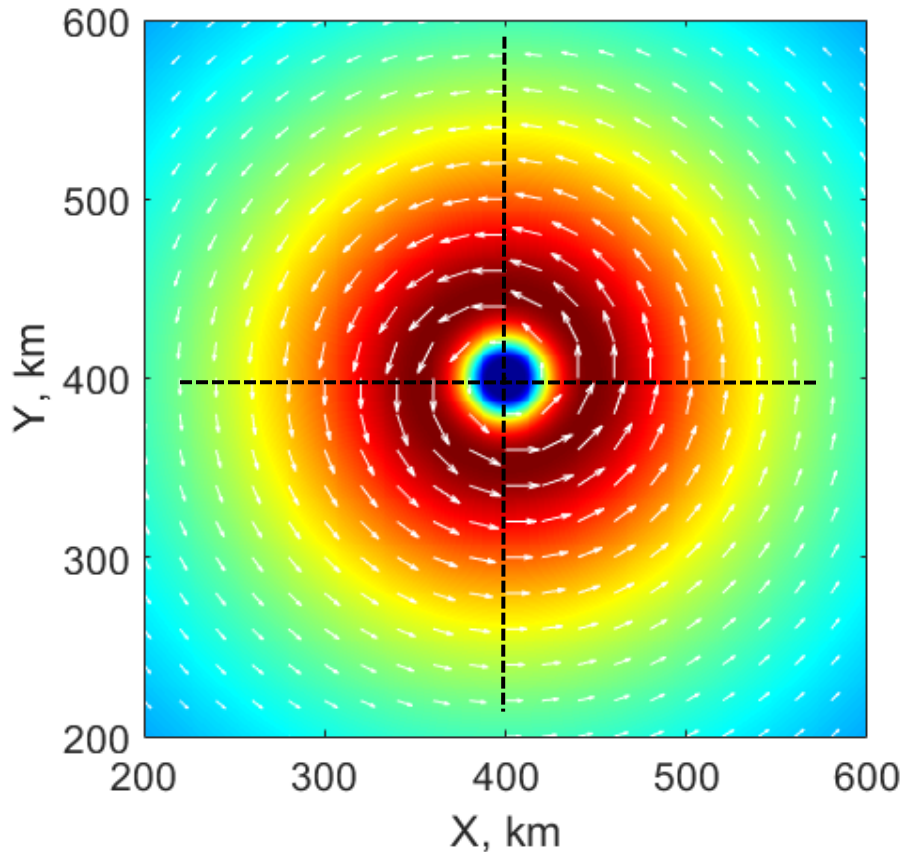
Wind velocity convergence forces wave rays to concentrate (caustic), then diverge and converge again under the action of wind gradient (recurrent process).

**Swell:** wave-ray thickening is terminated, rays diverge away from the last caustic zone, energy rapidly attenuates



# Stationary cyclone-type wind field

$$u(r) = \left[ \left( u_m^2 + u_m r f \right) \left( \frac{R_m}{r} \right)^B \exp \left( - \left( \frac{R_m}{r} \right)^B + 1 \right) + \left( \frac{r f}{2} \right)^2 \right]^{1/2} - \frac{r f}{2} \quad \text{Holland, 1980}$$



## Wind field with zero inflow angle

Wind direction gradient:

$|G_w| = 1/r$  with a direction tangent to the circle

Cross-ray projection:  $G_w^n = 0$

## Wind field with 20 deg inflow angle

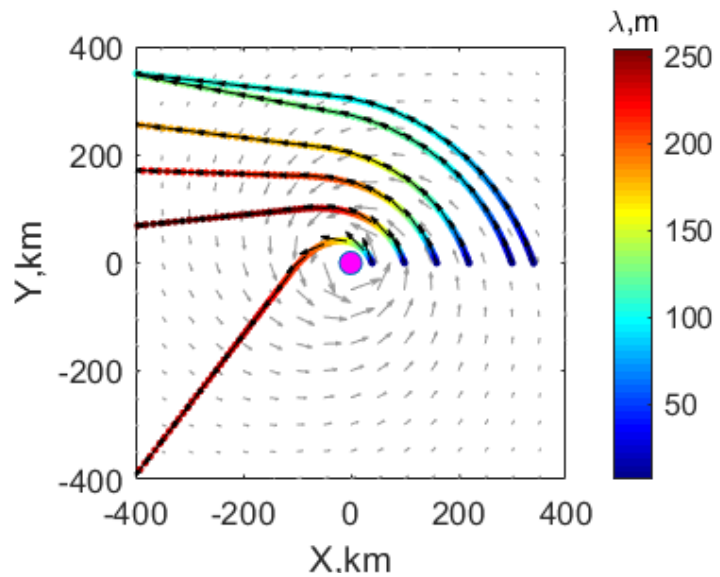
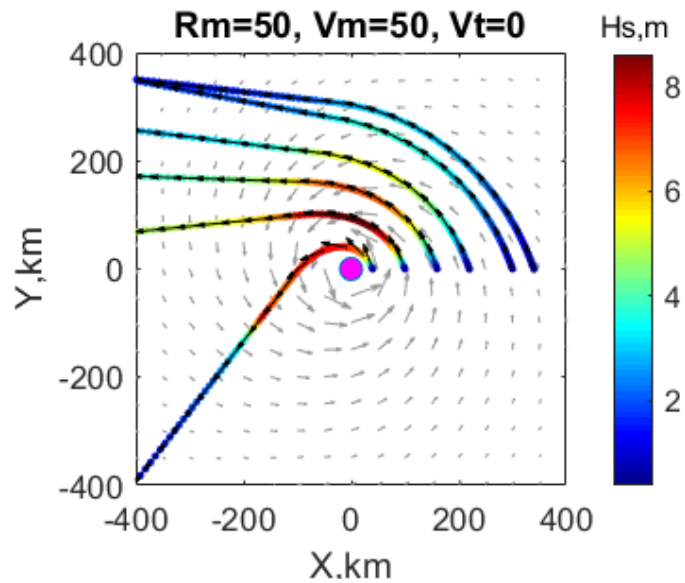
(Shea and Gray, 1973)

$G_w^n = -|G_w| \sin \phi_{in}$  - wave-ray focusing



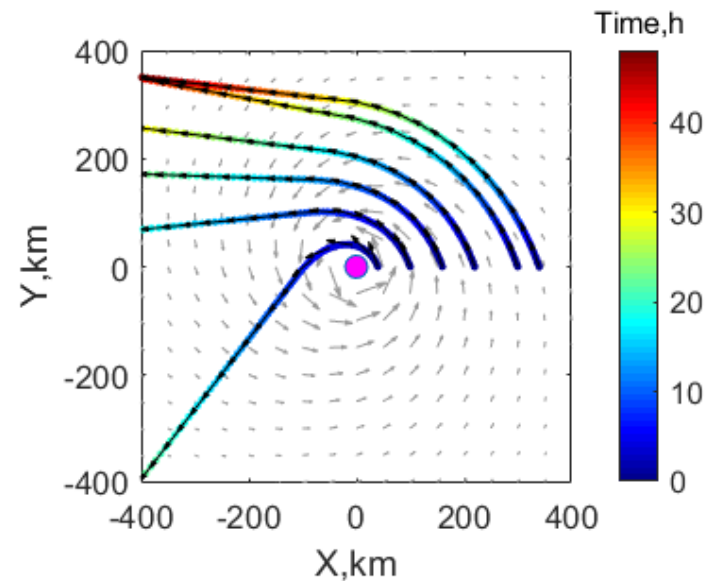
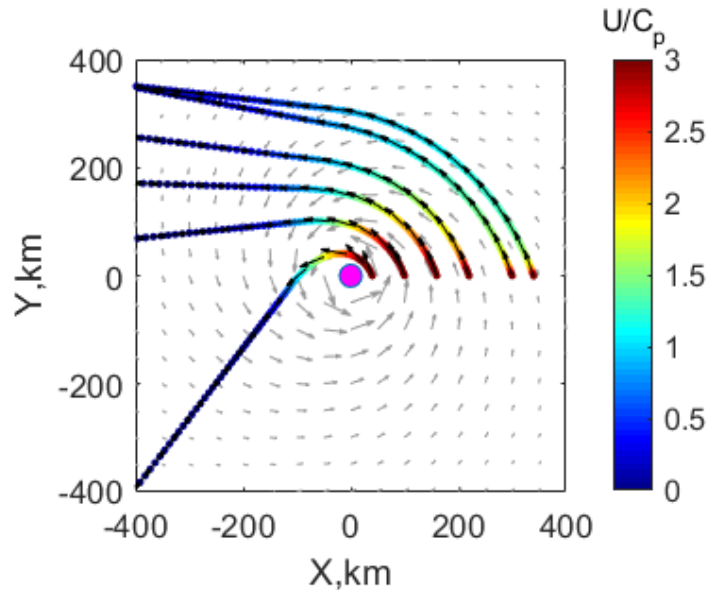
# Typical Wave Rays in Stationary Cyclone (20 deg wind inflow angle)

Significant wave height



Wave length

Wave age



Time



# Along-ray Profiles

Zero inflow angle

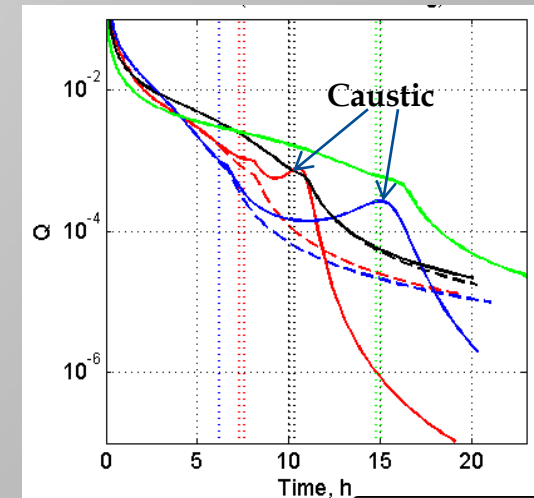
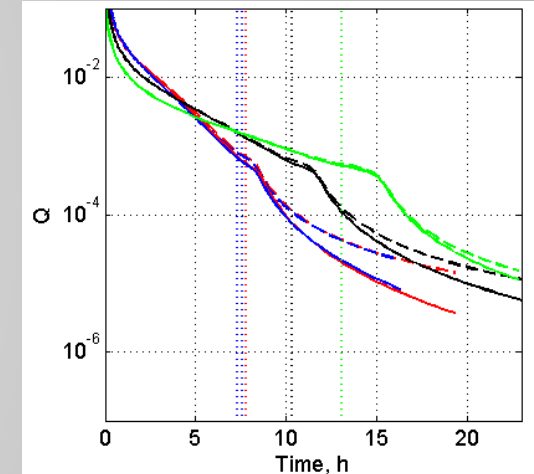
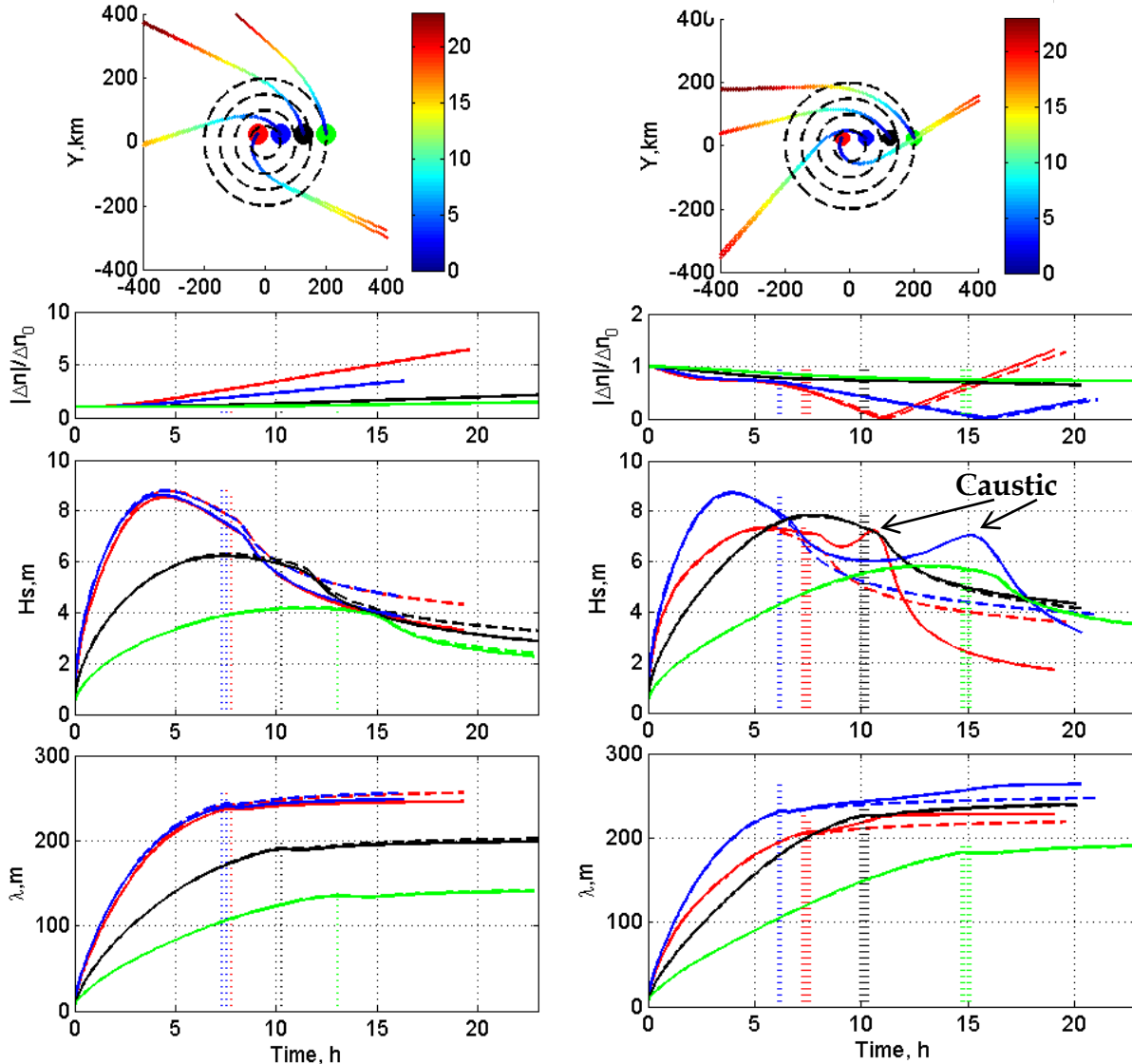
20 deg inflow angle

Wave breaking

(strong dependency on wave age)

Zero inflow angle

20 deg inflow angle



Dash lines - focusing term is off ( $G_n=0$ )

Vertical dash lines - a wave-train passes from wind force regime to swell one

# Radial Distributions for Different Wind Fields

**Different combinations** of TC radii and maximum wind speeds:

$R_m = 30, 50, 70$  km,

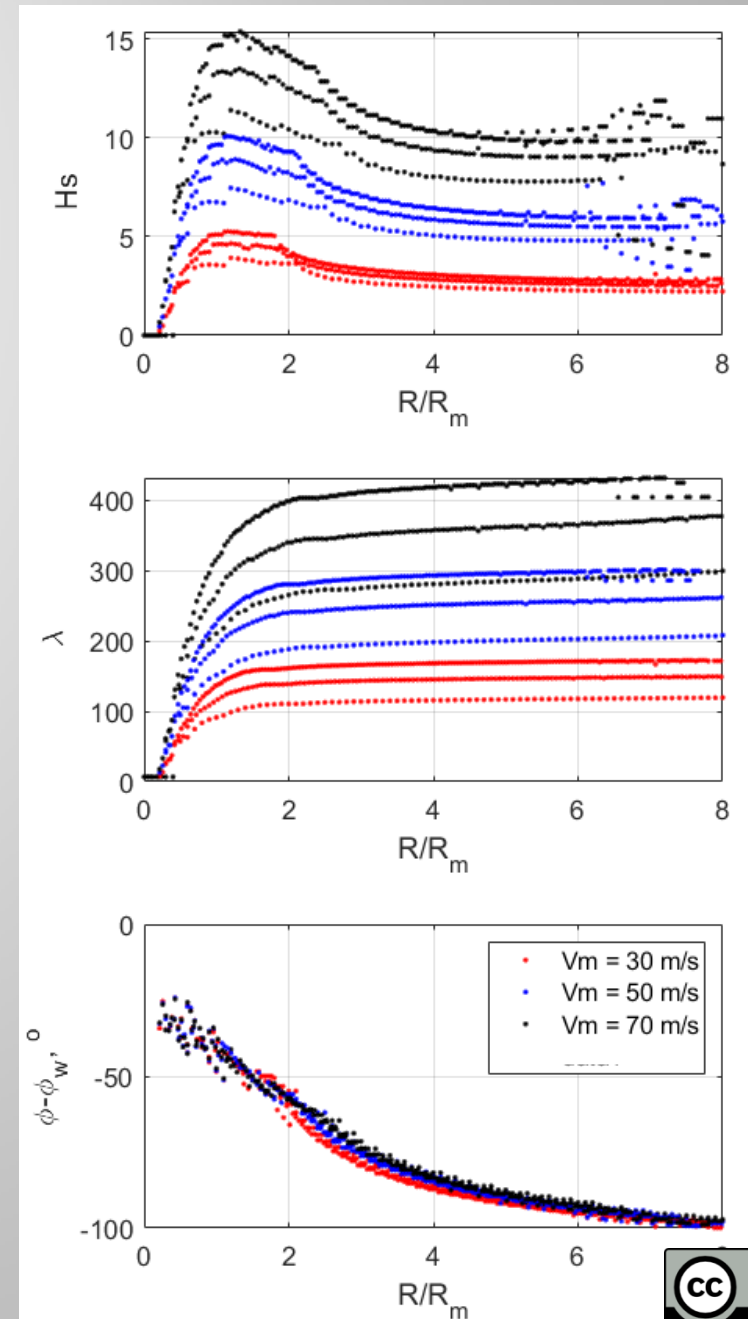
$U_m = 30, 50, 70$  m/s

For the **same radius**:

the larger the wind speed, the larger the wavelength and  $H_s$

For the **same maximum wind speed**:

the larger the radius, the larger the wavelength and  $H_s$



# Radial Distributions (Scaled)

Different combinations of TC radii and maximum wind speeds  
( $R_m=30, 50, 70$  km,  
 $U_m=30, 50, 70$  m/s)

**Radial distributions are scaled:**

$$Hs_d = Hs(g/U_m^2)/\tilde{H}s,$$

$$\lambda_d = \lambda(g/U_m^2)/\tilde{\lambda}$$

where

$$\tilde{H}s \sim \sqrt{\tilde{e}} = \tilde{R}^{p/2}$$

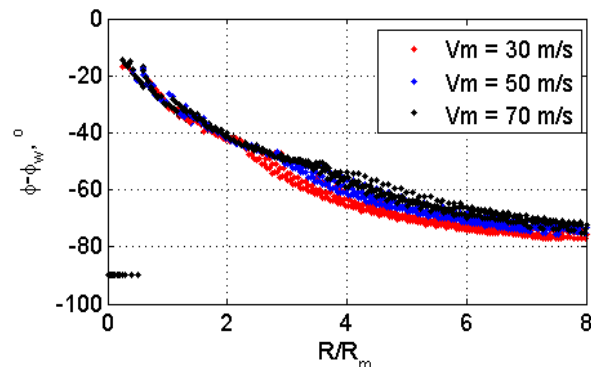
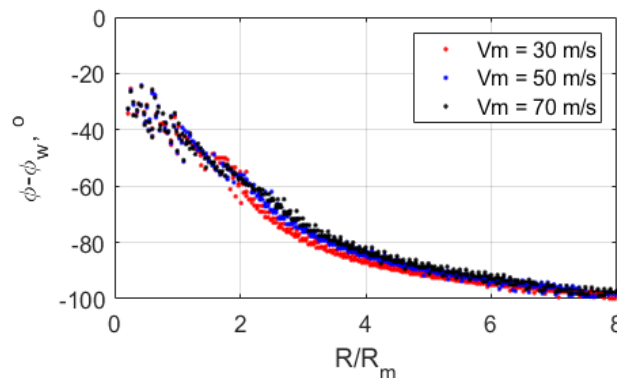
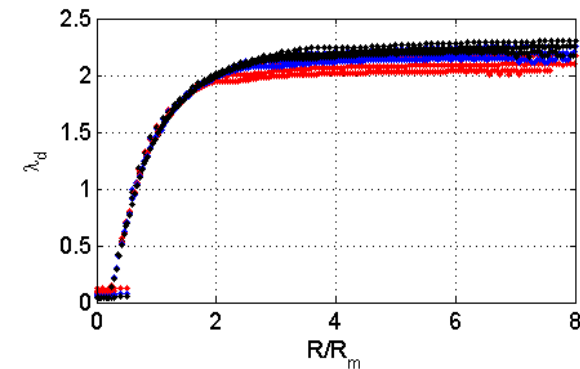
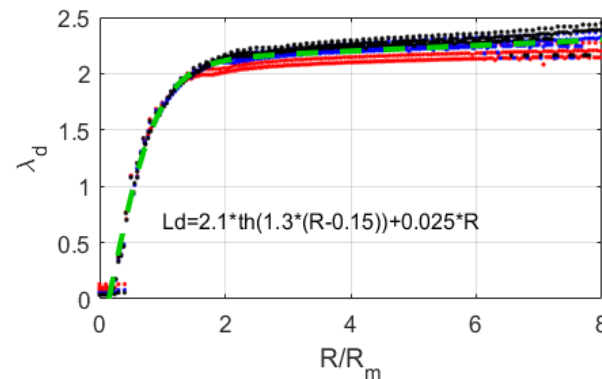
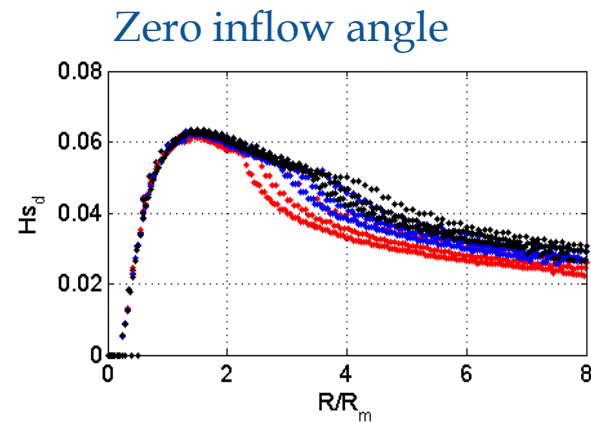
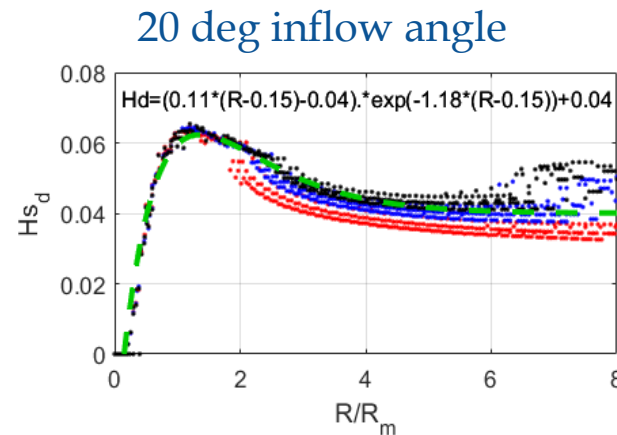
$$\tilde{\lambda} \sim \tilde{\omega}_p^{-2} = \tilde{R}^{-2q}$$

$$\tilde{R} = R_m g/U_m^2$$

$$p = 3/4, q = -1/4$$

Profiles almost **collapse**,  
exhibiting self-similar shapes for  
distances smaller than  $2R_m$

**Inflow angle** modifies  $Hs$  profiles  
(extra energy pumping due to  
cross-ray convergence)  
These effects on wavelength are  
less strong

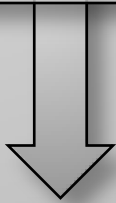


# Waves in Moving TC

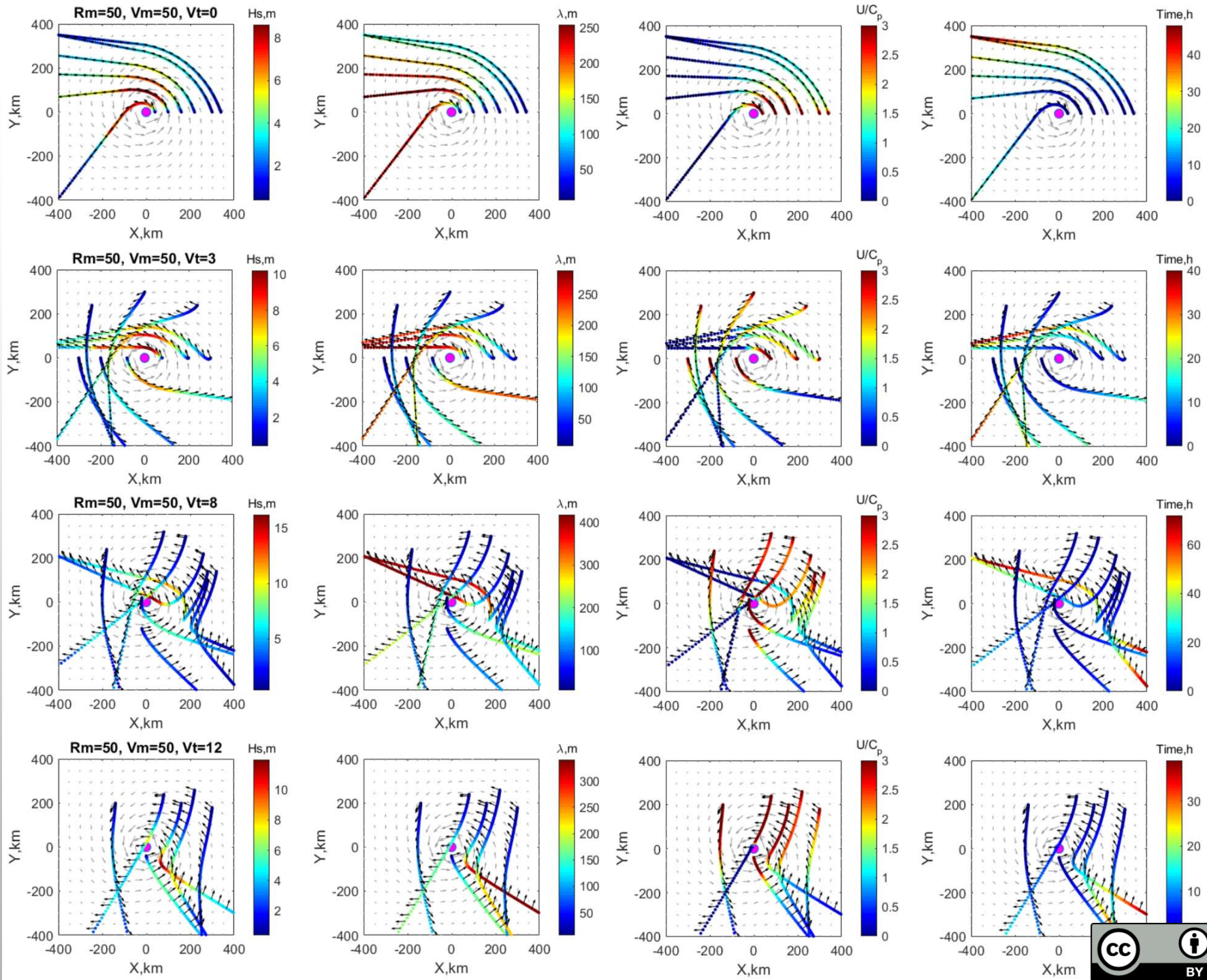
In coordinate system related to TC,  
wave train position:

$$\frac{d}{dt} x_j = \kappa_j^p \bar{c}_g (-V t_i)$$

Typical wave train parameters for different hurricane  
translation velocities,  $Vt$   
(TC is moving upwards)

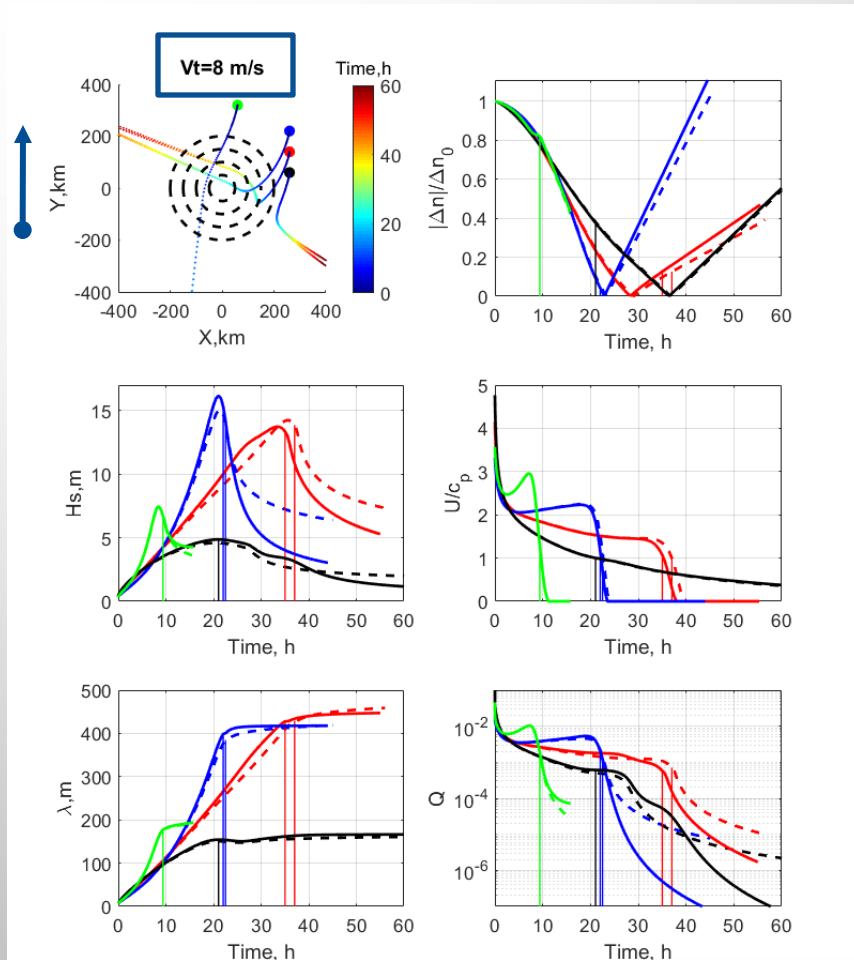




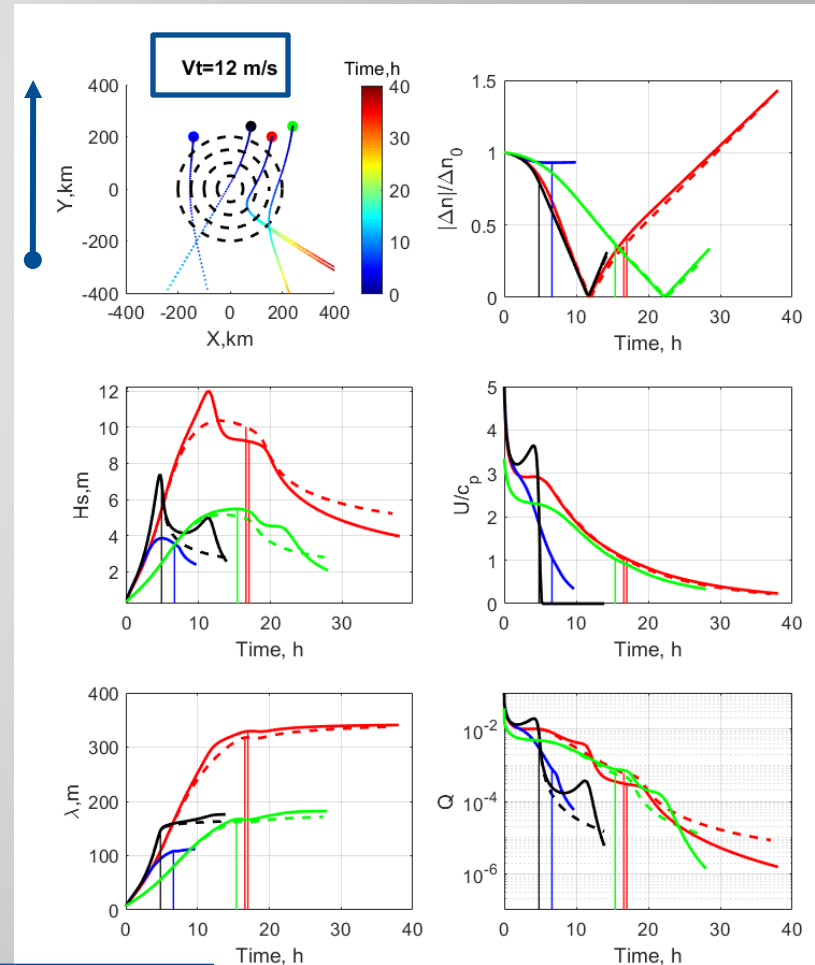




# Along-ray Profiles



Dash line:  $G_n = 0$  (no focusing effects)

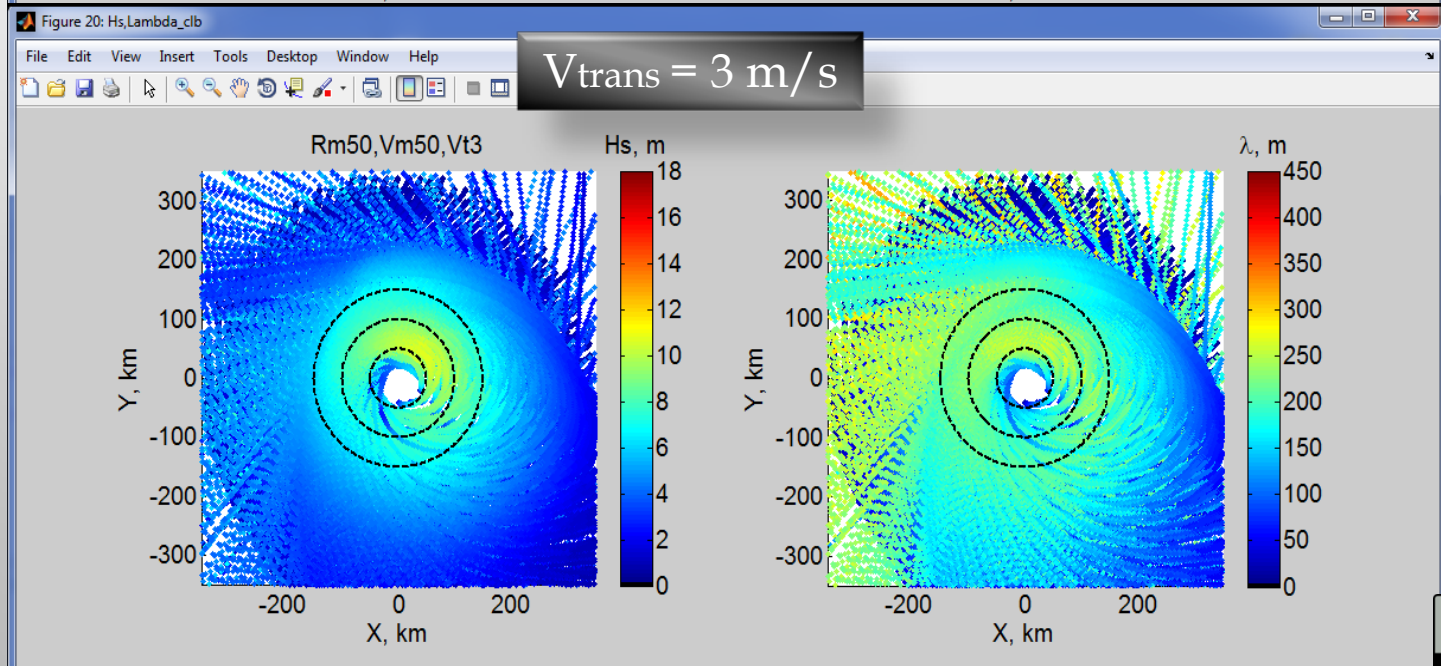
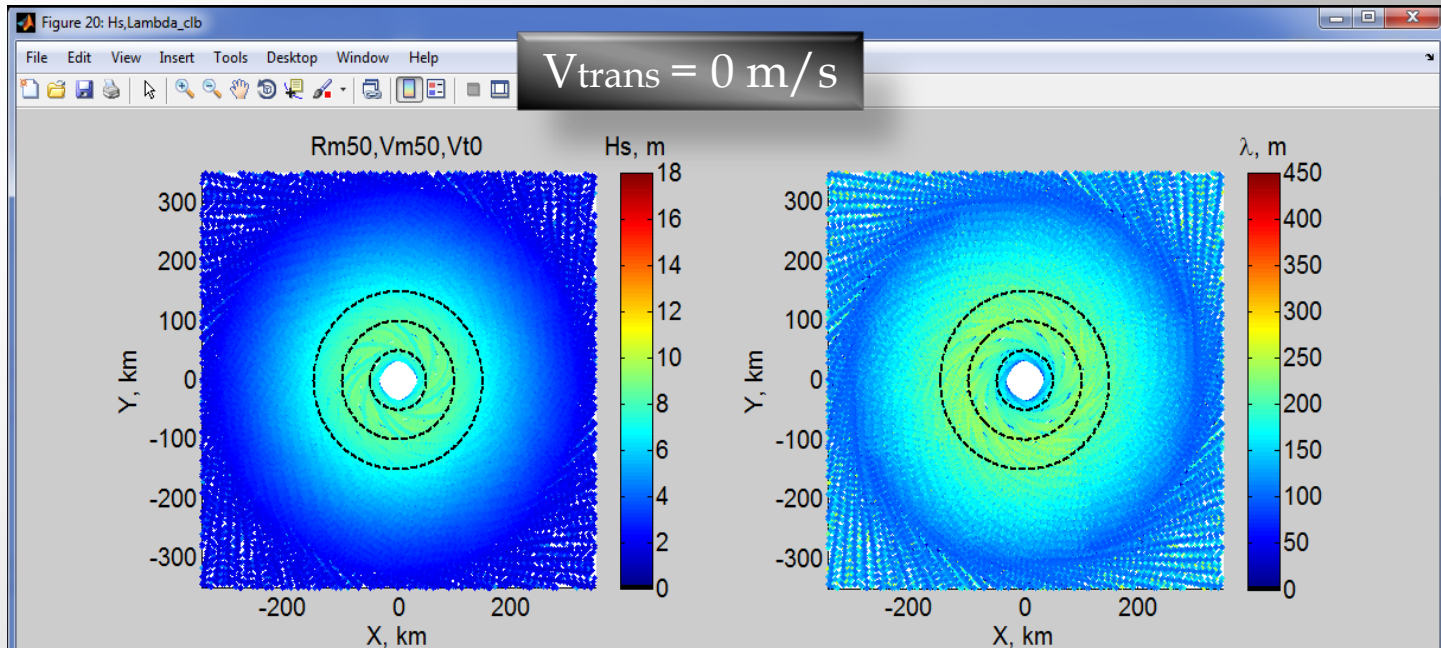


Waves from up-right sector (red, blue) are “trapped” by TC central part and shifted to the left (high energy).  
Extra energy pumping is due to ray focusing effect.  
After caustic → stronger dissipation.

In very fast hurricanes most waves pass downwards.  
Energy intensification is in down-right TC sector.

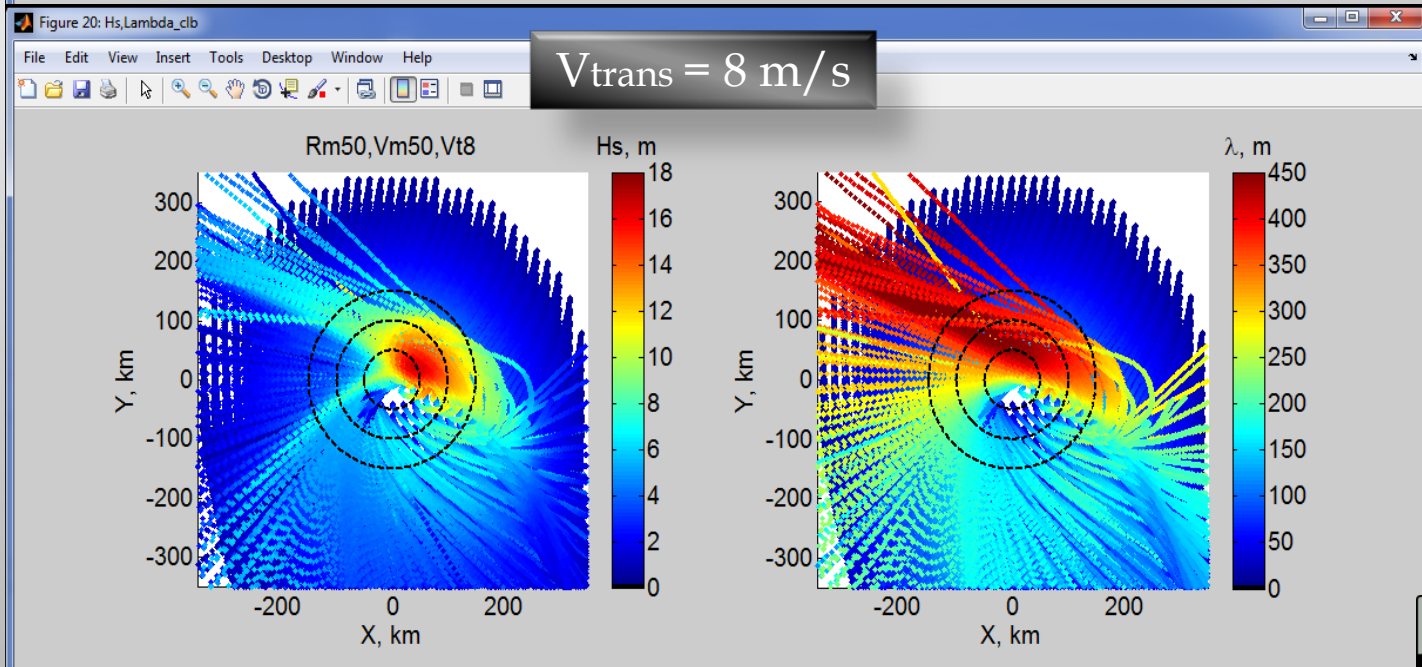
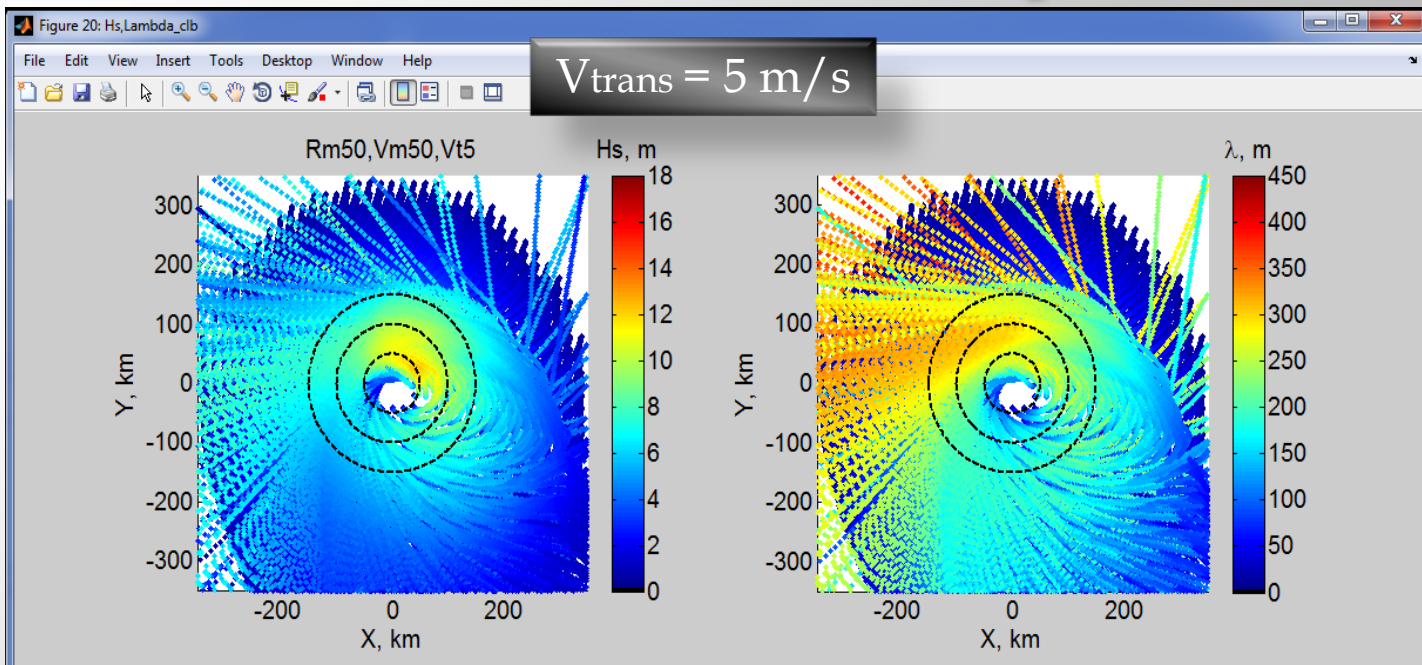
# Wave Parameters from All Trajectories

Hs and wavelength



# Wave Parameters for All Trajectories

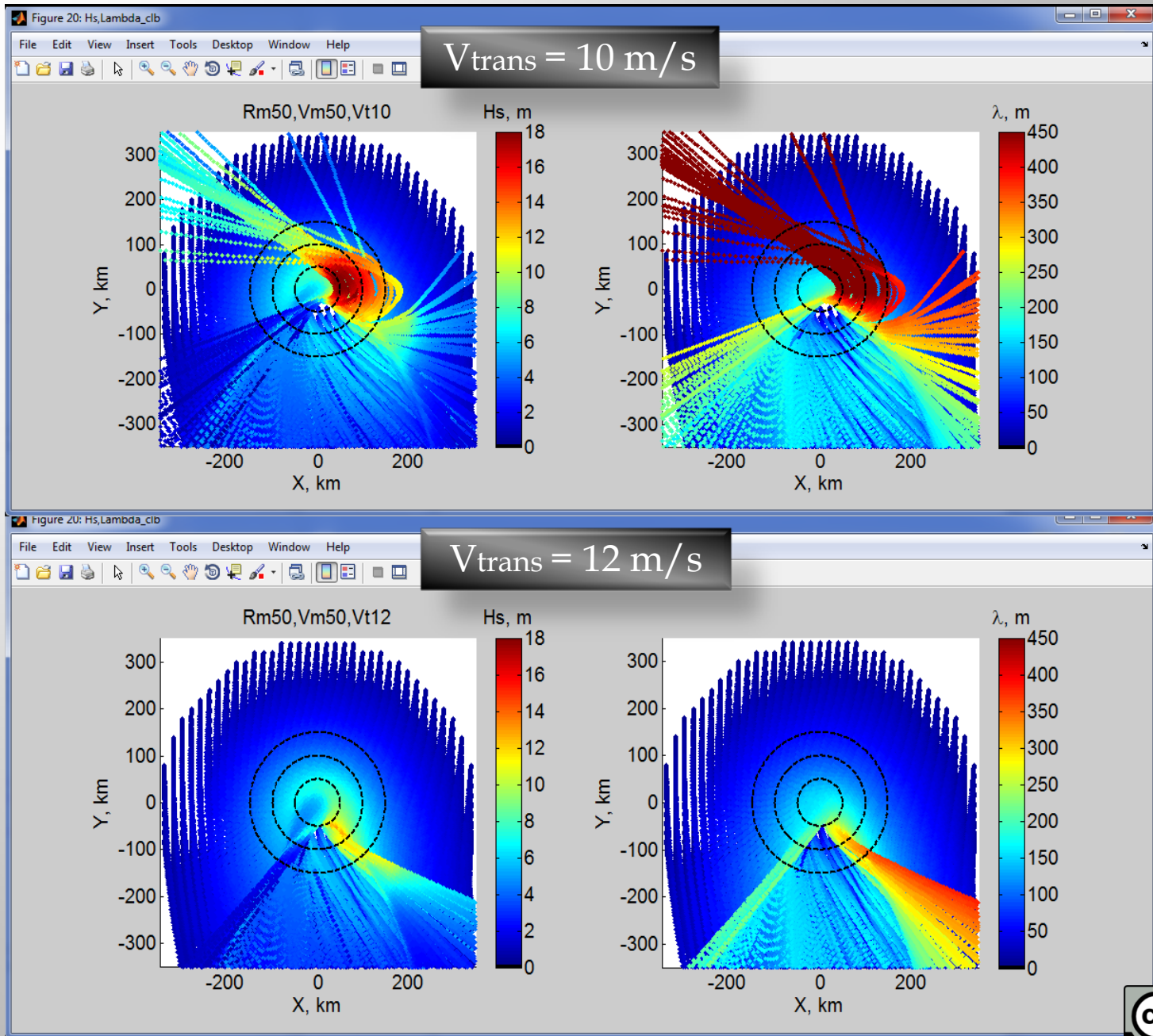
Hs and wavelength





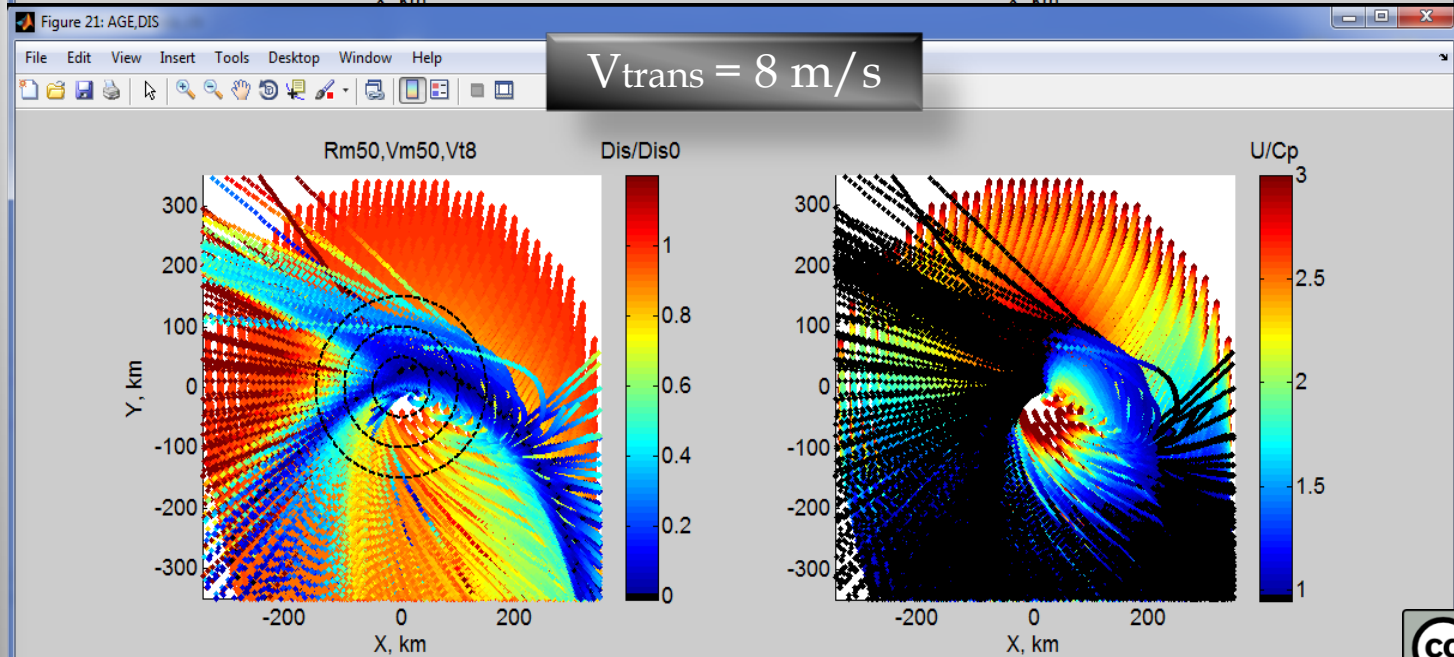
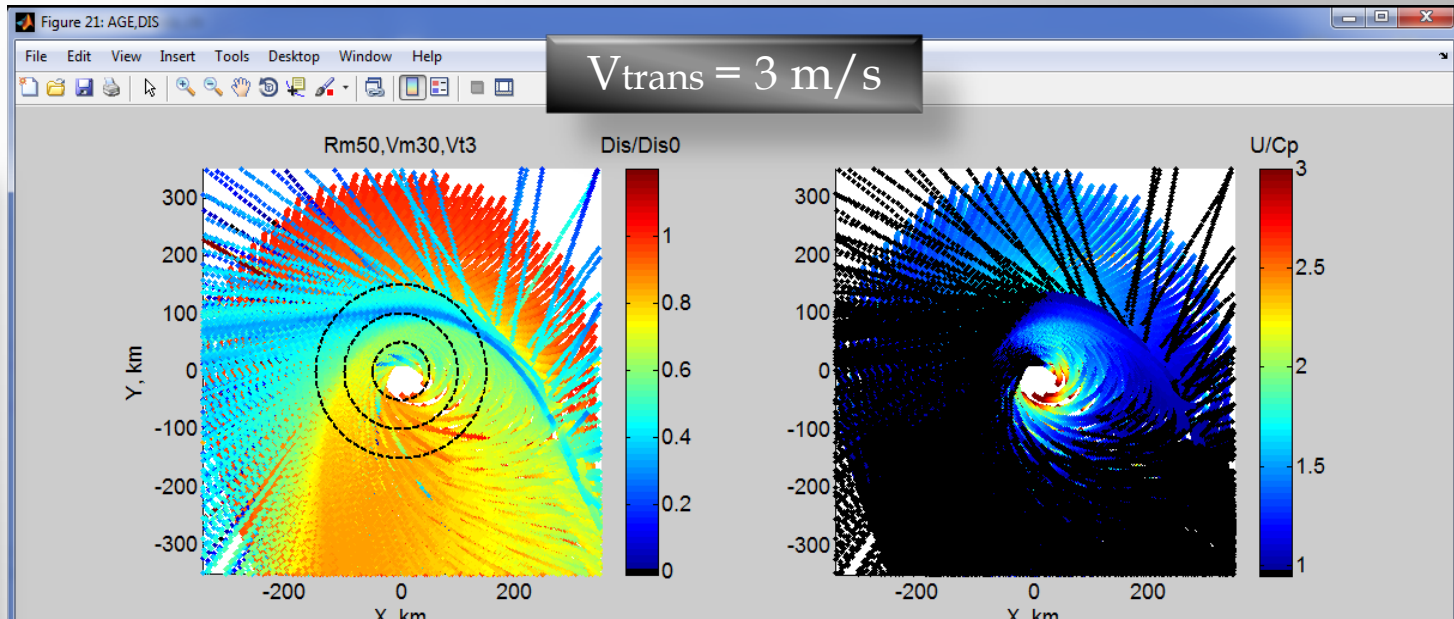
# Wave Parameters for All Trajectories

Hs and wavelength



# Wave Parameters for All Trajectories

Distance between neighbor characteristics (caustic)  
and wave age

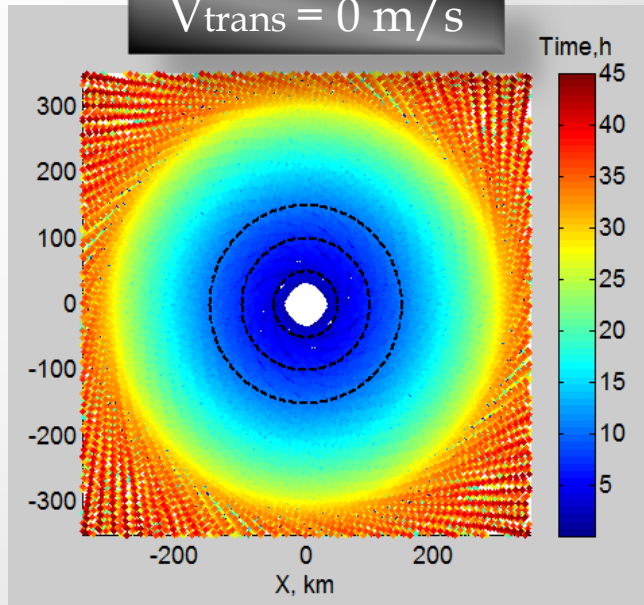




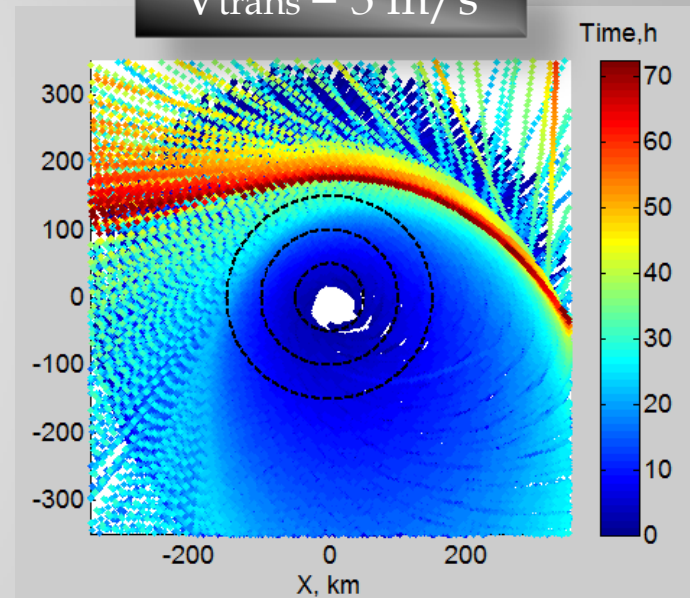
# Wave Parameters for All Trajectories

Time of wave development

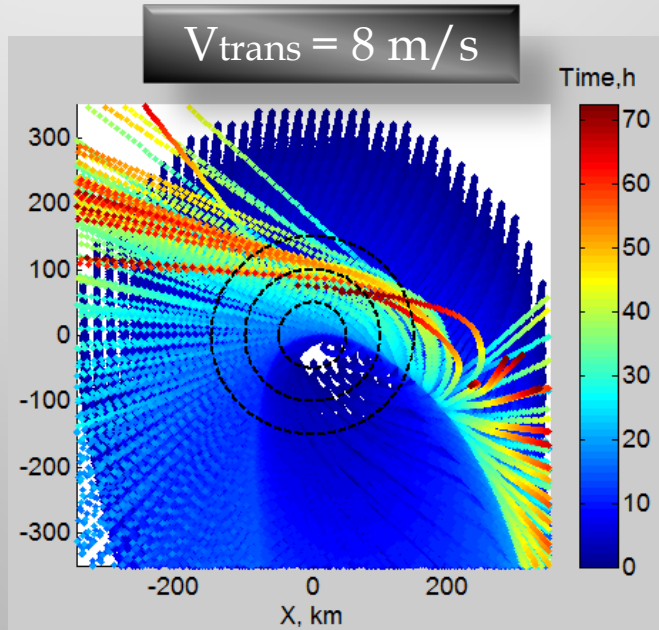
$V_{\text{trans}} = 0 \text{ m/s}$



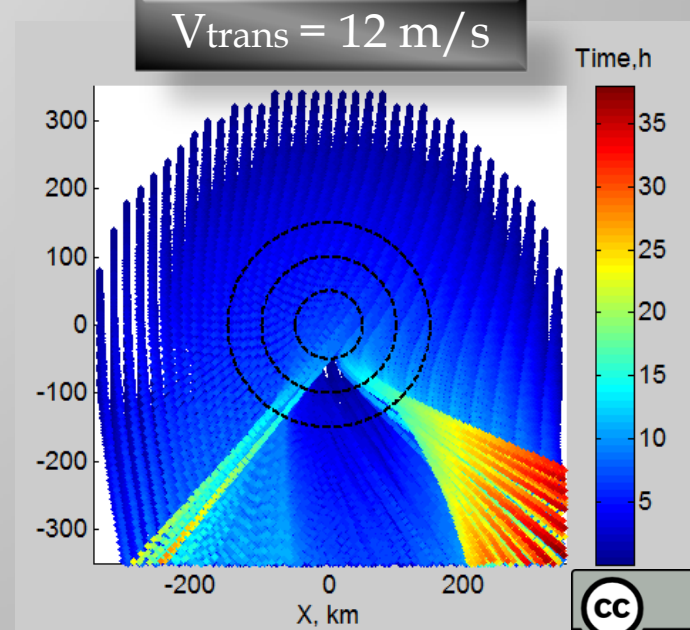
$V_{\text{trans}} = 3 \text{ m/s}$



$V_{\text{trans}} = 8 \text{ m/s}$



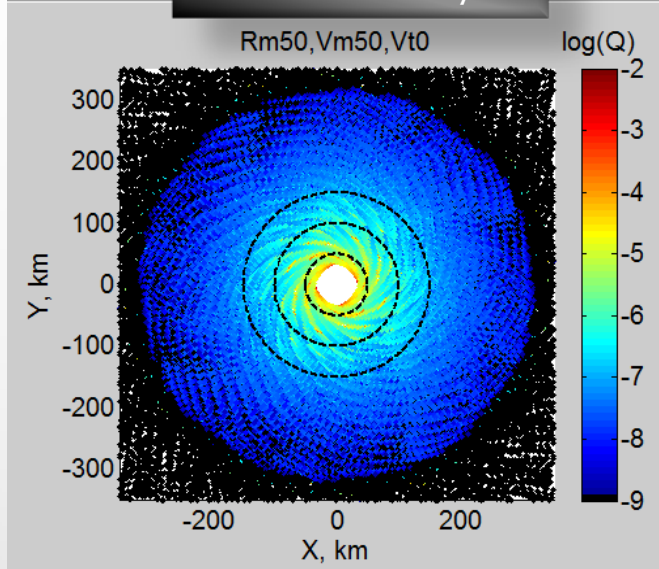
$V_{\text{trans}} = 12 \text{ m/s}$



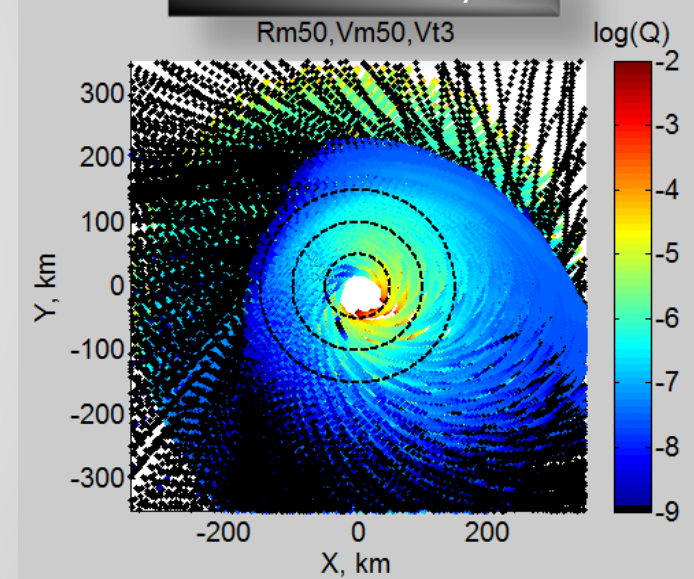
# Wave Parameters for All Trajectories

Wave breaking of peak waves

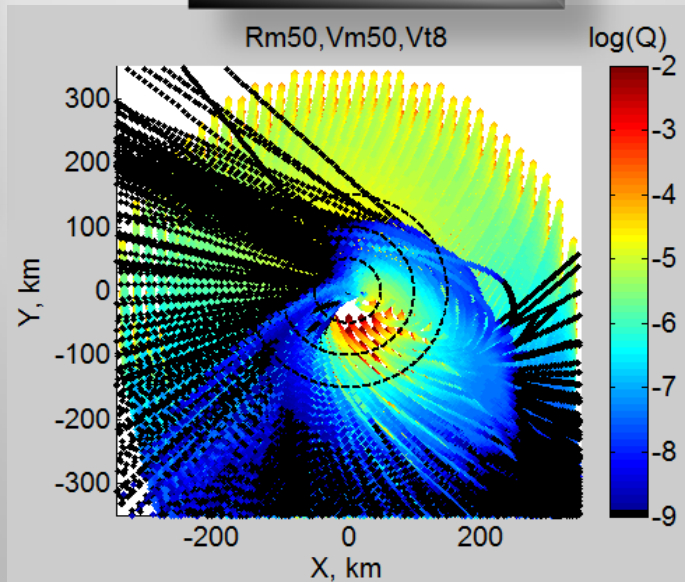
$V_{\text{trans}} = 0 \text{ m/s}$



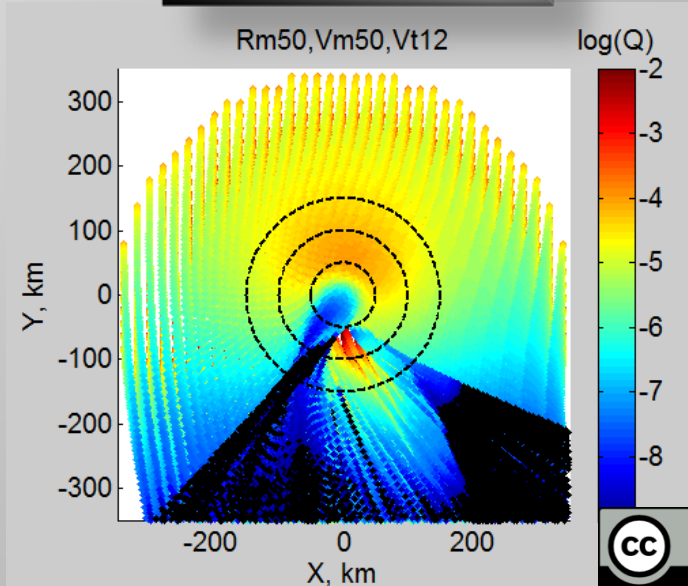
$V_{\text{trans}} = 3 \text{ m/s}$



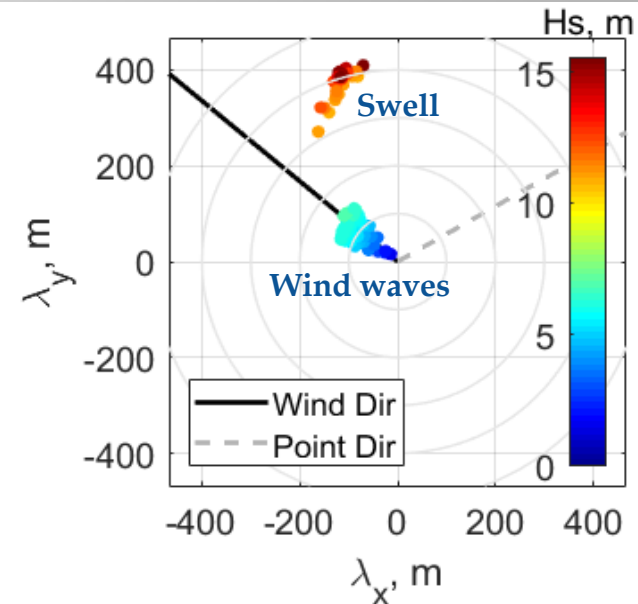
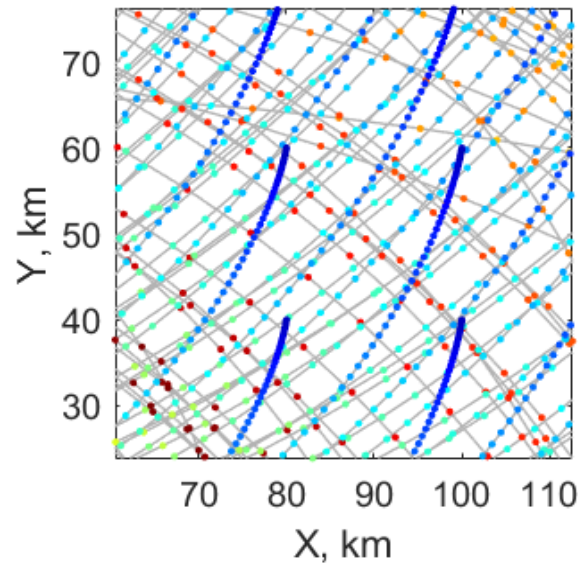
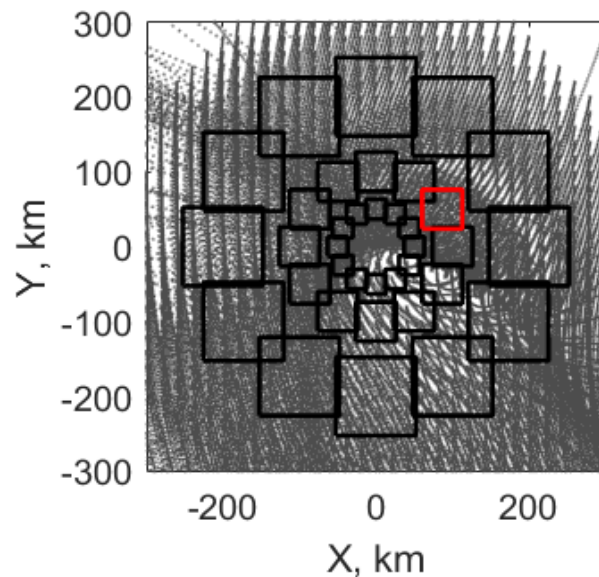
$V_{\text{trans}} = 8 \text{ m/s}$



$V_{\text{trans}} = 12 \text{ m/s}$



# Hs-Wavelength Angular Distributions



$V_{trans}=8\text{m/s}$

Square areas with  $\sim 30^\circ$  angular size are taken at distances  $R_m$ ,  $2R_m$ ,  $4R_m$  from TC center.

Ray trajectories inside one of the areas (red one).

High point concentration corresponds to starting stage of wave development ( $dt$  is small).

Color is  $H_s$ .

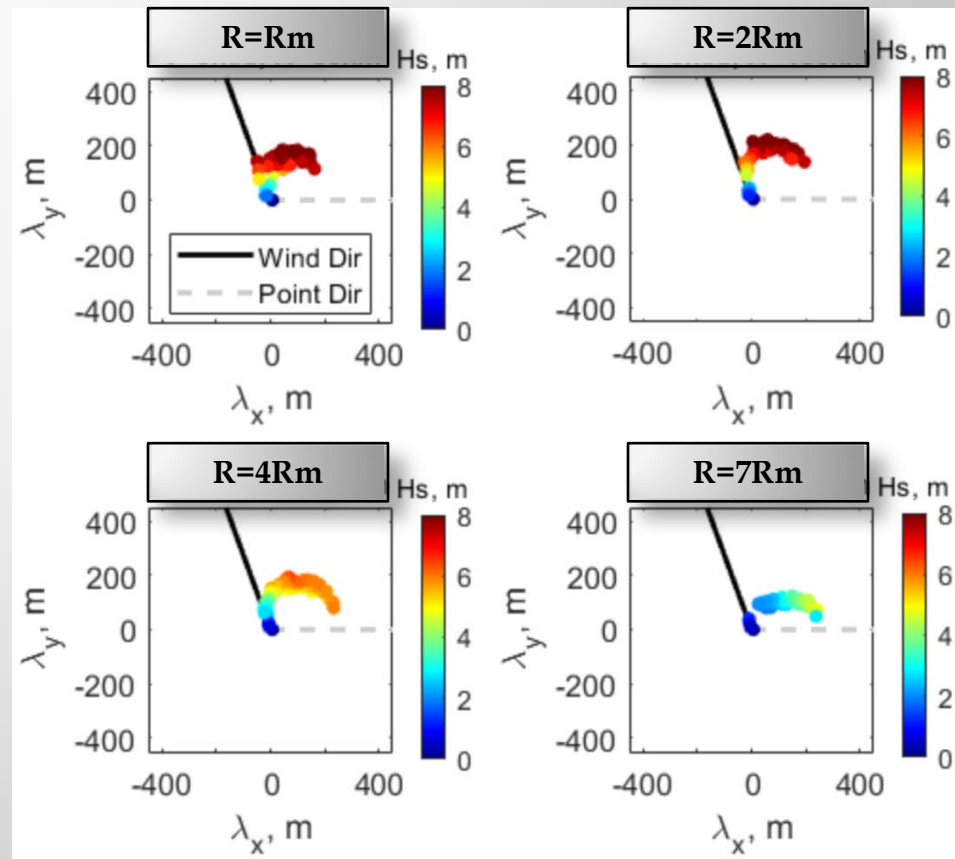
$H_s$  “spectrum”.

Every point is mean  $H_s$  along trajectory part inside square area, in mean wave direction.

**NB** In moving coordinate system, wave peak direction does not coincide with tangent to trajectory!



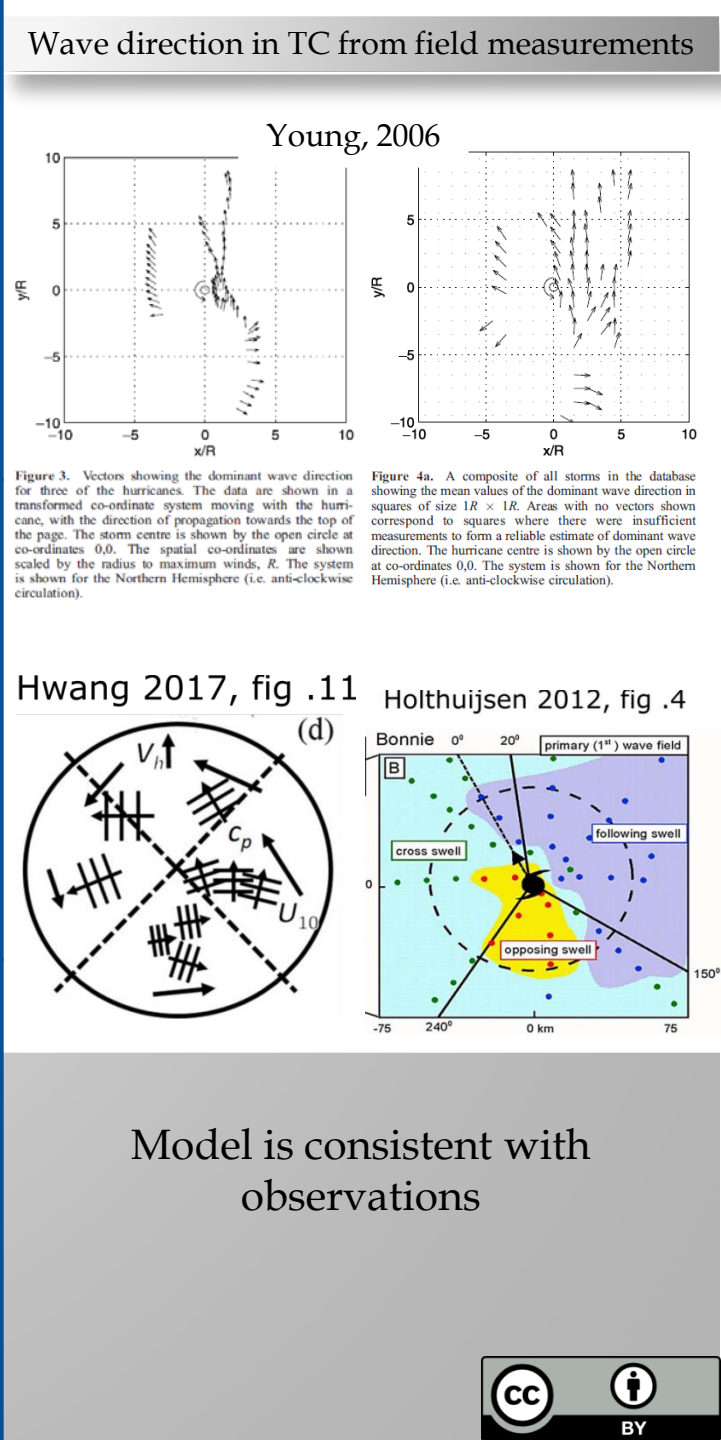
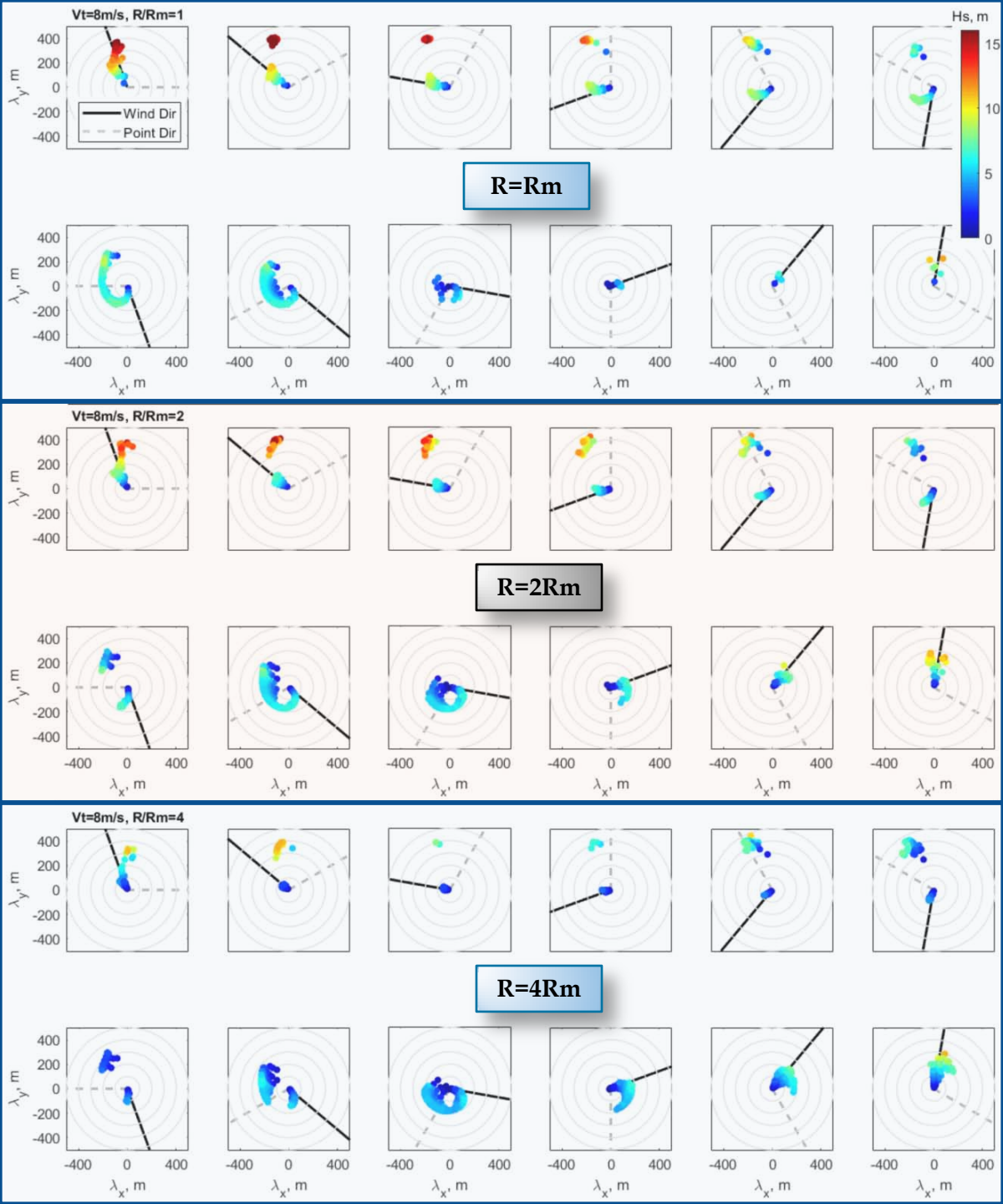
# Hs-Wavelength Angular Distributions In Stationary Cyclone



Distributions are  
“tracing” wave  
evolution

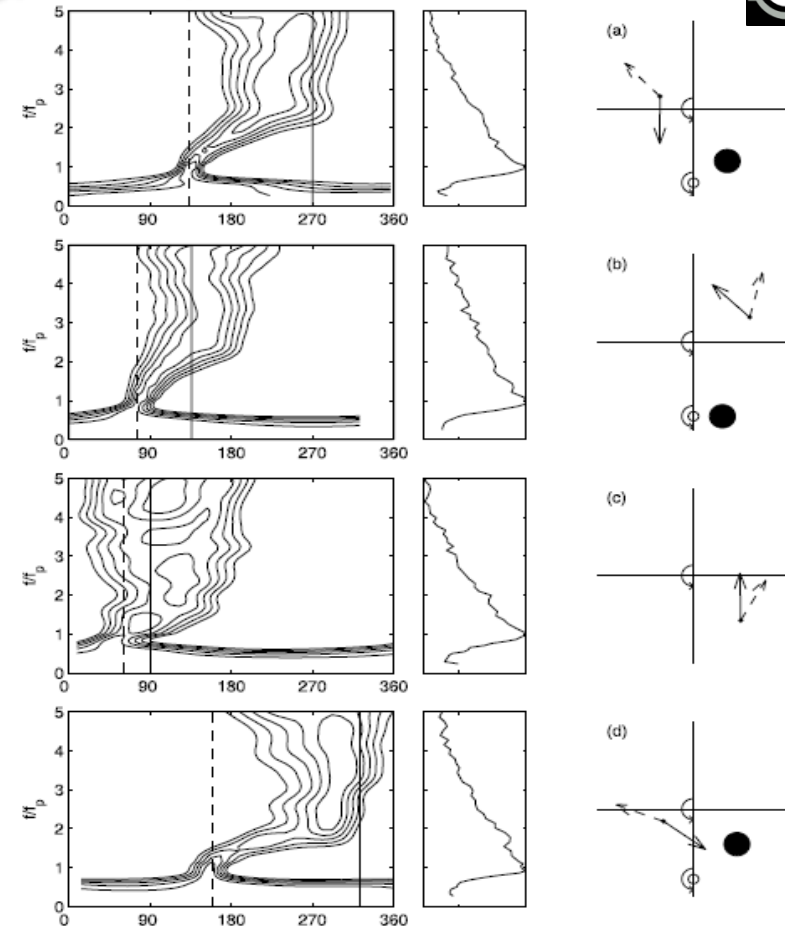
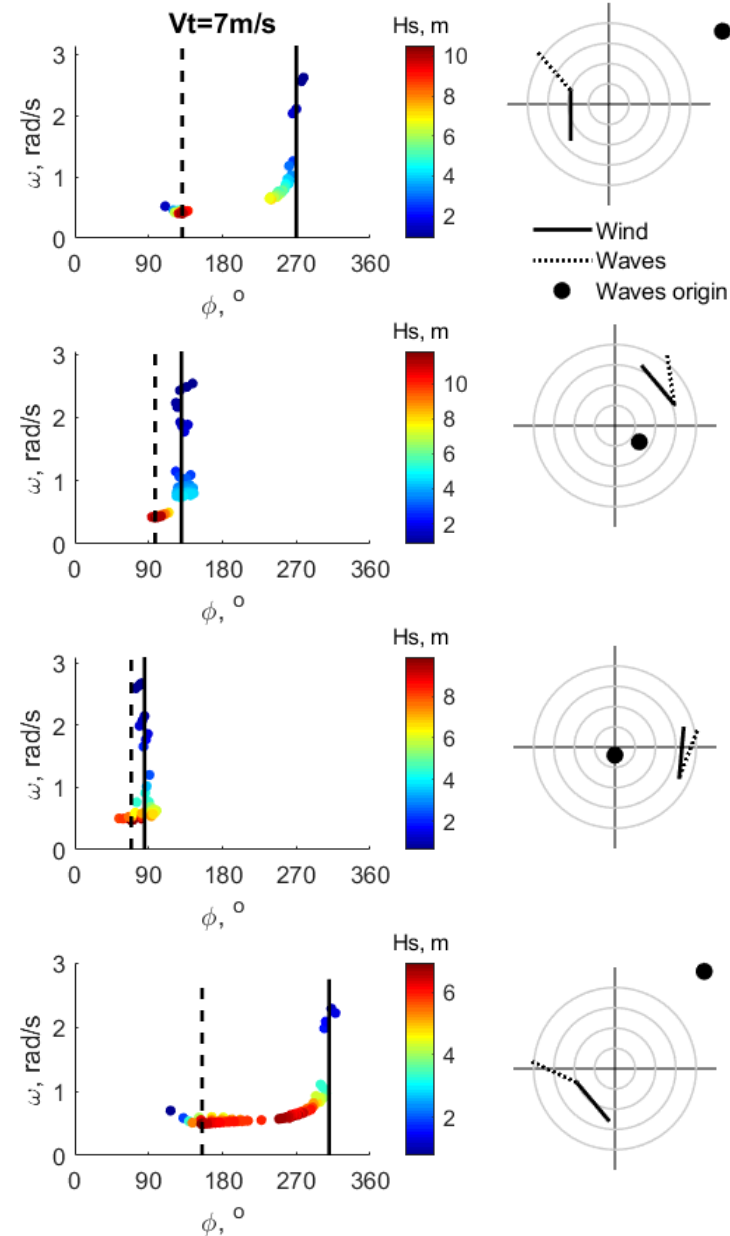
“Spectra” in moving TC







# Wave Angular distribution. Comparison with Buoy Data (Young, 2006)

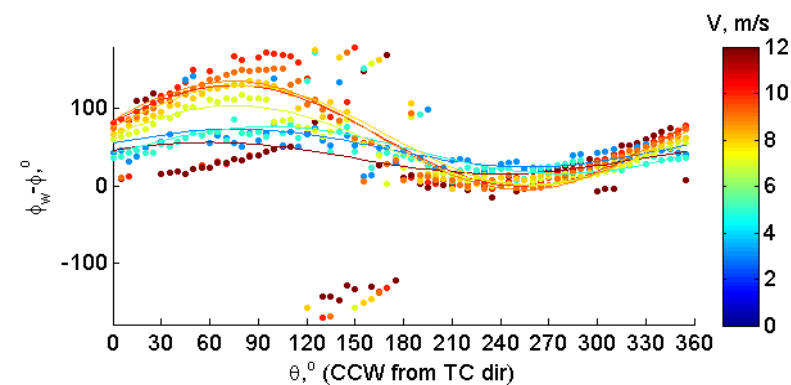
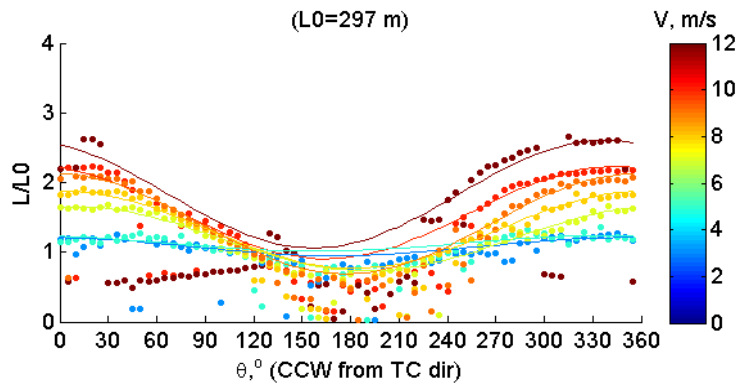
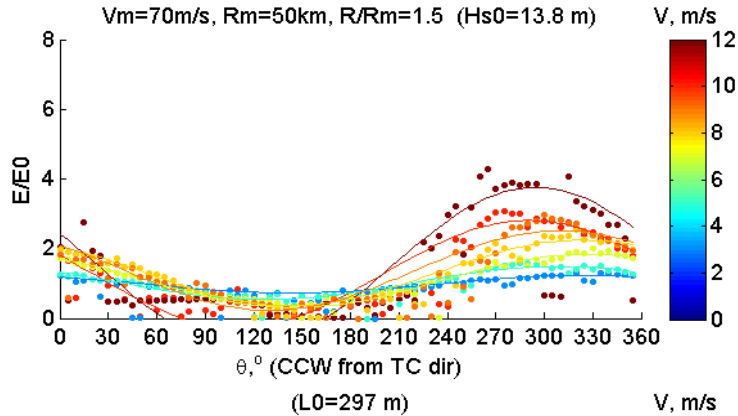


**Figure 5.** Examples of the directional spreading function,  $D(f, \theta)$  for each quadrant of a hurricane. For each quadrant, the panel to the left shows  $D$  contoured in  $f, \theta$  cartesian space. At each frequency,  $D$  has been normalized to have a maximum value of one. Contours are drawn 0.9, 0.8, 0.7, 0.6 and 0.5. The vertical dashed line shows the dominant wave direction and the vertical solid line the local wind direction. To the right of the spreading function the one-dimensional frequency spectrum is shown. For these one-dimensional spectra, the energy scale is logarithmic, with the maximum ordinate being 1.0 and the minimum  $10^{-3}$ . The panels to the extreme right show the corresponding position of the measurement in the quadrant under consideration (small solid dot). The dominant wave direction is shown by the dashed arrow and the local wind direction by the solid arrow. At the time of the measurement, the hurricane is located at the centre of the “cross” shown on the panel. The open circle below the cross shows the estimated position of the centre of the hurricane at the time when the dominant waves at the measurement location were generated. The large solid circle to the right of this point shows the approximate region in which these dominant waves were generated. The system is shown for the Northern Hemisphere (i.e. anti-clockwise circulation).

# Fitting of Wave Parameters

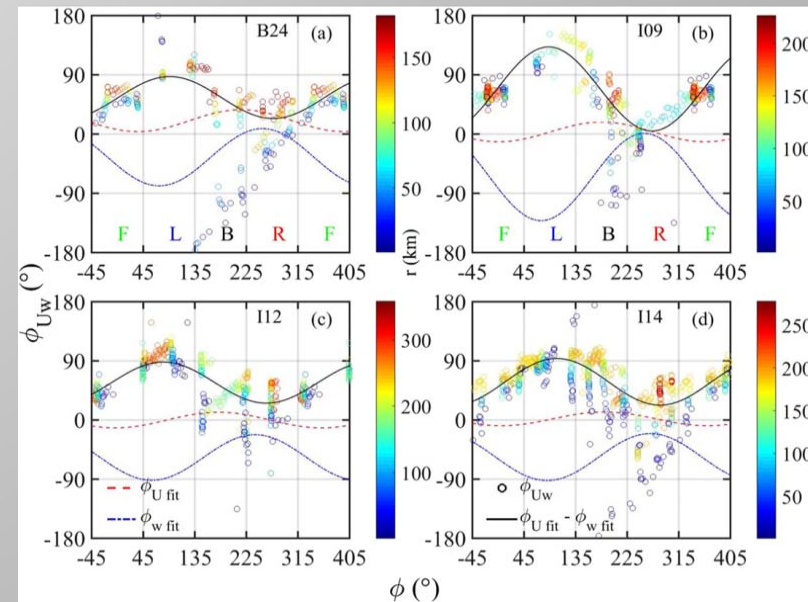
## Fitting example at radius $R=1.5R_m$

$V_m=70\text{m/s}$ ,  $R_m=50\text{km}$ ,  $R/R_m=1.5$  ( $H_s0=13.8\text{ m}$ )

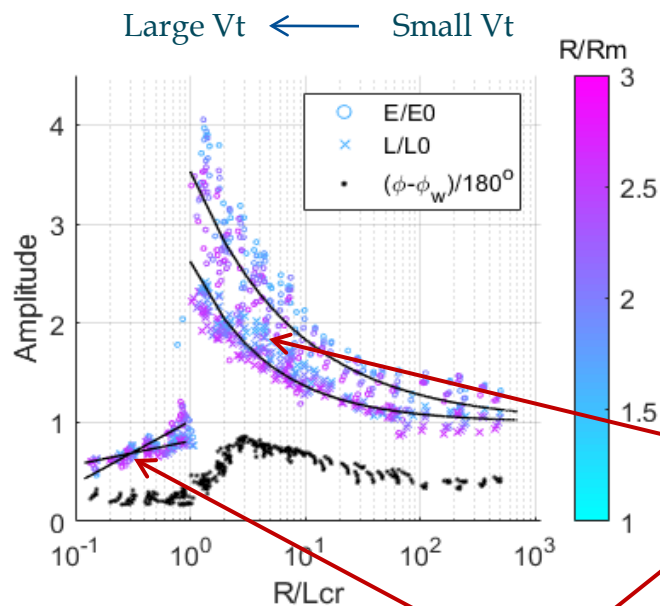


Wave energy, wavelength and wave direction at different distances from TC center are fitted with **cosine** functions for all considered cases (different TC radii,  $U_{max}$  and translation speed)

Hwang 2017, fig .8



# Parameterization of Fitting Functions



Magnitude (A) and location (P) of fitting function's maxima **vs** dimensionless parameter:

$$Xd = R / Lcr$$

$$Lcr = -qc_a^{-1/q} (U^2 / g)(U / 2V_t)^{1/q} / (1 + q)$$

**Two regimes:**

1. Slow TC ( $X_d > 1$ ):

$$AE1 = 1 + 2.3 * X_d.^{-0.46}$$

$$AL1 = 1 + 1.4 * X_d.^{-0.62}$$

$$PE1 = 8.5 * \log(X_d) + 293$$

$$PL1 = 19 * \log(X_d) + 340$$

2. Fast TC ( $X_d < 1$ ),

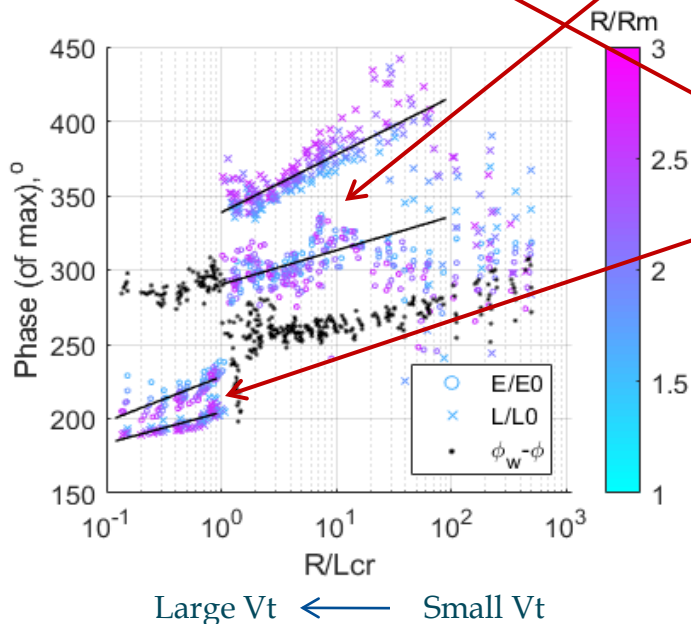
$V_t \gg C_p$ , waves are not trapped:

$$AE2 = 0.26 * \log(X_d) + 1.03$$

$$AL2 = 0.093 * \log(X_d) + 0.815$$

$$PE2 = 12 * \log(X_d) + 229$$

$$PL2 = 8.7 * \log(X_d) + 205$$



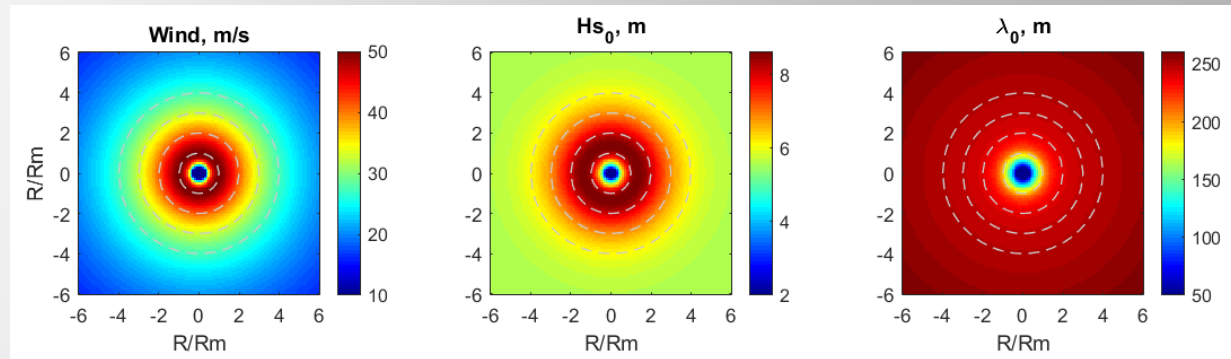
# TC Reconstruction from Analytical Functions

Parameters of stationary cyclone ( $R_m=50$  km,  $U_m=50$  m/s)

**Wind:** Holland, 1980

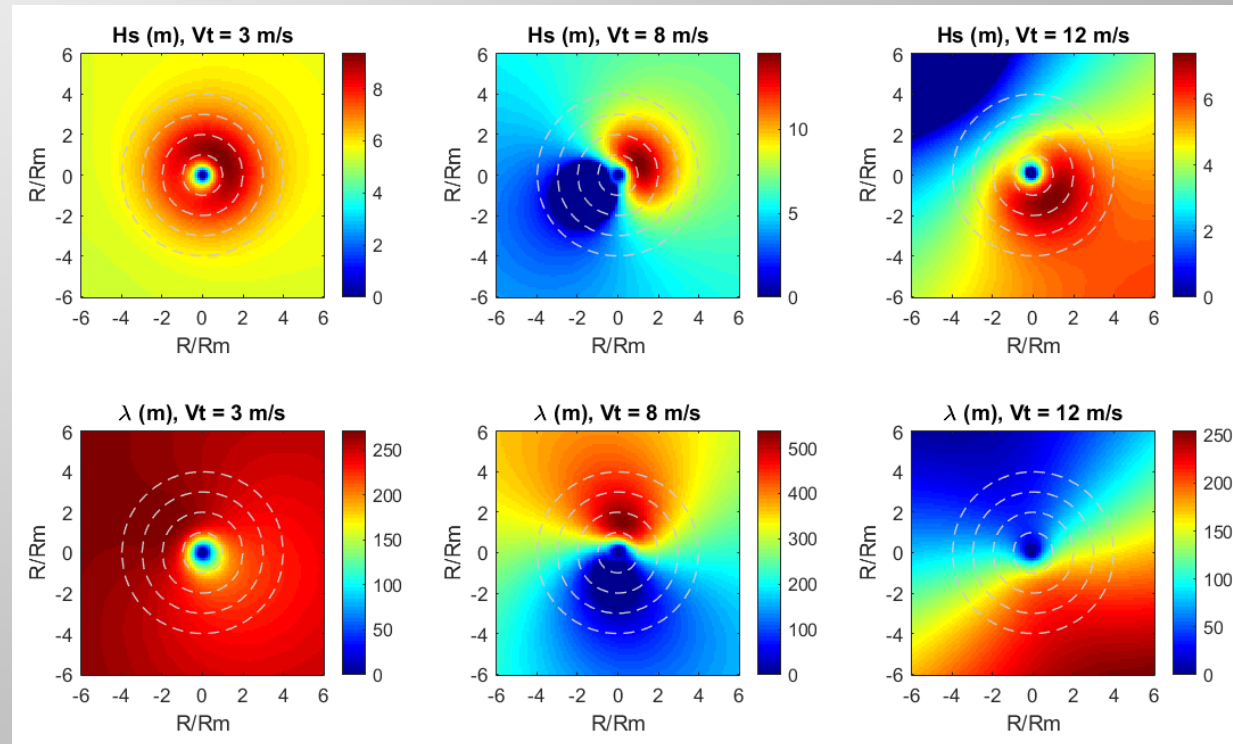
**Stationary cyclone:**  $H_s$  and wavelength from 1D fit

**Moving TC:** angular distributions from parameterized cosine functions (depend on  $R_m$ ,  $U_m$ ,  $V_t$  and distance from TC center)



Example of TC reconstruction for  $V_{trans}=3, 8, 12$  m/s

$V_{trans}$





- ▣ A model for waves development and propagation under spatially and time varying winds, is suggested.
- ▣ The model is based on energy and momentum conservation laws. Wind energy input and wave breaking dissipation are the main sources to govern the wave energy conservation equation, while non-linear interactions are essential to control the peak frequency downshift of the energy-containing part of the spectrum.
- ▣ 1D self-similar fetch-laws are used to derive fully consistent parametric solutions for 2D surface wave development.
- ▣ Calculations were carried out for the case of the uniform wind field and for an inhomogeneous cyclonic wind field with different hurricane translation velocities.
- ▣ The calculations reproduce the anisotropy of the energy distribution inside the hurricane and the effect of wave trapping by a moving cyclone.
- ▣ As shown, varying winds can lead to the divergence of group velocities (focusing/ defocusing wave groups), to significantly affect the energy balance.
- ▣ The results are in line with field measurements and existing knowledge about TC dynamics
- ▣ The model can provide practical means to rapidly map and assess the energy, frequency and peak wave direction distributions. Applications can serve to provide prior-information to analyze high-resolution satellite measurements and to improve remote sensing algorithm developments.





Thank you for  
your attention!



BY