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Simulating Climate Change Impacts on the Recharge Dynamics of a Mediterranean Karst Aquifer

EGU General Assembly 2020, Mai 5th, 2020

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Characteristics of karst systems

■ Dualistic flow dynamics in the phreatic zone:

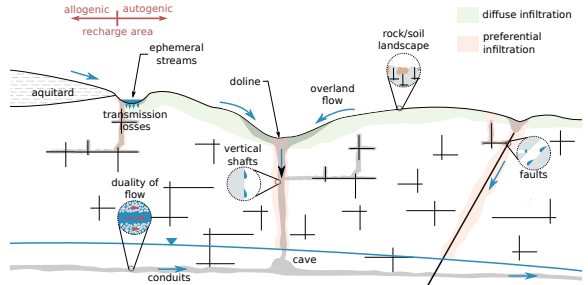
- Matrix: Low hydraulic conductivity, high storage.
- Fracture/Conduit: High hydraulic conductivity, low storage.

■ Dualistic infiltration dynamics in the vadose zone:

- Matrix: Diffuse recharge
- Fracture/Conduit: Focused direct recharge (i.e. preferential flow)

⇒ Continuum Porous Equivalent models often fail to account for this heterogeneity

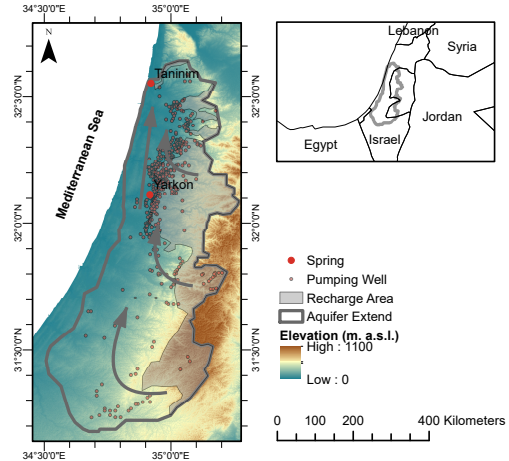
⇒ Accounting for unsaturated flow crucial for predicting flow



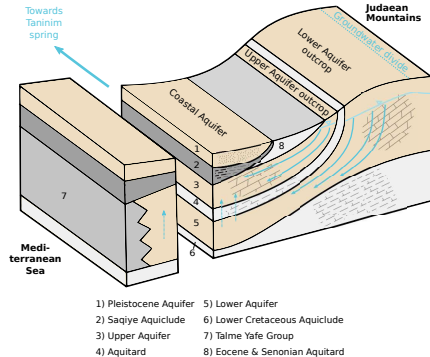
Conceptual model of infiltration into karst rocks (modified after Kordilla et al., 2017; Hartmann et al., 2014).

Project area

- Western Mountain Aquifer (WMA) located in Israel and the Palestinian Territories
- Area: $\sim 9000 \text{ km}^2$
- Semi-arid Mediterranean climate; rainy season from November to April
- Average precipitation of 550 - 600 mm/a
- 330 - 360 MCM/a recharge, $\sim 30 - 35\%$ of precipitation
- Historically, the aquifer drained towards two springs (Taninim and Yarkon spring)
- Heavy groundwater abstraction led to the drying up of the Yarkon spring in the 1970s



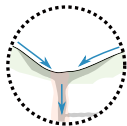
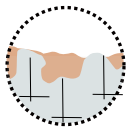
Location map of the Western-Mountain-Aquifer. Arrows indicate the general flow direction.



Conceptual illustration of the general hydrogeology
(modified after Weinberger et al., 1994).

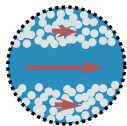
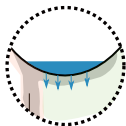
- Highly karstified and fractured carbonate aquifer (mainly limestone and dolomite)
 - Subdivided into an Upper and Lower Aquifer by Marl of the Moza and Bet Meir Formation.
 - Little interaction with saline Mediterranean waters due to impermeable layers (chalky marls) of the Talme Yafe Formation.
- Groundwater recharge occurs through the exposed rock along the anticline in East
 - Scarce cover of soil
 - Abundant direct exposure of karstic carbonate rock
 - ⇒ Emphasizing focused direct recharge
- Several hundreds meters thick vadose zone

rock/soil
landscape



focused recharge
along karst features

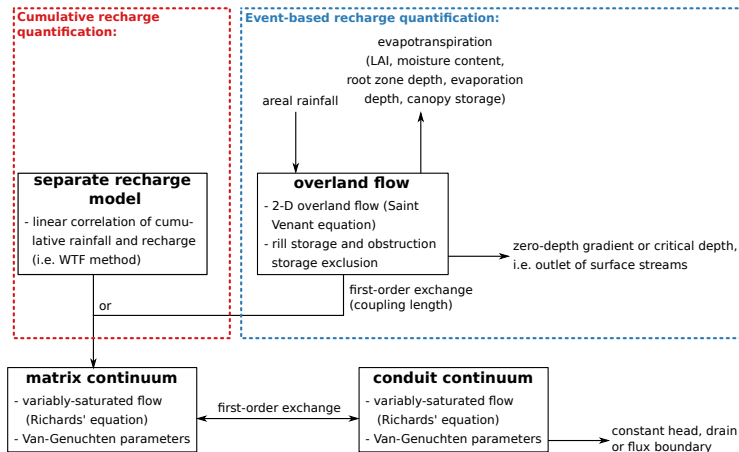
transmission
losses



duality of
flow

- Estimate groundwater recharge based on a rigorous implementation of the surface-hydrological processes, that accounts for:
 - the particularities of rock-soil landscape,
 - focused recharge along karst features (i.e. sinkholes),
 - transmission losses of ephemeral streams (wadis),
 - specific climate conditions as well as the different precipitation patterns.
- Simulation of the effect of infiltration through a thick (several hundreds of meters) vadose zone on groundwater flow dynamics.

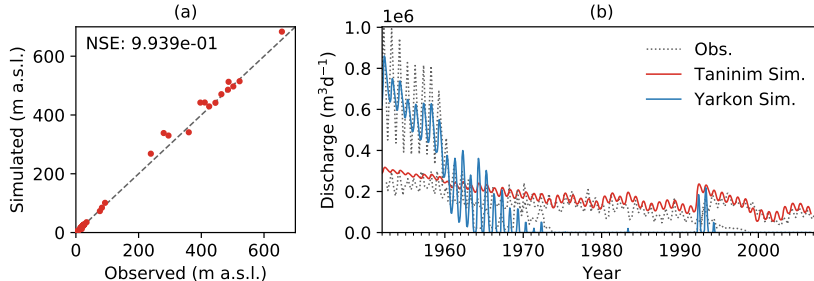
- HydroGeoSphere (HGS) from Aquanty, Waterloo, Canada utilized as flow simulator
- Dual-continuum representation of the subsurface
 - Variably-saturated flow (Richards' equation)
 - Van-Genuchten Parametrization
- Computation of Overland flow
- Surface-subsurface coupled model
- For the mathematical framework refer to Appendix A.



Flow compartments of HGS.

Calibration of variably-saturated dual-continuum flow model

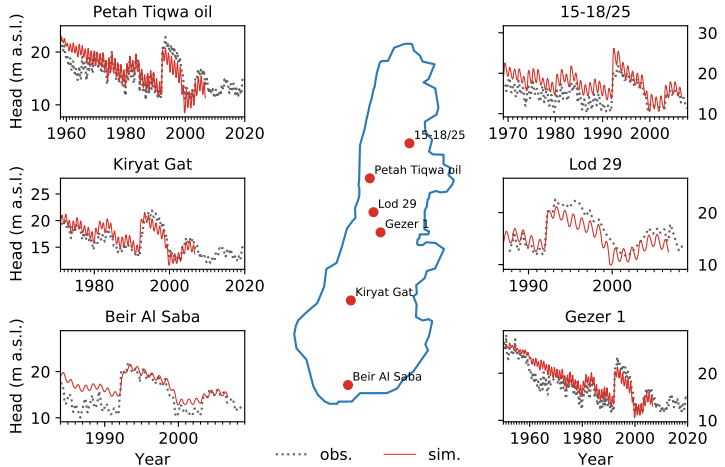
- A variably-saturated dual-continuum model of the WMA has been inversely calibrated based on the hydraulic heads and spring discharge rates (1951 - 2006).
- The simulated discharge reproduces the drying up of the Yarkon spring in the 1970s. The simulation replicates the reactivation (1991/92) of the Yarkon spring.



Computed vs. observed (a) steady-state well heads and (b) spring discharge.

Transient variably-saturated simulation (CPE-Model)

- Water levels well represented
- Only few data points in the mountainous regions



- Simulation of infiltration through a synthetic solution doline
- Shape of the doline described via (Péntek et al., 2007):

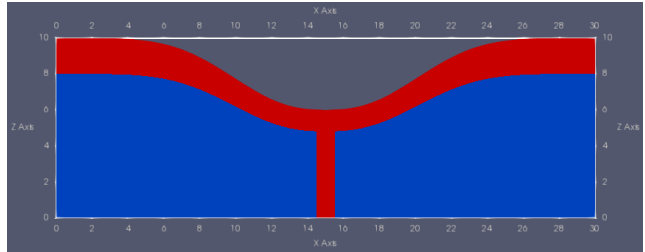
$$\mu(x) = \left[\frac{1}{M} \ln \frac{x}{L} \right]^{\frac{1}{K}} \quad (1)$$

$L > 0$: Parameter controlling the doline depth

$M < 0$: Parameter controlling the doline diameter

$K \leq 0$: Parameter controlling the inflection point of the meridian curve

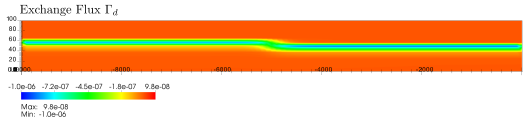
- Van-Genuchten Parameter of the primary continuum have a much greater impact for infiltration dynamics



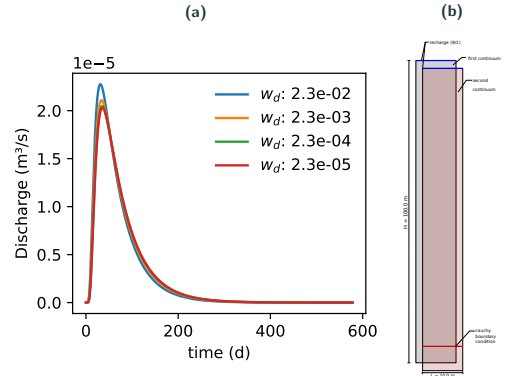
Model geometry of the doline. The red area indicates zones that have been discretized in a dual-continuum representation.

Small-scale process-oriented studies

- The volumetric fraction w_d of the second continuum has very little influence on the discharge
 - Exchange flux mostly occurs along the capillary fringe.
 - Under unsaturated conditions the matrix continuum has a lower matric potential.
- ⇒ Flow from matrix to conduit is mathematically impossible under unsaturated conditions (Van-Genuchten limitations).



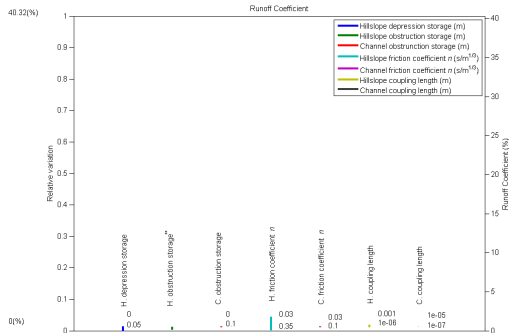
Matrix-Conduit exchange flux



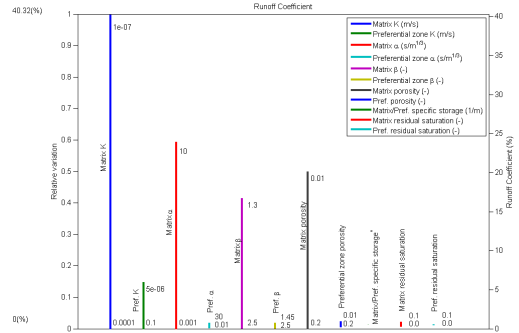
Testing the coupling of the two continua under unsaturated conditions via a simplified simulation.

Small-scale process-oriented studies

- Synthetic dry valley
- Investigation of the parameters controlling the coupling of surface-subsurface flow



Influence of the different surface hydraulic parameters on the runoff coefficient.



Influence of the different subsurface hydraulic parameters on the runoff coefficient.

Conclusions:

- Variably-saturated dual-continuum flow models seem to not allow for unsaturated flow through the second continuum.
- Hydraulic properties of the near-surface subsurface strongly control the runoff coefficient.
- With increasing computational resources, integrated surface-subsurface flow models may provide useful tools to estimate event-based recharge.

Outlook:

- Currently, separately calculated monthly recharge rates from 1951 to 2006 are used in the model.
- In the long run, groundwater recharge shall be calculated by simulating overland flow and computing actual Evapotranspiration within HydroGeoSphere. This allows accounting for the partitioning of rainfall into surface runoff in a spatially and temporally distributed manner. The impact of climatic changes on infiltration dynamics shall be investigated as a next step.

Thank you for your attention – Questions?
Contact me via email (lbresin@gwdg.de) or join the live chat.

Supplementary Slides:

References

Appendix:

Appendix A: "Mathematical Framework of HGS"

Appendix B: "Geology and Palaeo-hydrogeology of the WMA"



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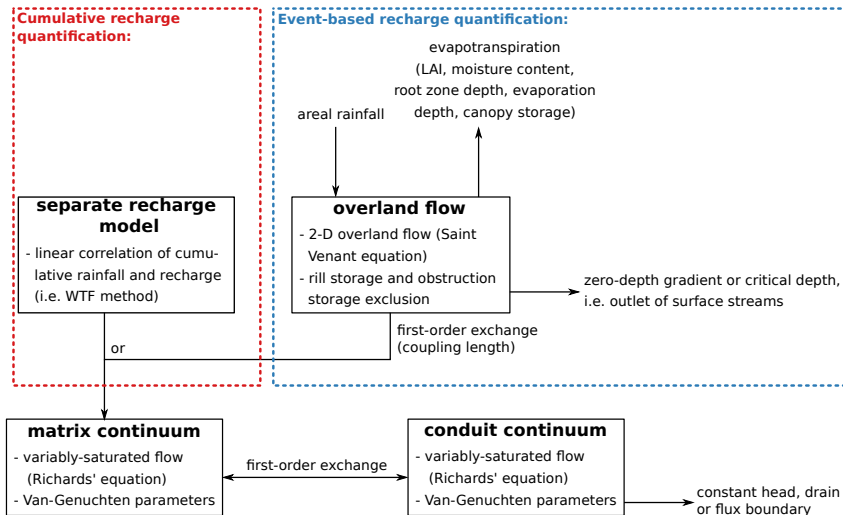


Bundesministerium
für Bildung
und Forschung



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Appendix A.1: Mathematical Framework of HGS - Overview of the flow compartments



Simulation of various flow compartments with HGS

Appendix A.2: Mathematical Framework of HGS - Computation of flow

■ 2D surface routing (Saint Venant):

$$-\nabla \cdot (d_o \mathbf{q}_o) - d_o \Gamma_o \pm Q_o = \frac{\partial \phi_o h_o}{\partial t}. \quad (2)$$

where \mathbf{q}_o is defined as: $\mathbf{q}_o = -\mathbf{K}_o \cdot k_{ro} \nabla (d_o + z_o)$

d_o : depth of flow ($h_o = z + d_o$)

ϕ_o : porosity (olf)

Γ_o : exchange term

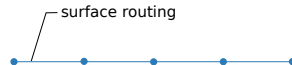
K_o : obt. from Chezy, Manning or Darcy-Weisbach equation

k_{ro} : conductance reduction from obstruction storage exclusion

h_o : surface water head

Q_o : volumetric fluid flux (bcs)

\mathbf{q}_o : fluid flux



Framework of integrated multi-continuum models.

Appendix A.2: Mathematical Framework of HGS - Computation of flow

■ Richards' equation (porous medium):

$$-\nabla \cdot (w_m \mathbf{q}_m) + \Gamma_o + \Gamma_d \pm Q_m = w_m \frac{\partial}{\partial t} (\theta_{sm} S_{wm}), \quad (3)$$

where the fluid flux \mathbf{q}_m is defined as: $\mathbf{q}_m = -\mathbf{K}_m \cdot k_{rm} \nabla (\psi_m + z_m)$.

w_m : volumetric fraction

Γ_o, Γ_d : exchange term

θ_{sm} : saturated water content

z_m : elevation head

S_{wm} : water saturation ($S_{wm} = \frac{\theta_m}{\theta_{sm}}$)

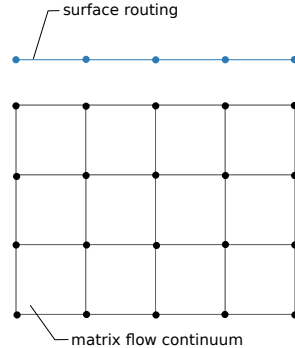
k_{rm} : relative conductivity (controls variably-saturated flow)

\mathbf{q}_m : fluid flux

Q_m : volumetric fluid flux (bcs)

\mathbf{K}_m : hydraulic conductivity

ψ_m : pressure head



Framework of integrated multi-continuum models.

Appendix A.2: Mathematical Framework of HGS - Computation of flow

■ Richards' equation (dual medium):

$$-\nabla \cdot (w_d \mathbf{q}_d) - \Gamma_d \pm Q_d = w_d \frac{\partial}{\partial t} (\theta_{sd} S_{wd}), \quad (4)$$

where \mathbf{q}_d is defined as: $\mathbf{q}_d = -\mathbf{K}_d \cdot k_{rd} \nabla (\psi_d + z_d)$.

w_d : volumetric fraction

Γ_d : exchange term

θ_{sd} : saturated water content

z_d : elevation head

S_{wd} : water saturation ($S_{wd} = \frac{\theta_d}{\theta_{sd}}$)

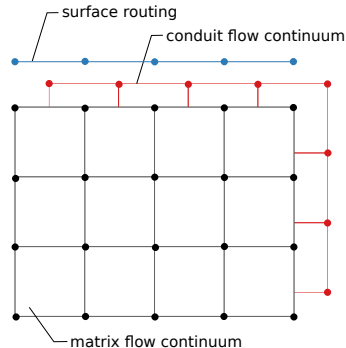
k_{rd} : relative conductivity (controls variably-saturated flow)

\mathbf{q}_d : fluid flux

Q_d : volumetric fluid flux (bcs)

\mathbf{K}_d : hydraulic conductivity

ψ_d : pressure head



Framework of integrated multi-continuum models.

Appendix A.2: Mathematical Framework of HGS - Computation of flow

■ Porous/dual medium coupling:

$$\Gamma_d = \frac{\beta_g}{a^2} \gamma_w K_\alpha k_{ra} (\psi_d - \psi_m). \quad (5)$$

β_g : geometrical shape factor

γ_w : empirical coefficient

k_{ra} : relative hydraulic conductivity

a : skin thickness

ψ_d, ψ_m : pressure head

K_α : interface hydraulic conductivity

■ Surface/subsurface coupling:

$$d_o \Gamma_o = w_m \frac{k_{rm} K_{zz}}{l_{ex}} (h_m - h_o) + w_d \frac{k_{rd} K_{dzz}}{l_{ex}} (h_d - h_o). \quad (6)$$

h_m, h_d : hydraulic head

d_o : depth of flow ($h_o = z + d_o$)

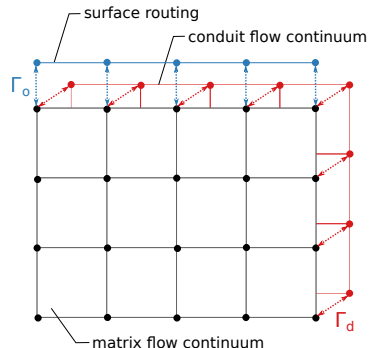
k_{rm}, k_{rd} : relative conductivity

K_{zz}, K_{dzz} : vertical hydraulic conductivity

h_o : surface water head

w_m, w_d : volumetric fraction

l_{ex} : coupling length



Framework of integrated multi-continuum models.

Appendix A.2: Mathematical Framework of HGS - Van-Genuchten parameterization

- Nonlinear dependence of $k_r(S_w)$ and $S_w(\psi)$ (Mualem, 1976; van Genuchten, 1980):

$$k_r = S_e^{l_p} (1 - (1 - S_e^{\nu^{-1}})^{\nu})^2, \quad (7)$$

$$S_e = \frac{S_w - S_{wr}}{1 - S_{wr}}, \quad (8)$$

$$S_w = S_{wr} + (1 - S_{wr})[1 + |\alpha\psi|^{\beta}]^{-\nu}, \text{ for } \psi < 0, \quad (9)$$

where $\nu = 1 - \frac{1}{\beta}$, $\beta > 1$.

S_e : effective saturation

S_{wr} : residual saturation

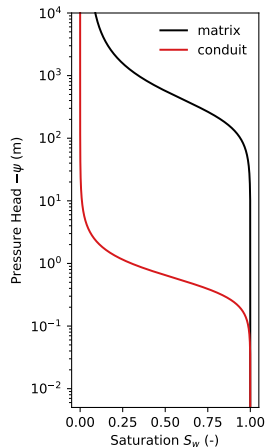
α : inverse air-entry pressure head

S_w : saturation ($S = \frac{\theta}{\theta_s}$)

l_p : pore-connectivity parameter

β : pore-size distribution index

- Prone to degeneracy.
- Hysteresis is not considered here.



- Time step size is a key factor in controlling the model accuracy and efficiency
- Implicit sub-time stepping approach:

$$\Delta t^{L+1} = \frac{X_{max}}{\max |X_i^{L+1} - X_i^L|} \Delta t^L \quad (10)$$

X : value of the time-controlling variable at node i

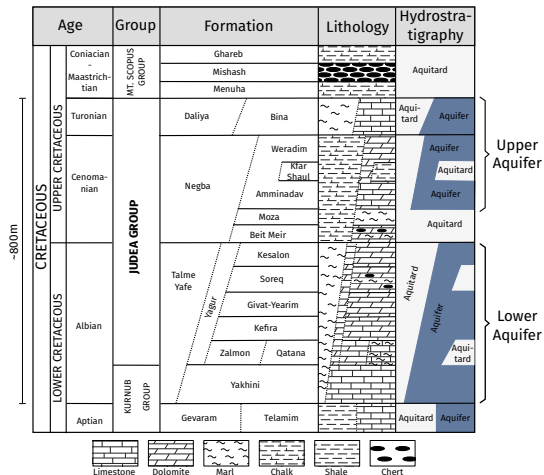
L : current time level

X_{max} : defined maximum change of variable X

Δt : time step

where the variable X can be the hydraulic head and/or saturation.

Appendix B.1: Geology and Palaeo-hydrogeology of the WMA - Stratigraphic column



Stratigraphic and hydrostratigraphic column from West to East (modified after Fleischer, 2002; Weinberger et al., 1994; Zilberbrand et al., 2014)

Appendix B.2: Geology and Palaeo-hydrogeology of the WMA - Development of karst voids

- Regional uplift (Oligocene) of the Judaeen mountains
 - Regression of the Tethys Sea
 - Formation of deep canyons along the coastline
 - ⇒ Increased density of conduits in the proximity to paleo-canyons
- Lowering of the Mediterranean sea level
 - Messinian Salinity Crisis (~ 6 Ma, Late Miocene) over a period of ~ 0.6 Ma
 - ⇒ Lowering of the base-level
 - ⇒ Development of karst conduits at great depth