

# A new furnace design to improve the thermal demagnetization in paleomagnetism

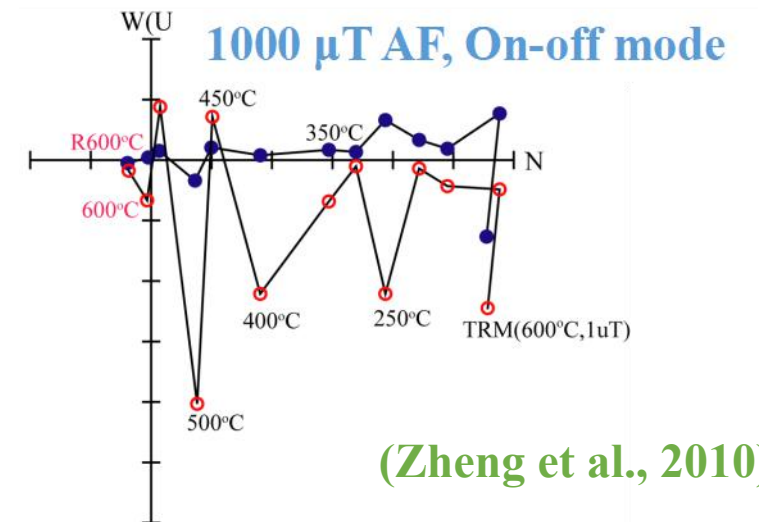
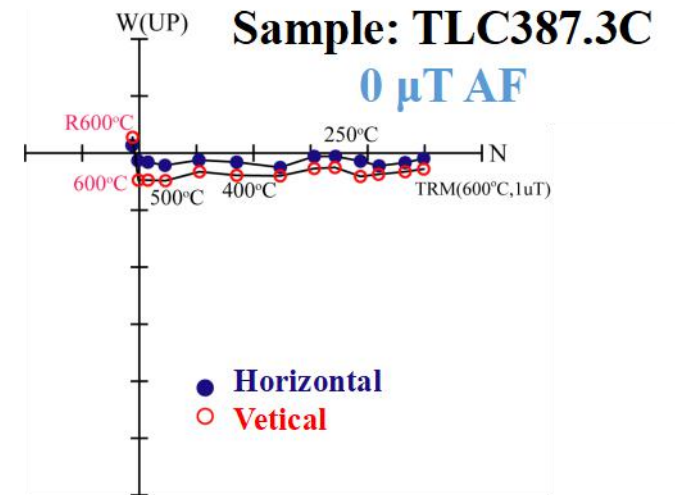
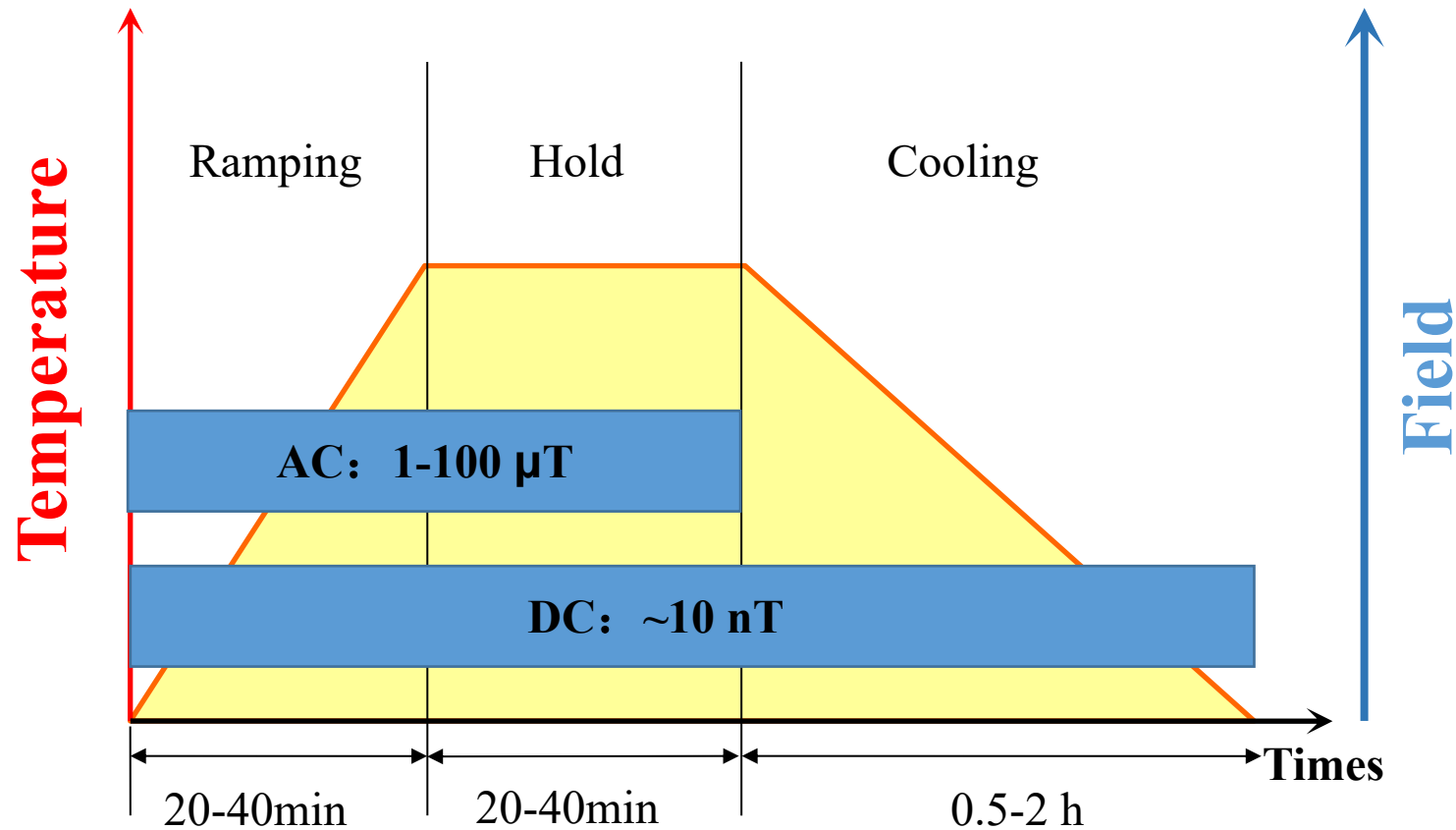
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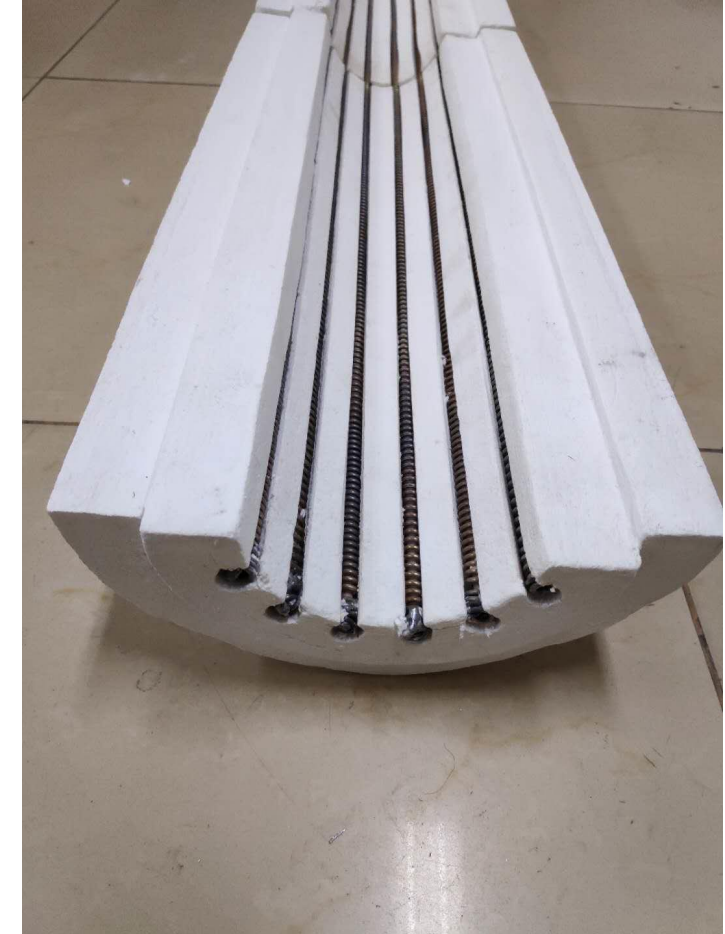
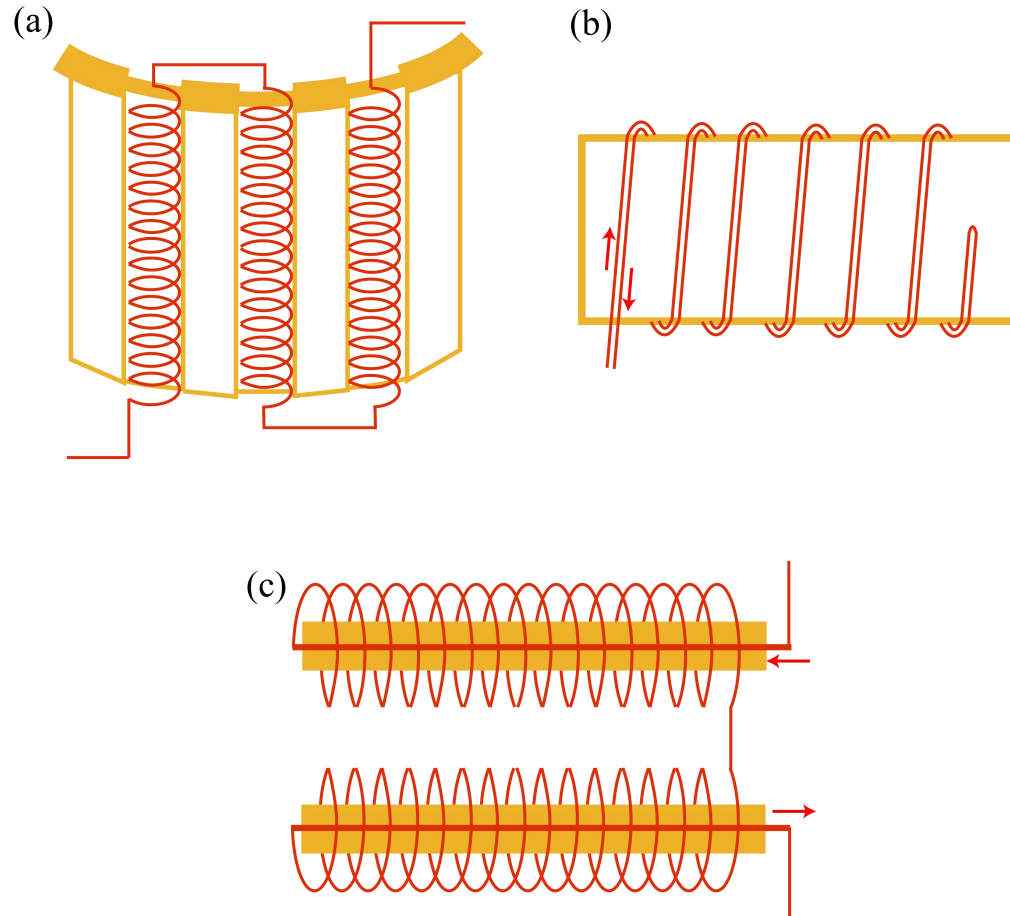
# Imperfect thermal demagnetization



(Zheng et al., 2010)

The samples should be in **zero magnetic field** during thermal demagnetization. However, magnetic field noise, including residual magnetic fields of material and induced fields caused by the heating current in the furnace are always present.

# Configuration of non-inductive heating wires



solenoids arranged in opposite direction (a), a bifilar solenoid wrapped (b) and new heating element made by solenoid and connected with a straight wire in series at one end for new developed demagnetizing furnace (c).

# Simulation of solenoid magnetic field

**Solenoid:**

$$dB_x = \frac{\mu_0 I}{4\pi} \frac{[(z_0 - a\theta)R \cos\theta - (y_0 - R \sin\theta)a]d\theta}{[(x_0 - R \cos\theta)^2 + (y_0 - R \sin\theta)^2 + (z_0 - a\theta)^2]^{3/2}}$$

$$dB_y = \frac{\mu_0 I}{4\pi} \frac{[(z_0 - a\theta)R \sin\theta + (x_0 - R \cos\theta)a]d\theta}{[(x_0 - R \cos\theta)^2 + (y_0 - R \sin\theta)^2 + (z_0 - a\theta)^2]^{3/2}}$$

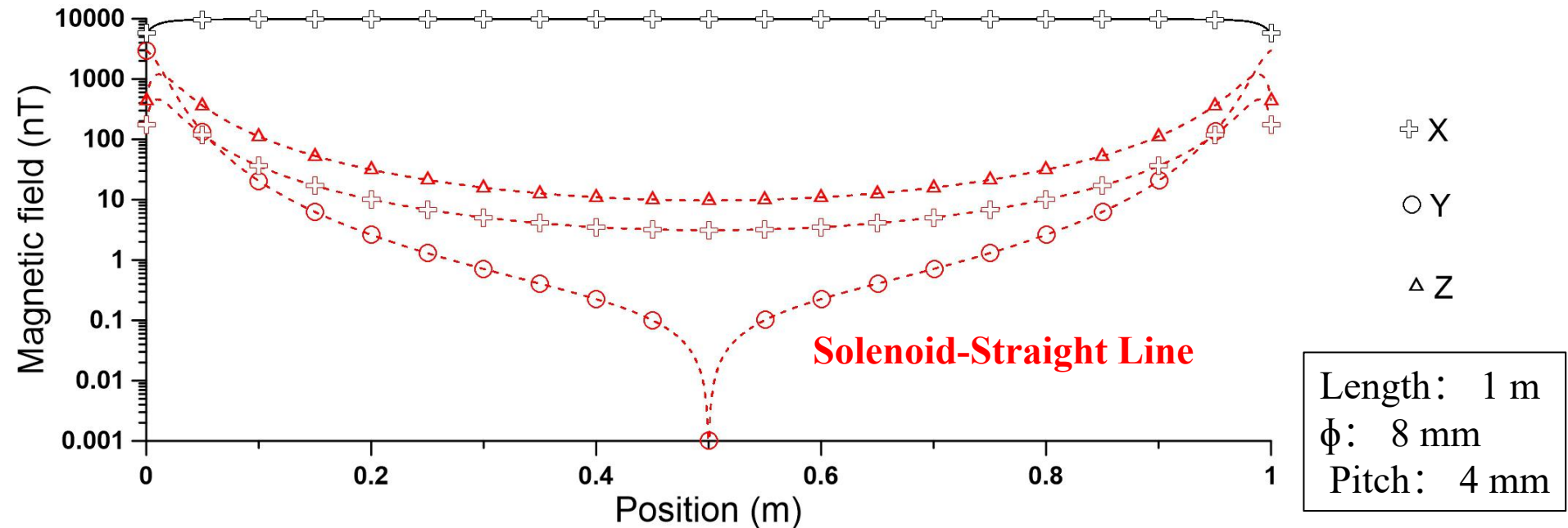
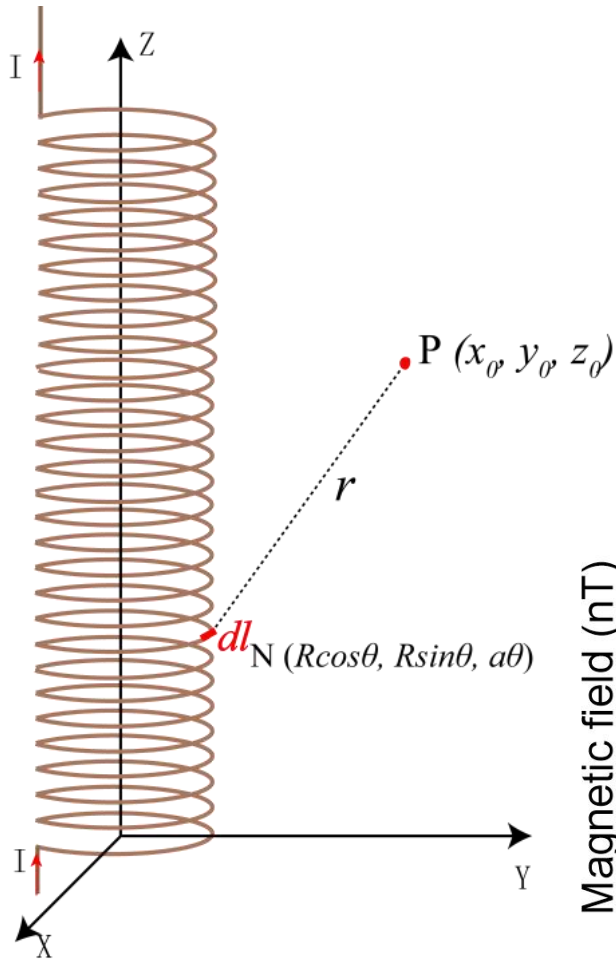
$$dB_z = -\frac{\mu_0 I}{4\pi} \frac{[(y_0 - R \sin\theta)R \sin\theta + (x_0 - R \cos\theta)R \cos\theta]d\theta}{[(x_0 - R \cos\theta)^2 + (y_0 - R \sin\theta)^2 + (z_0 - a\theta)^2]^{3/2}}$$

**Straight Line:**

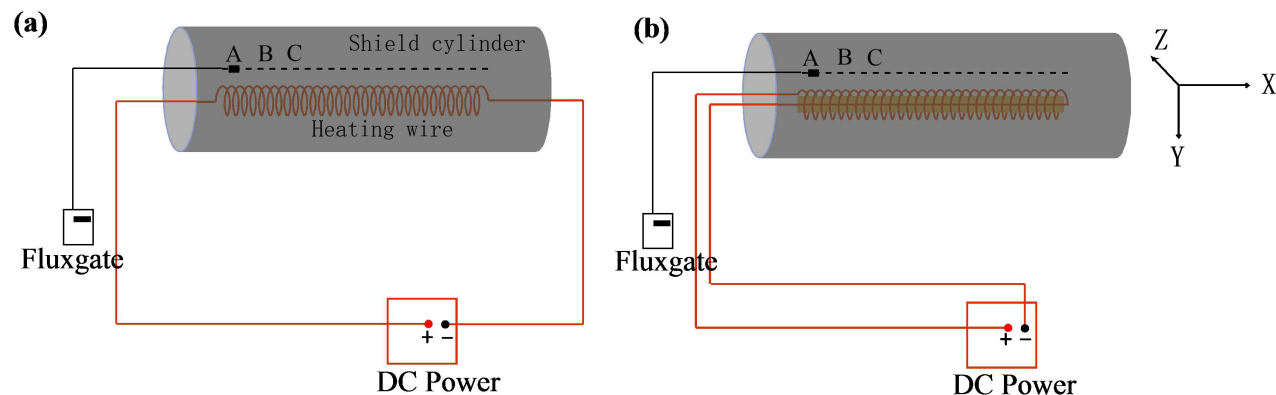
$$dB_x = -\frac{\mu_0 I}{4\pi} \frac{y_0 a d\theta}{[x_0^2 + y_0^2 + (z_0 - a\theta)^2]^{3/2}}$$

$$dB_y = -\frac{\mu_0 I}{4\pi} \frac{x_0 a d\theta}{[x_0^2 + y_0^2 + (z_0 - a\theta)^2]^{3/2}}$$

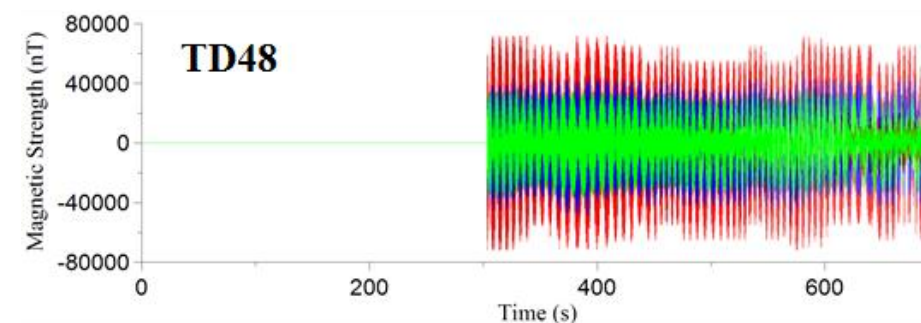
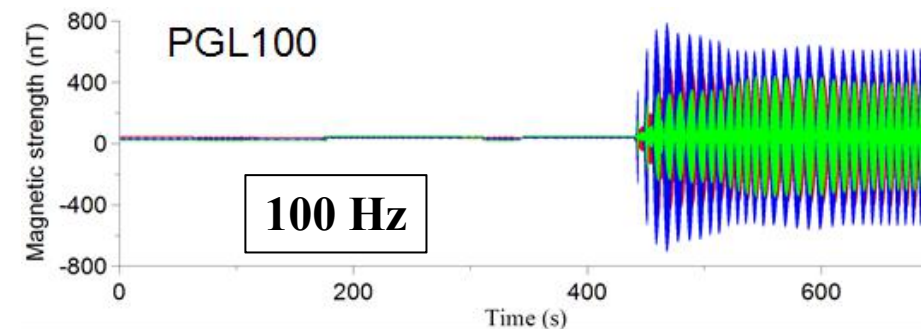
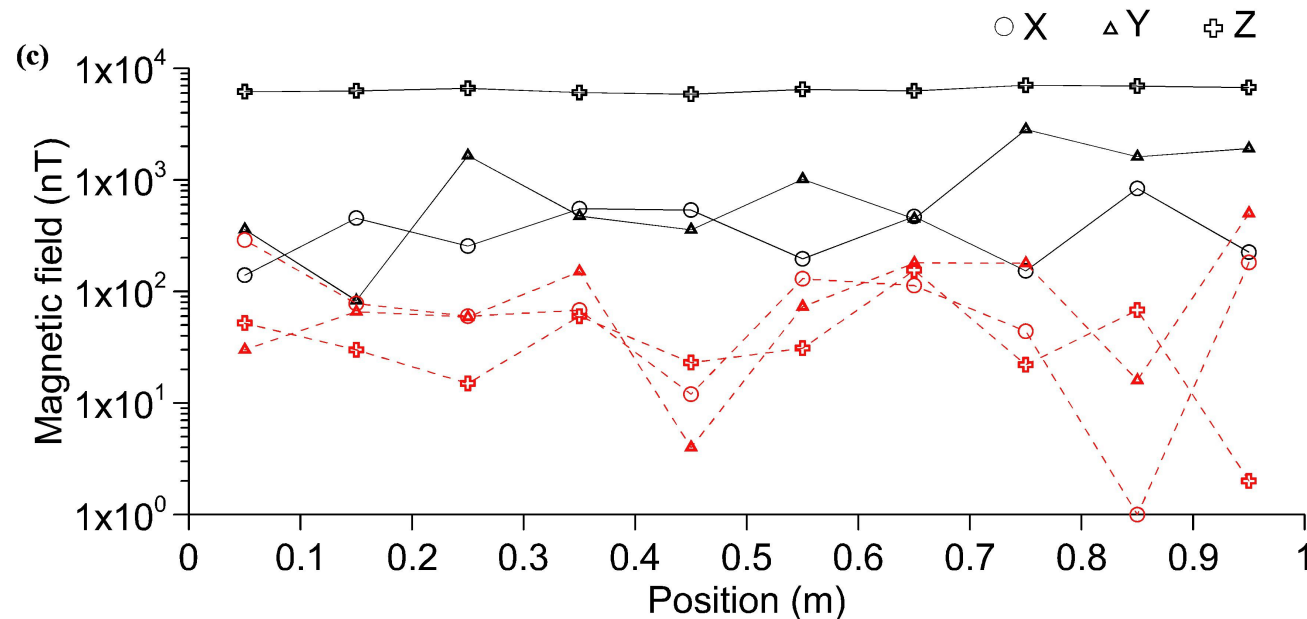
$$dB_z = 0$$



# Magnetic field measurement

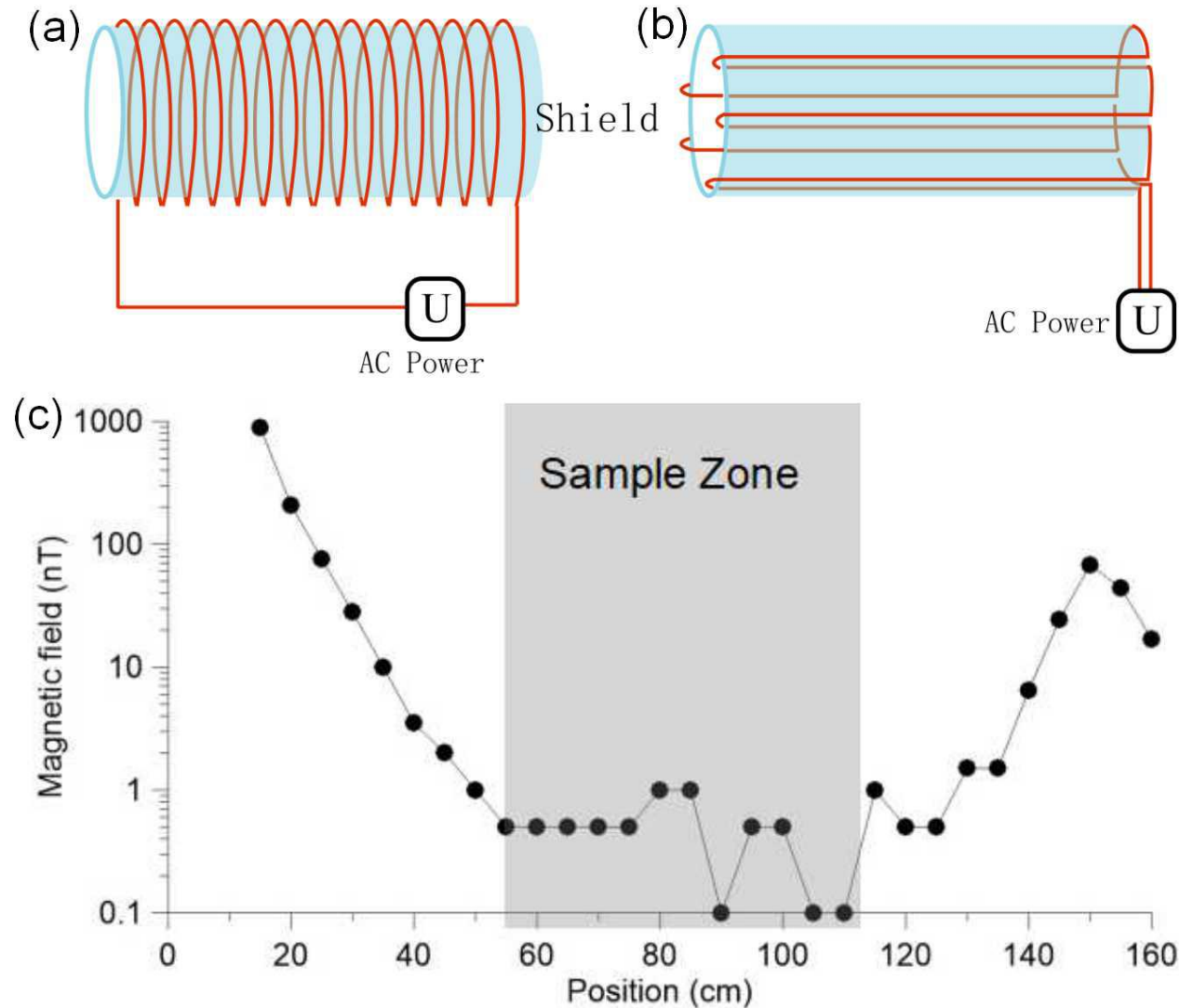


Model	Induce field (nT/A)
Sogo-fine-TD	260
ASC-TD48	9260
MMTD80	840
<b>TD-PGL100</b>	<b>130</b>



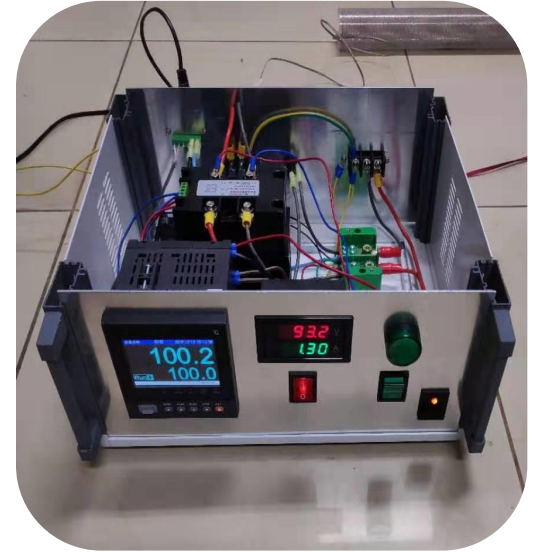
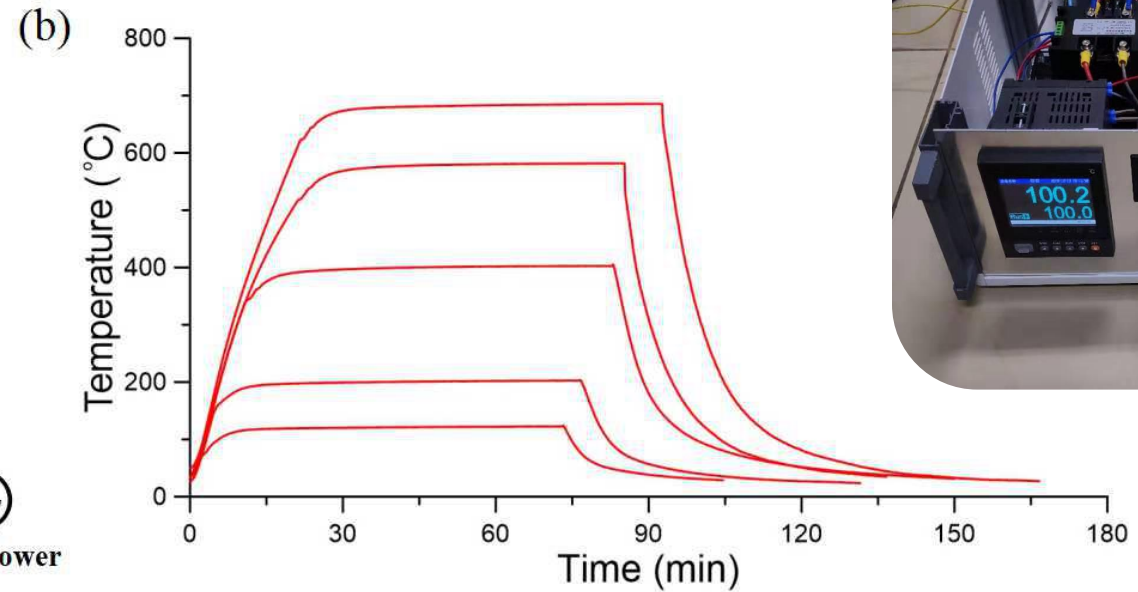
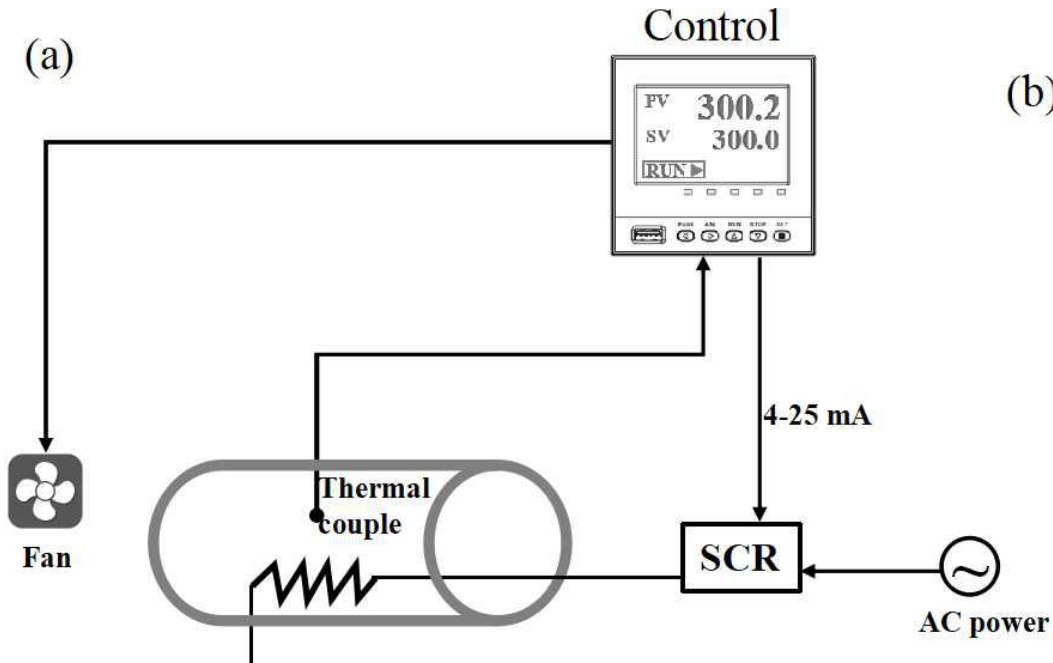


# Degaussing the shield cylinder



A solenoidal (a) and toroidal (b) degaussing coil embody the shield cylinder, and residual field in in shielding cylinder after demagnetization (c) with winding method according to figure (b). After demagnetization with this procedure, the residual magnetic field in the sample region can be less than 1 nT .

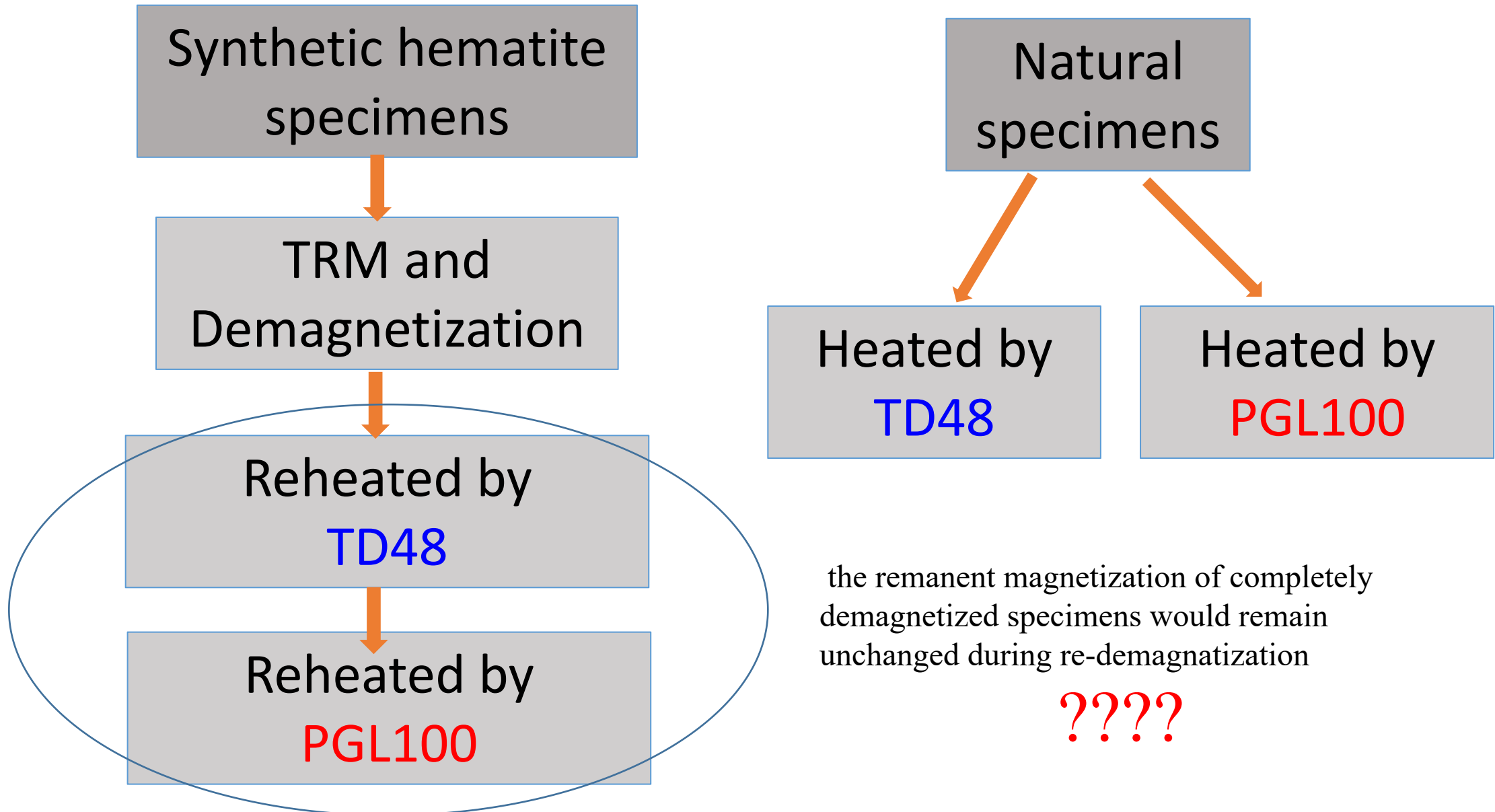
# Temperature control



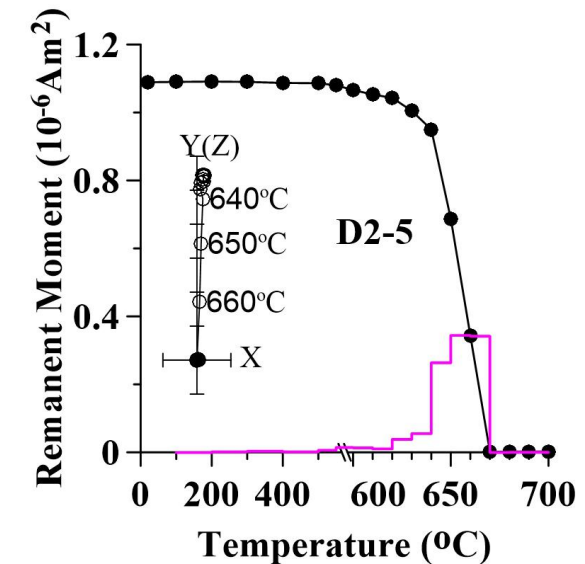
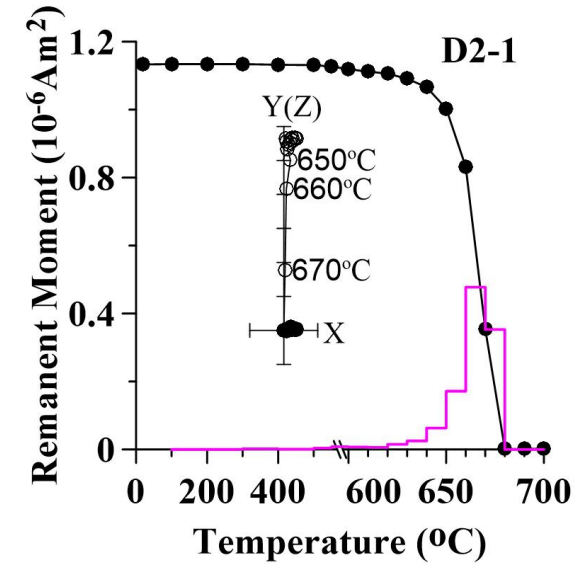
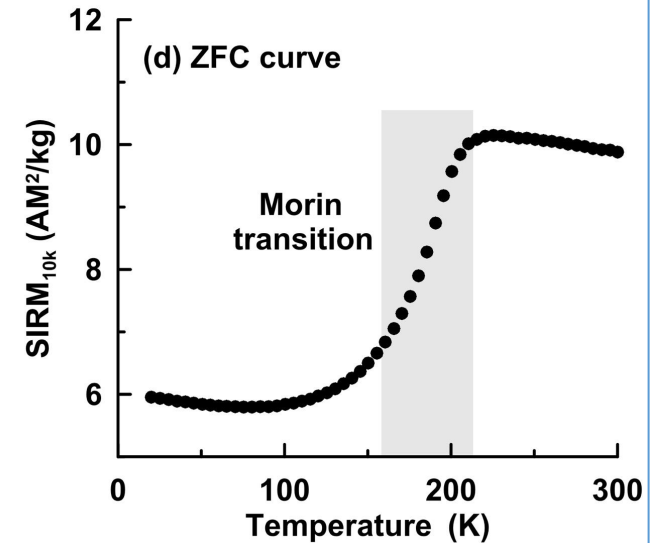
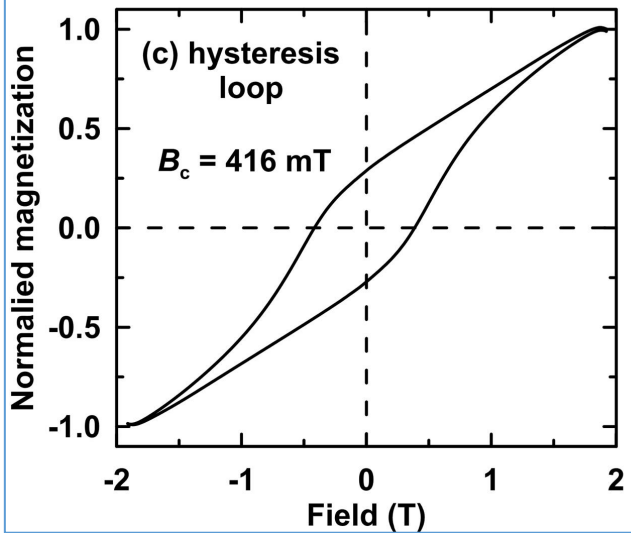
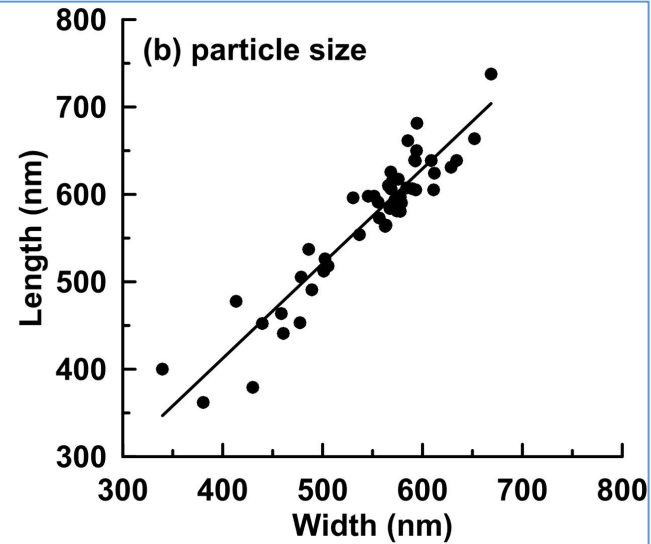
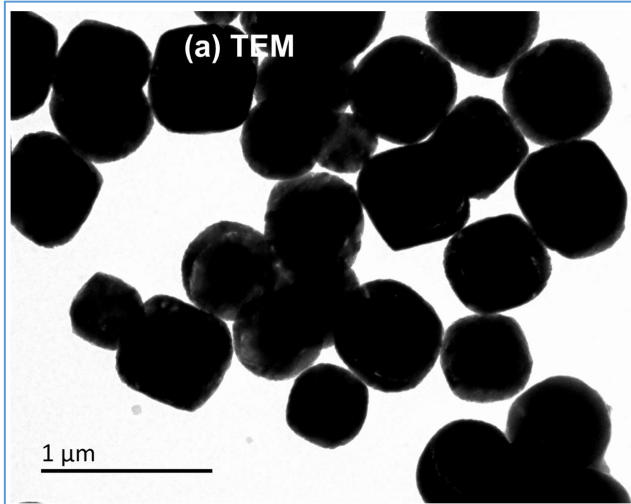
The heating current can be adjusted by Single-phase Voltage Module, which can reduce the current when approaching the target temperature. Its advantage is to ensure temperature stability and reduce the induced magnetic field. The temperature of heating process can be recorded in USB memory.



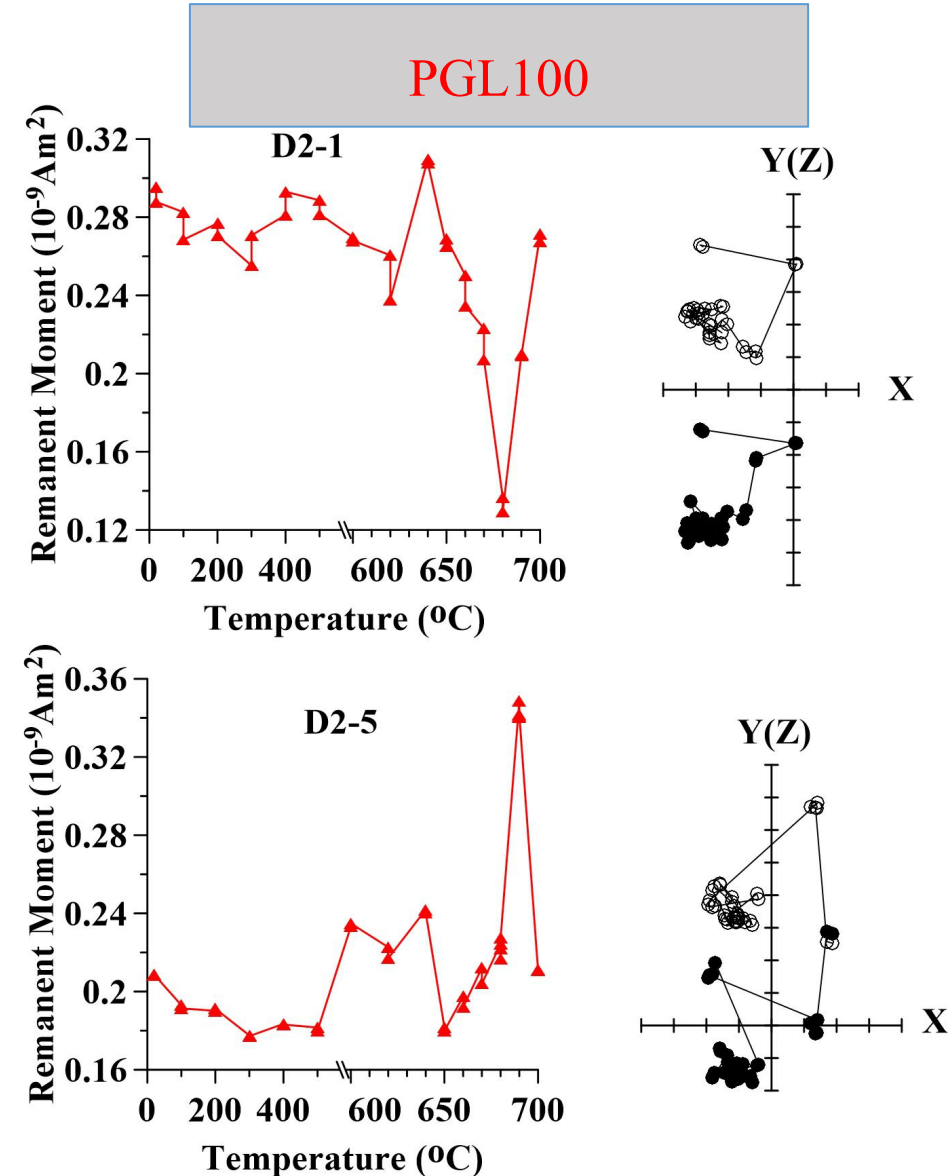
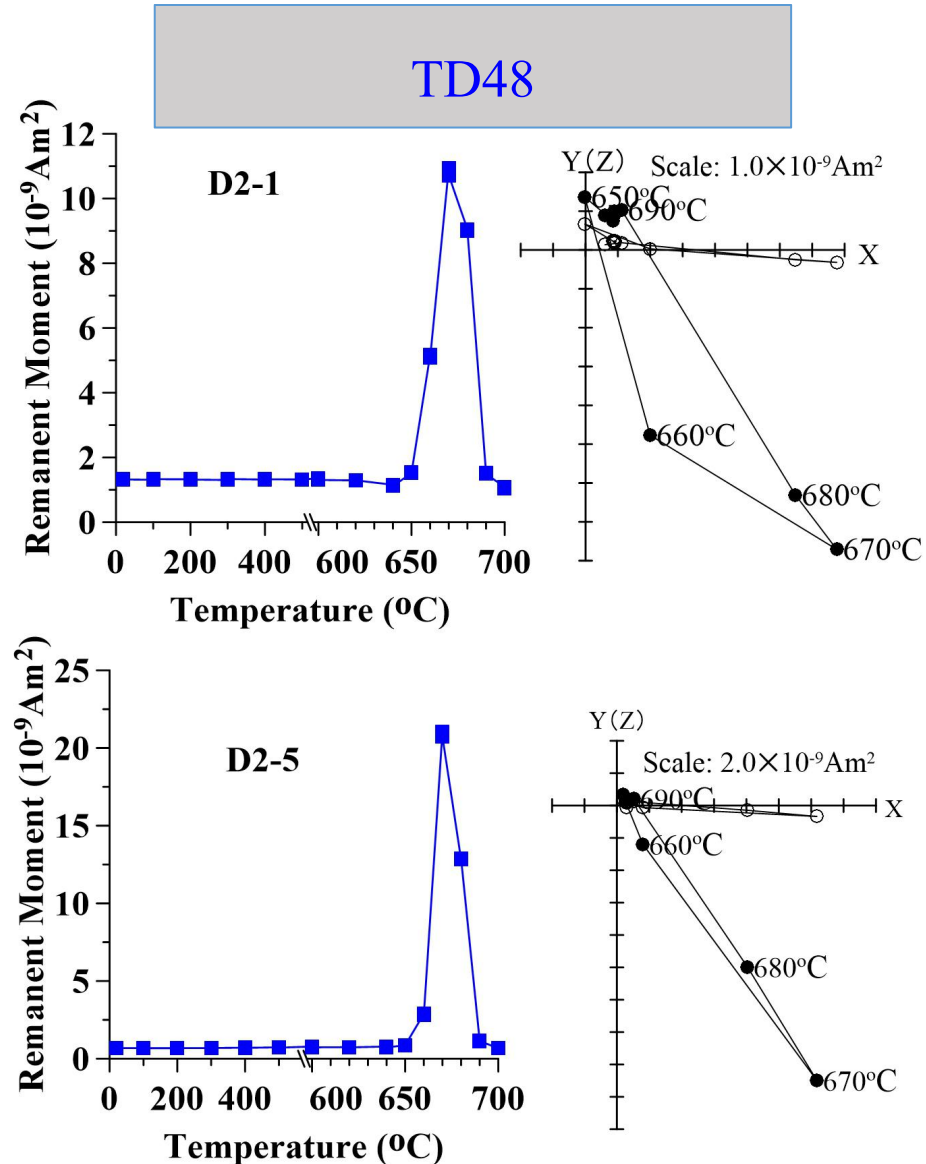
# Experimental Method



# Specimen and Demagnetization of TRM

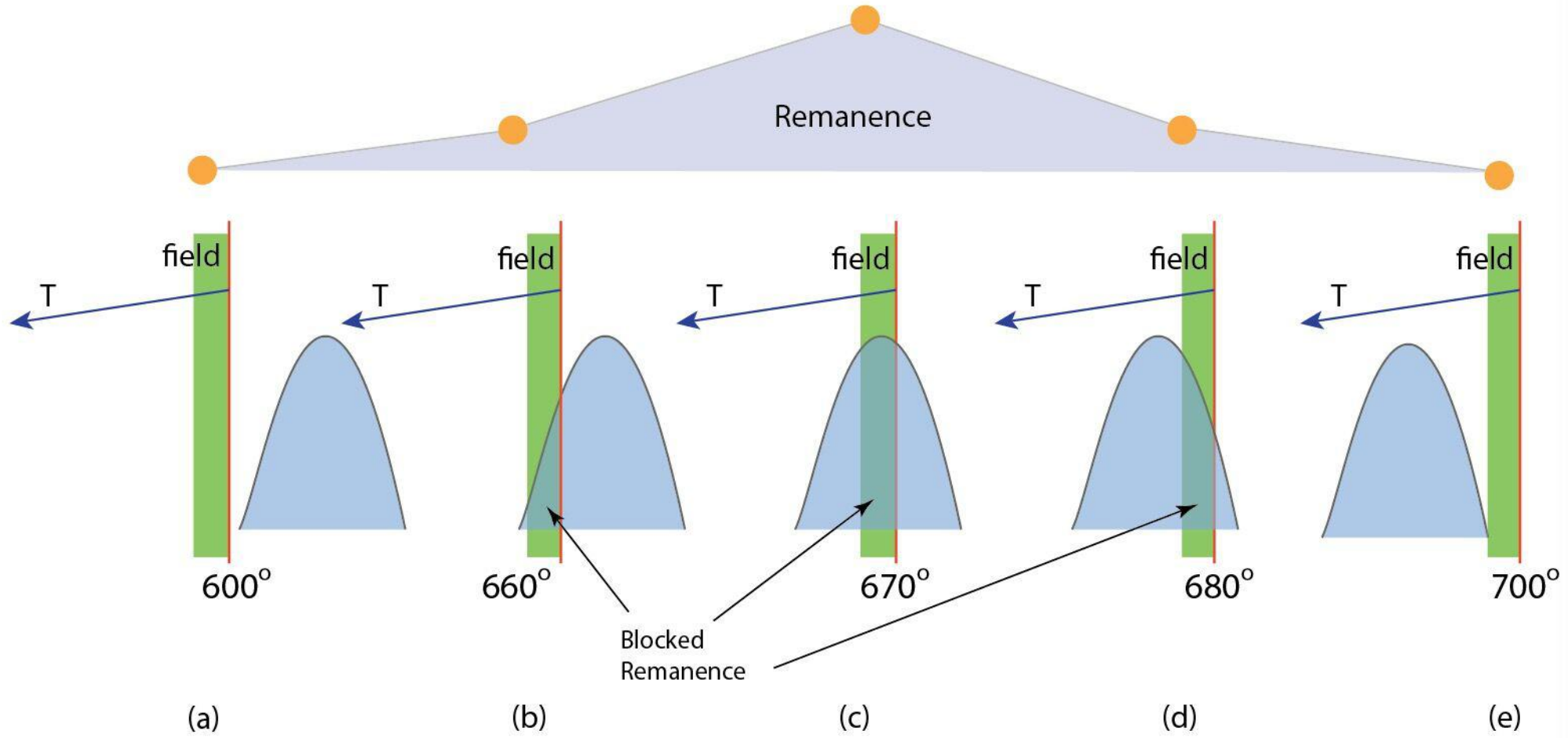


# Re-demagnetization of Synthetic specimens

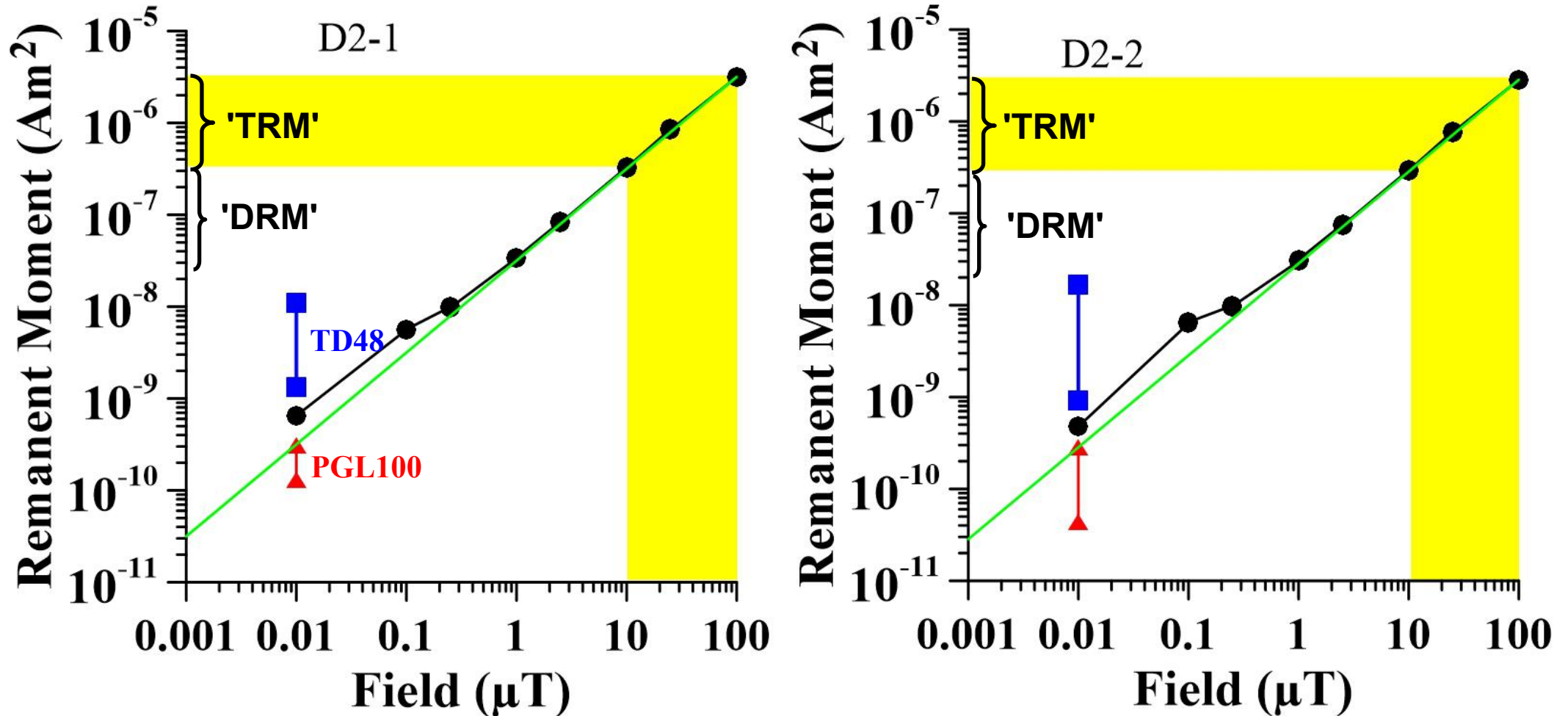


It proved that the extra undesirable remanence acquired during the thermal re-demagnetization process

# Reason for obtaining remanence

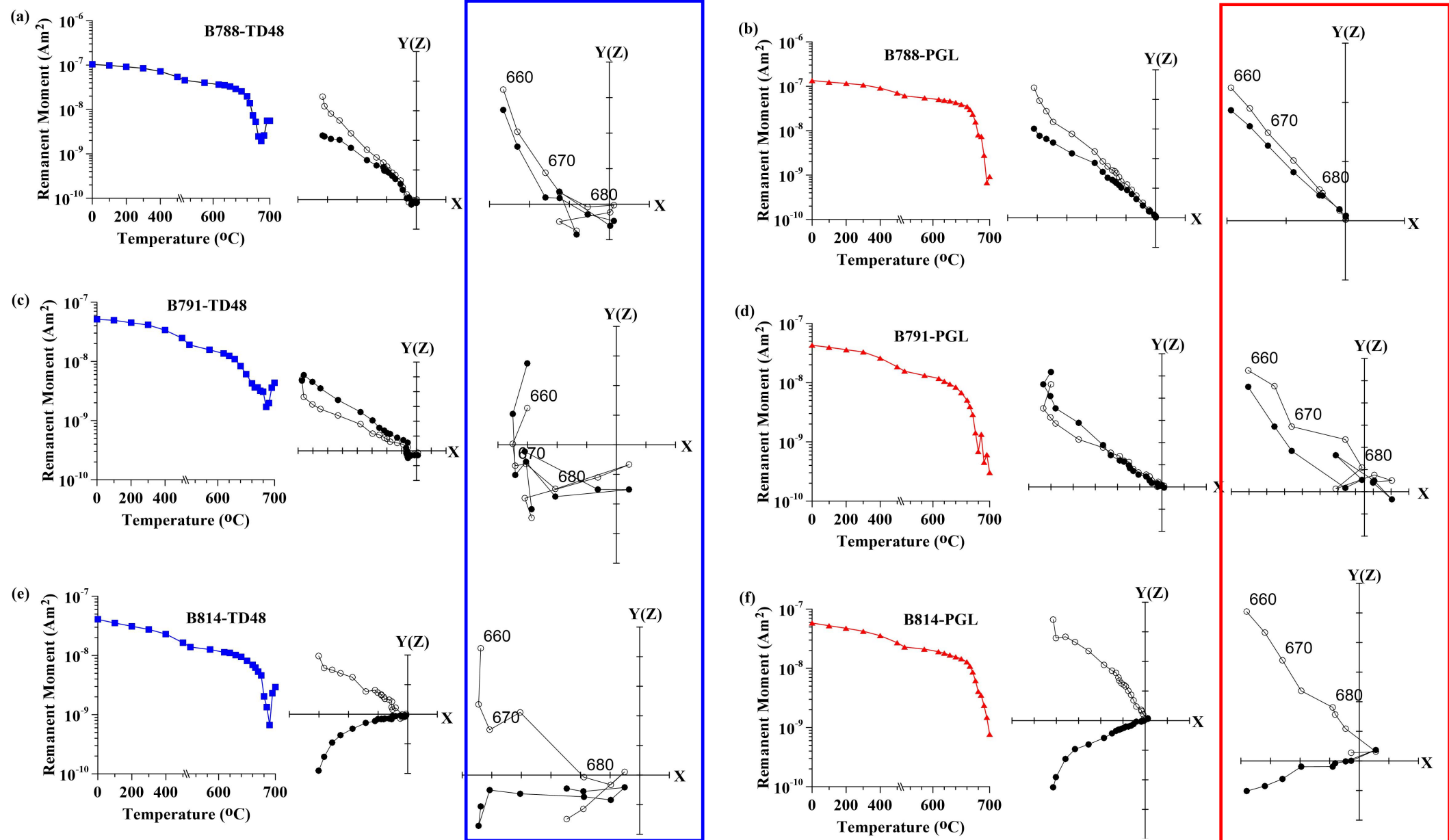


# Nosie Remanece Vs NRM ('TRM', 'DRM')



Suppose that detrital remanence (DRM) is typically an order of magnitude weaker than TRM, nosie fields in furnace may have a large impact on thermal demagnetization data obtained from sedimentary rocks

# Thermal demagnetization of natural specimens





# Conclusions

1. The new heating element design can significantly reduce magnetic field noises in thermal demagnetizer
2. The experiments confirm that magnetic field noise in various furnaces can have an observable and detrimental impact on demagnetization behavior
3. The new furnace represents an important improvement in the design of thermal demagnetizers and allows for extremely weak specimens to be successfully measured.

# Acknowledgements

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