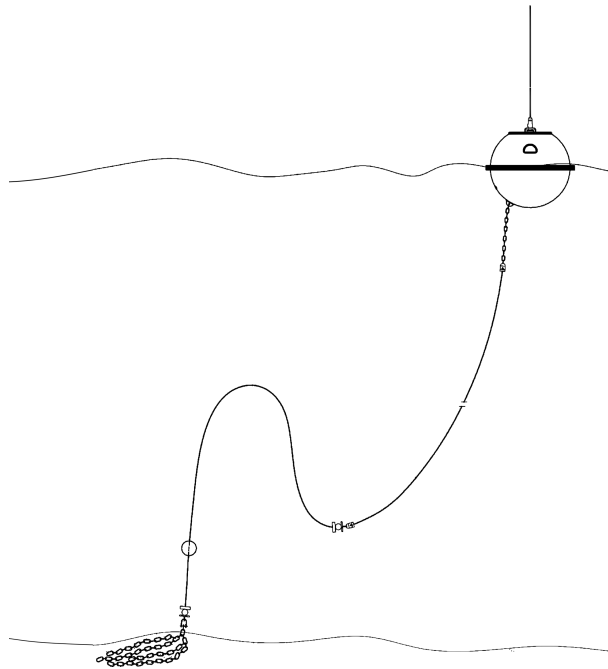


# An Experimental Study of the Systematic Underestimation of Wave Crests Measured by Lagrangian Buoys, and a Retrospective Correction Method

Mark L. McAllister and Ton S. van den Bremer

University of Oxford

EGU 4<sup>th</sup> May 2020



# Lagrangian Measurement of Waves by Buoys

- Motivation
- Second-Order Motion of a Wave-Following Measurement Buoy
- Statistical Properties of Directionally Spread Ocean Waves Measured by Buoys
- Approximate retrospective correction method for crest heights



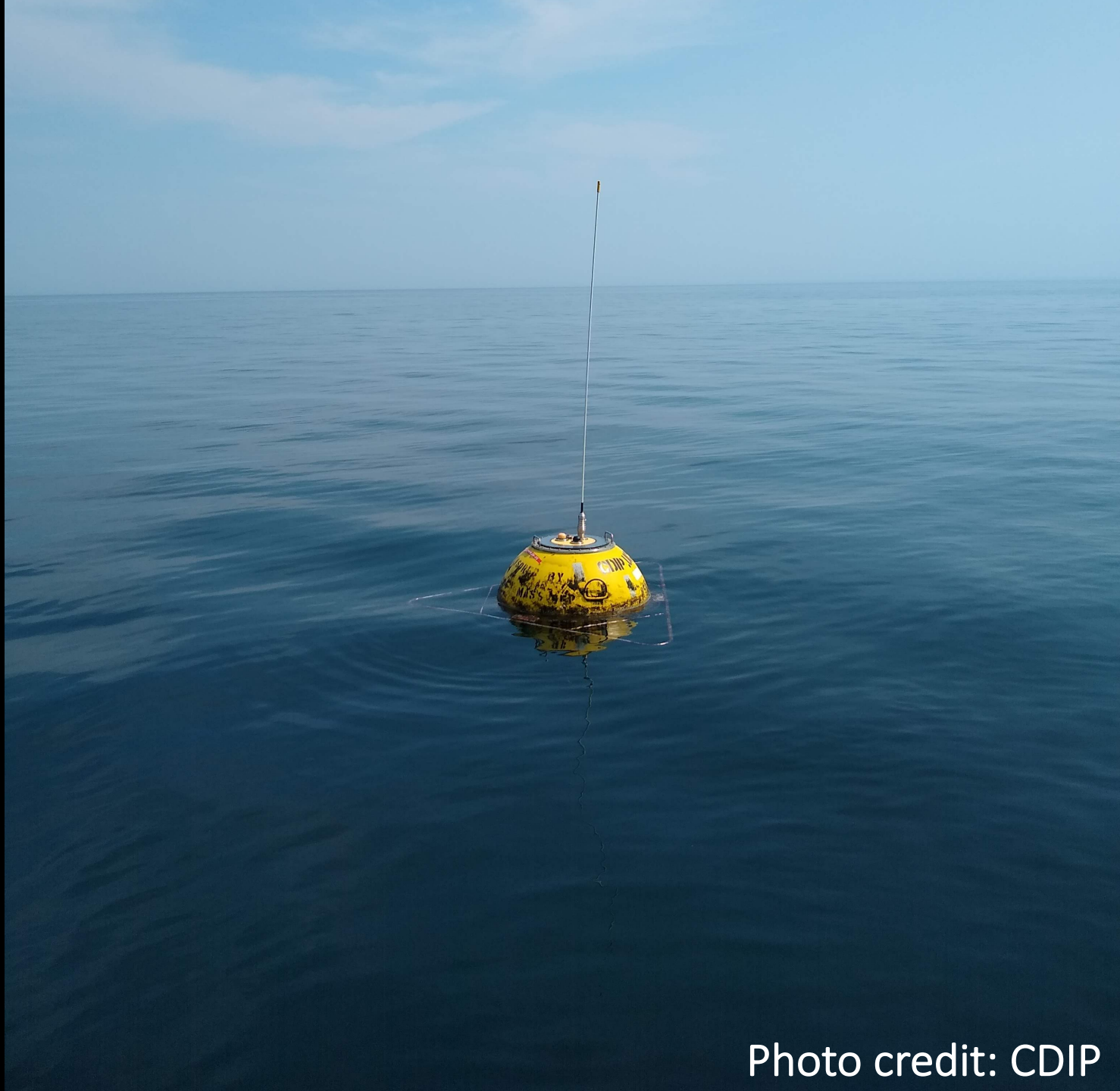


Photo credit: CDIP



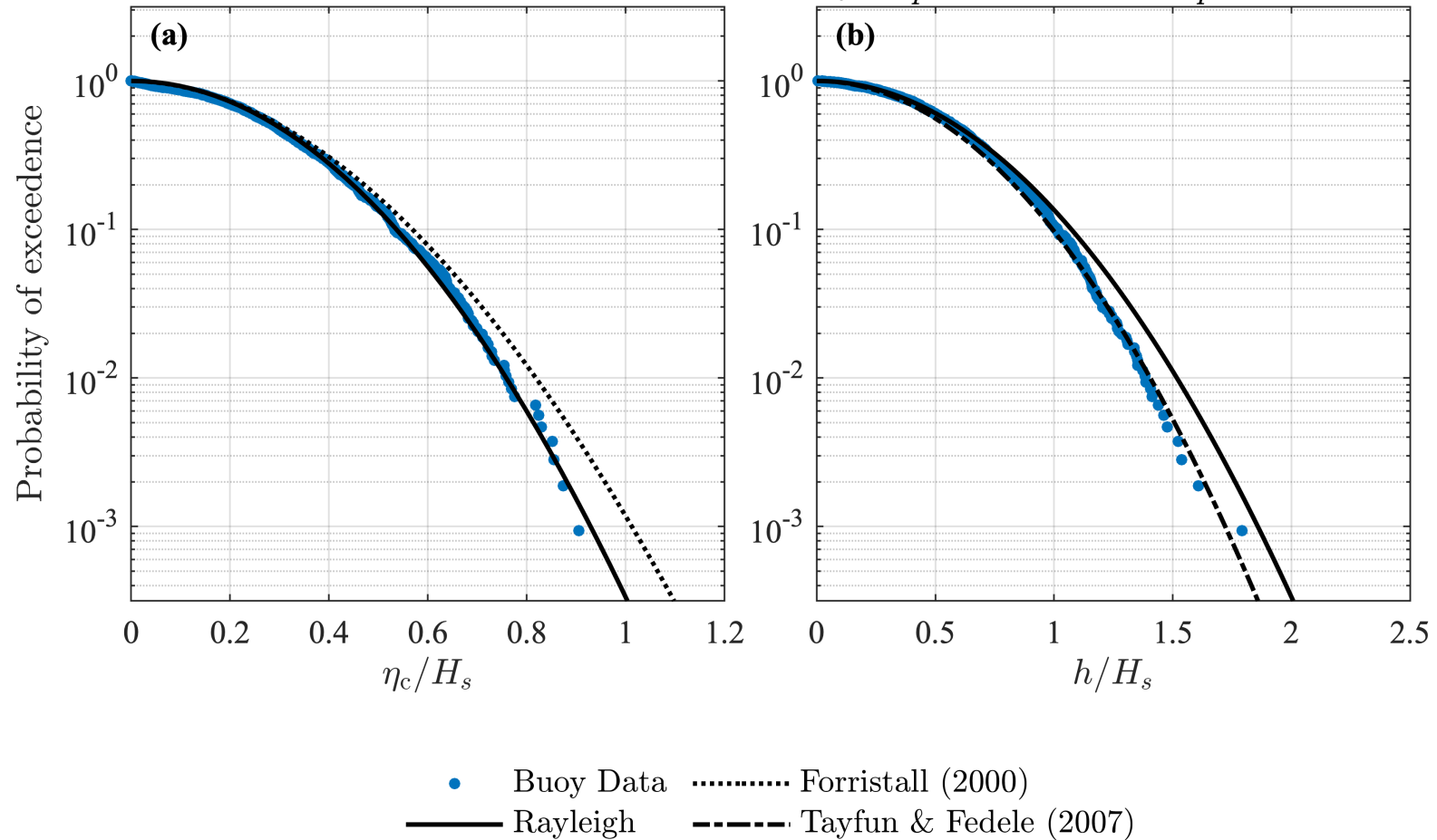


Photo credit: CDIP



# Motivation

San Nicholas Island CDIP buoy,  $k_p H_s \approx 0.25$ ,  $k_p d \approx 10$



# Motivation

- Buoys avoid large crest
- Lack of mooring compliance drags buoys under crests
- Low sampling rate misses crests
- Lagrangian motion “linearises” crests
- Instrumentation and signal processing

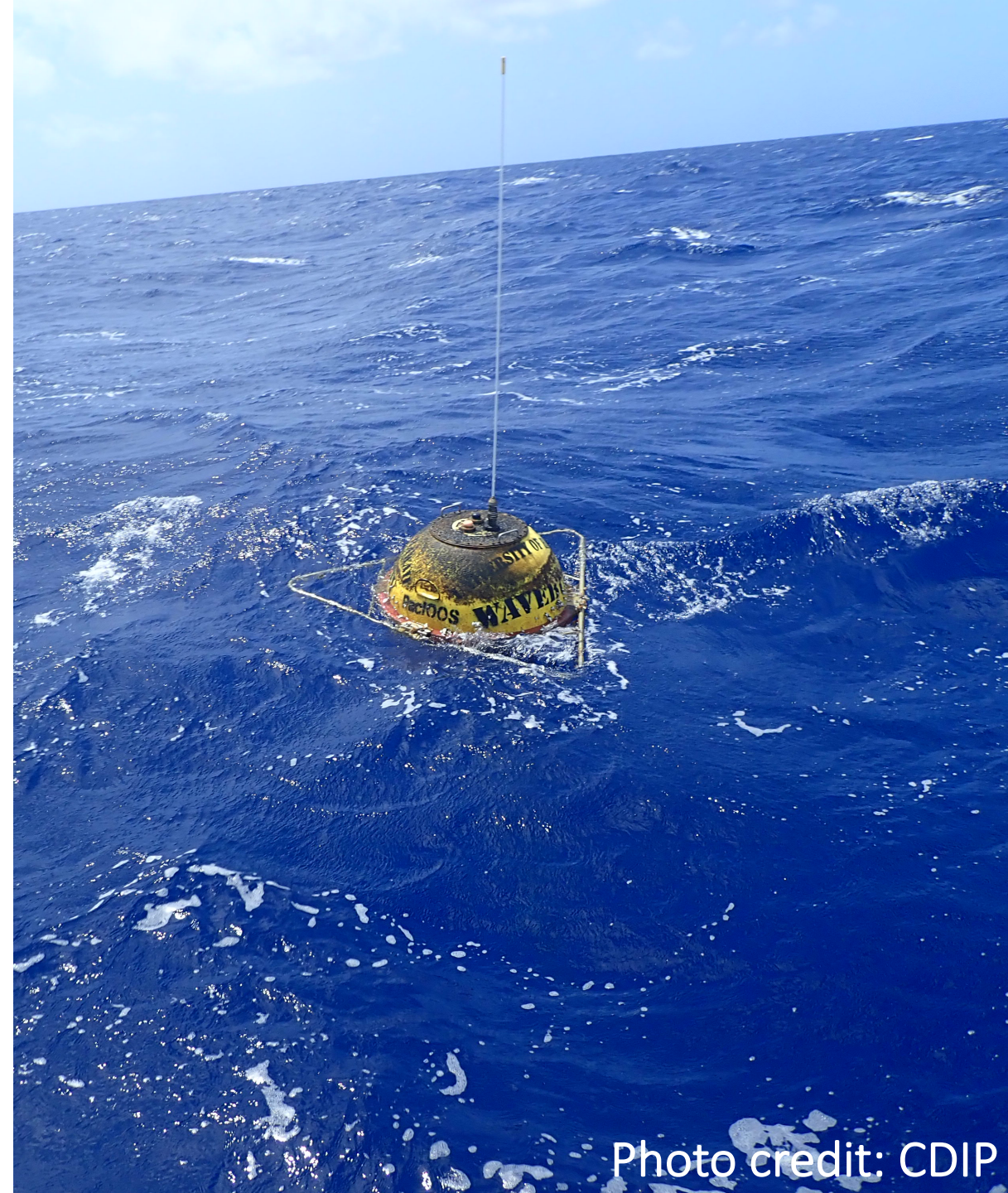
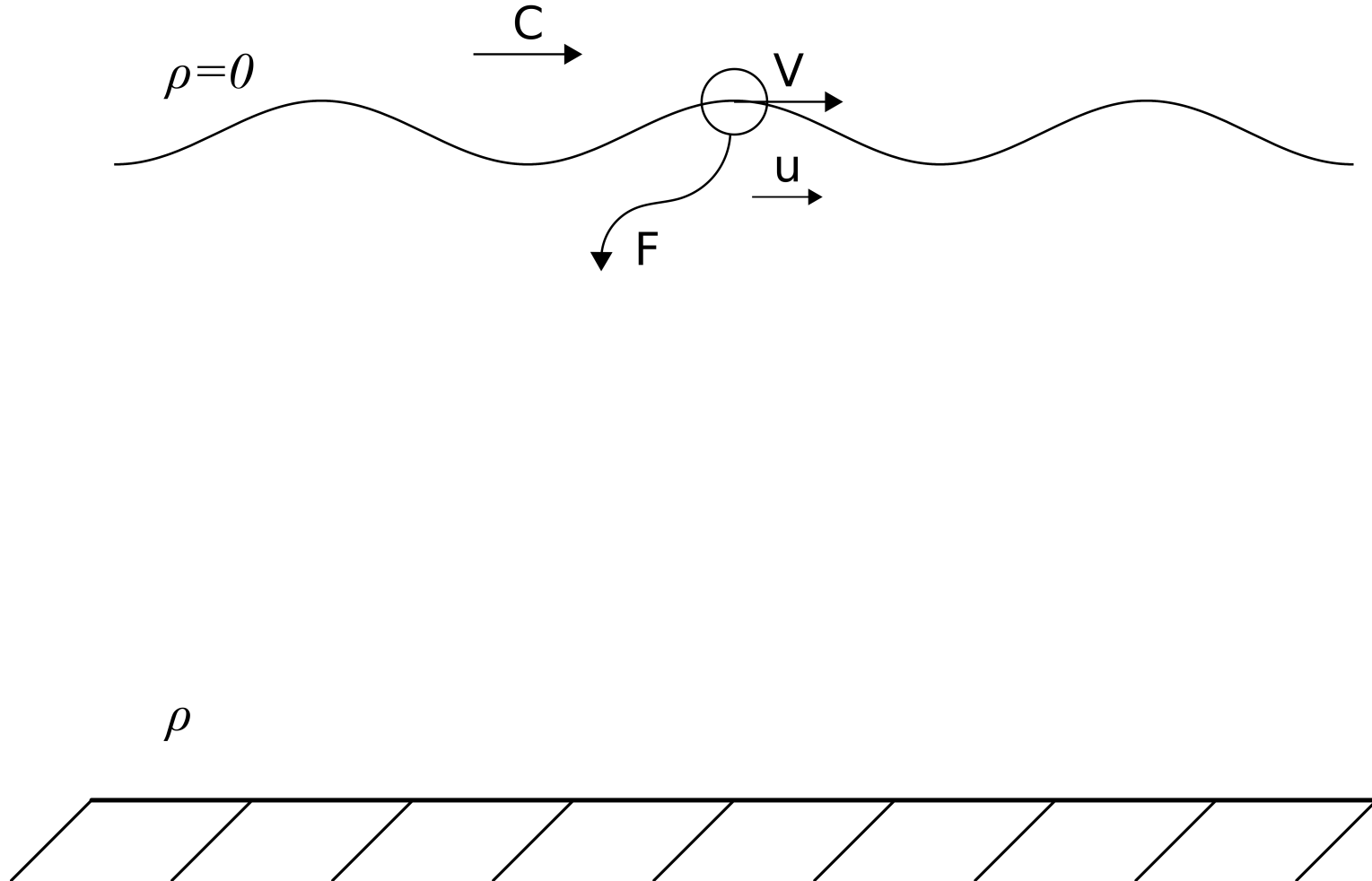


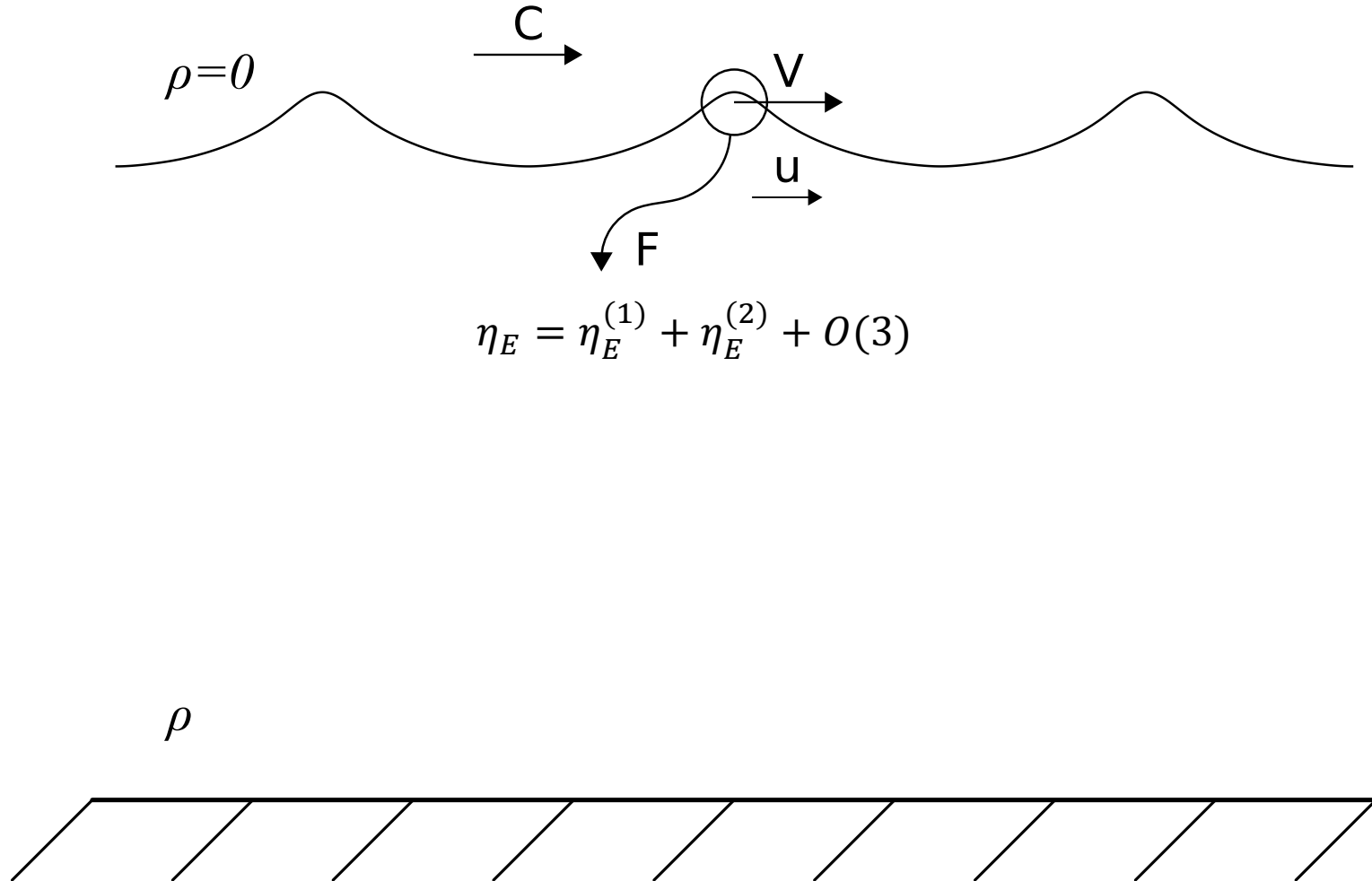
Photo credit: CDIP

# Second-Order Motion of a Wave-Following Measurement Buoy

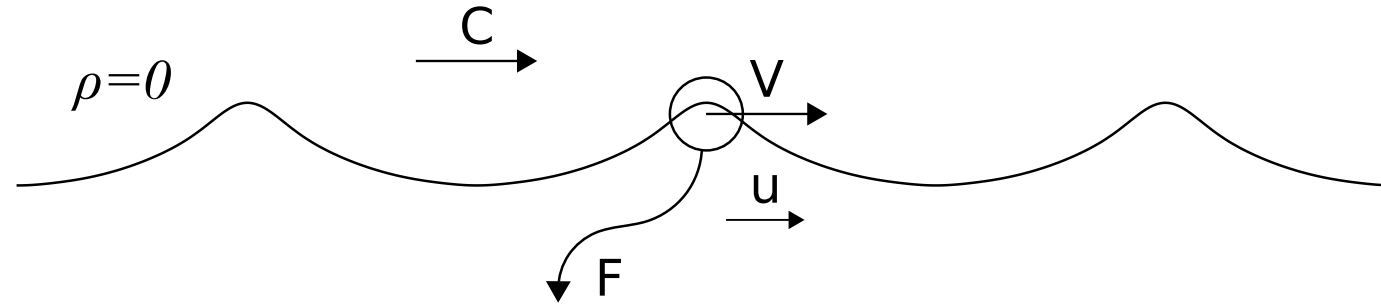




# Second-Order Motion of a Wave-Following Measurement Buoy



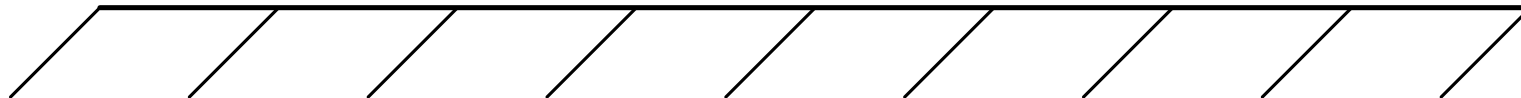
# Second-Order Motion of a Wave-Following Measurement Buoy



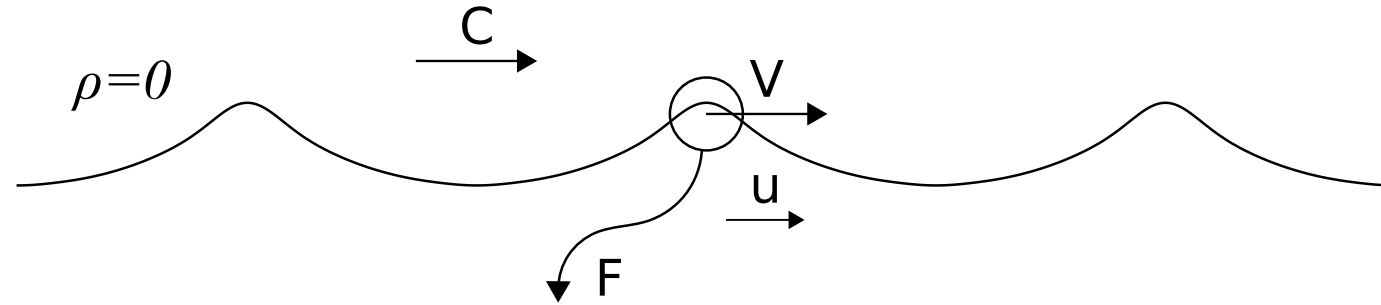
$$\eta_E = \eta_E^{(1)} + \eta_E^{(2)} + O(3)$$

$$\eta_L^{(2)} = \eta_E^{(2)} + \Delta\eta_L^{(2)}$$

$\rho$



# Second-Order Motion of a Wave-Following Measurement Buoy

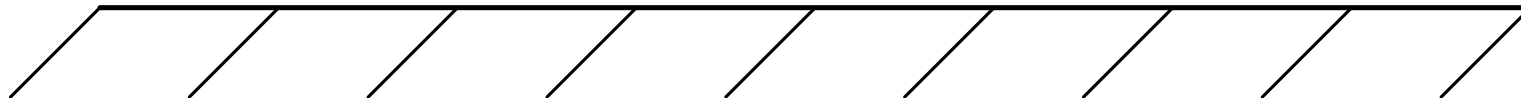


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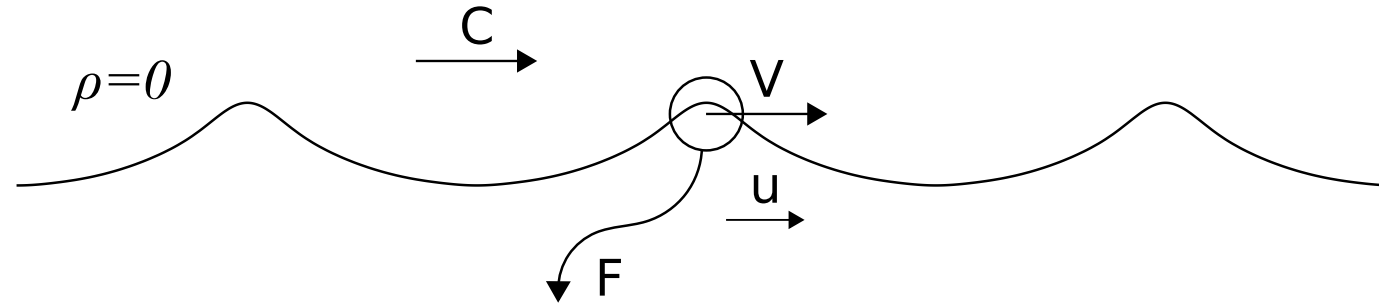
$$\Delta\eta_L^{(1)} = \Delta x_H^{(1)} \cdot \nabla_H \eta^{(1)}$$

$\rho$





# Second-Order Motion of a Wave-Following Measurement Buoy



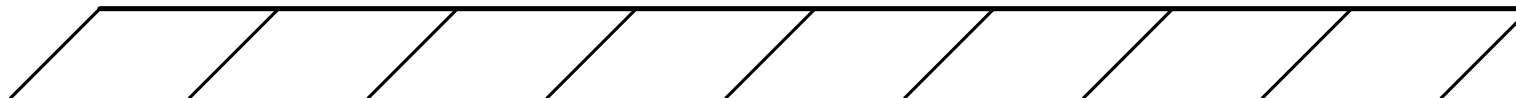
$$\eta_E = \eta_E^{(1)} + \eta_E^{(2)} + O(3)$$

$$\eta_L^{(2)} = \eta_E^{(2)} + \Delta\eta_L^{(2)}$$

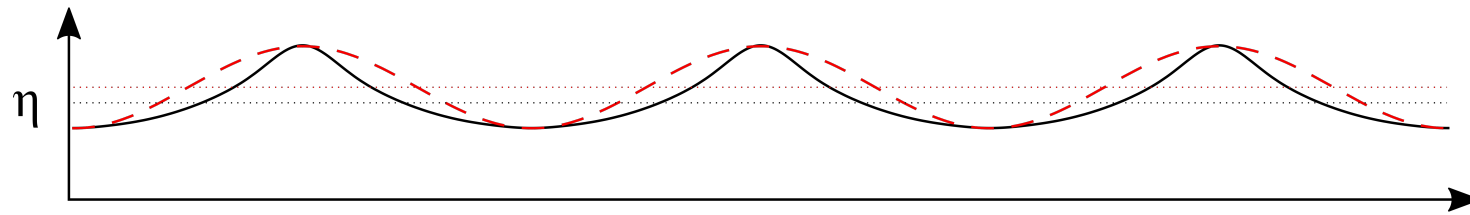
$$\Delta\eta_L^{(1)} = \Delta x_H^{(1)} \cdot \nabla_H \eta^{(1)}$$

$$\eta_E^{(2)} = -\Delta\eta_L^{(2)} \text{ (Deep water)}$$

$\rho$



# Second-Order Motion of a Wave-Following Measurement Buoy



$$\text{Eulerian } \eta = \frac{t}{\text{---}}$$

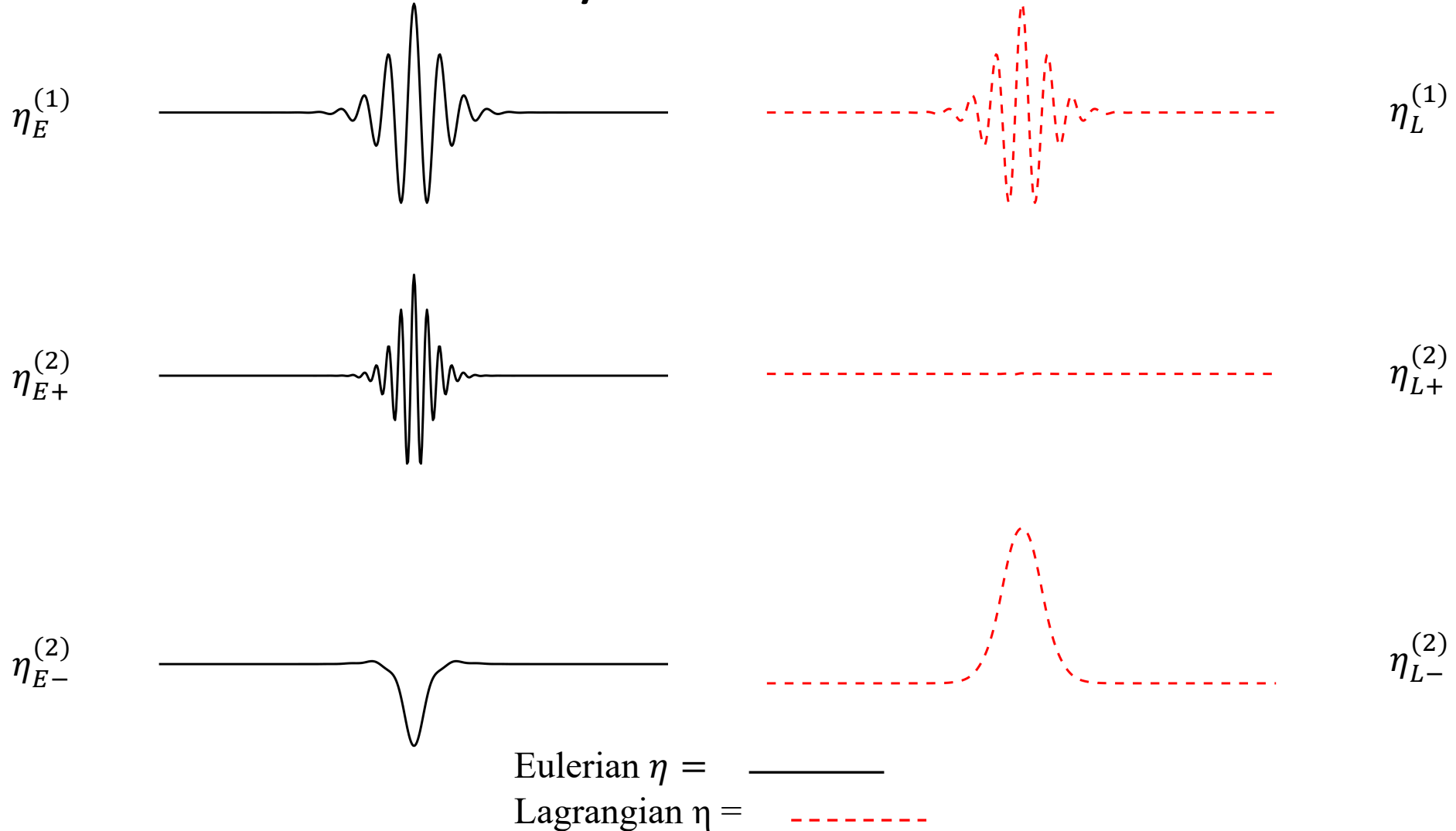
$$\text{Lagrangian } \eta = \text{---}$$

$$\eta_L^{(2)} = \eta_E^{(2)} + \Delta\eta_L^{(2)}$$

$$\Delta\eta_L^{(1)} = \Delta x_H^{(1)} \cdot \nabla_H \eta^{(1)}$$

$$\eta_E^{(2)} = -\Delta\eta_L^{(2)} \text{ (Deep water)}$$

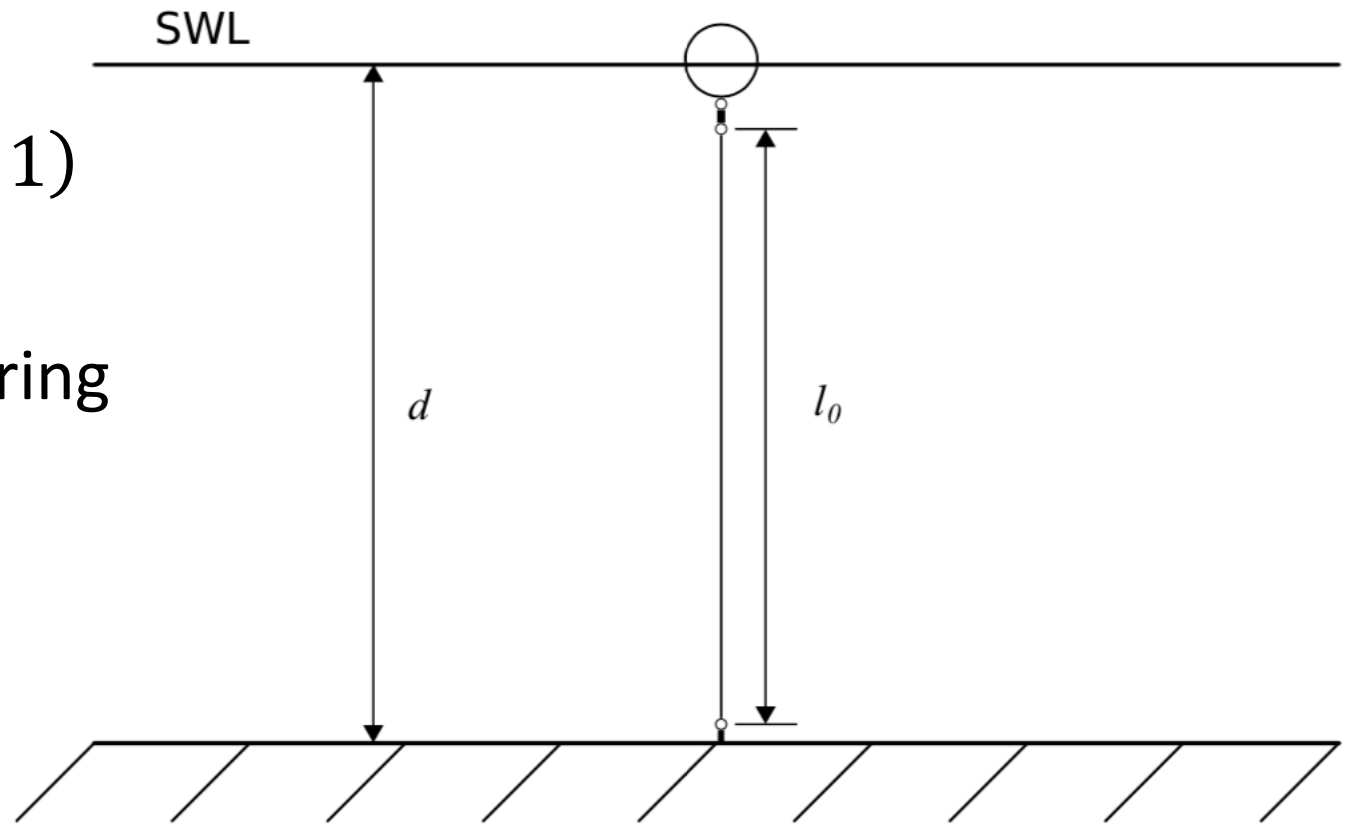
# Second-Order Motion of a Wave-Following Measurement Buoy



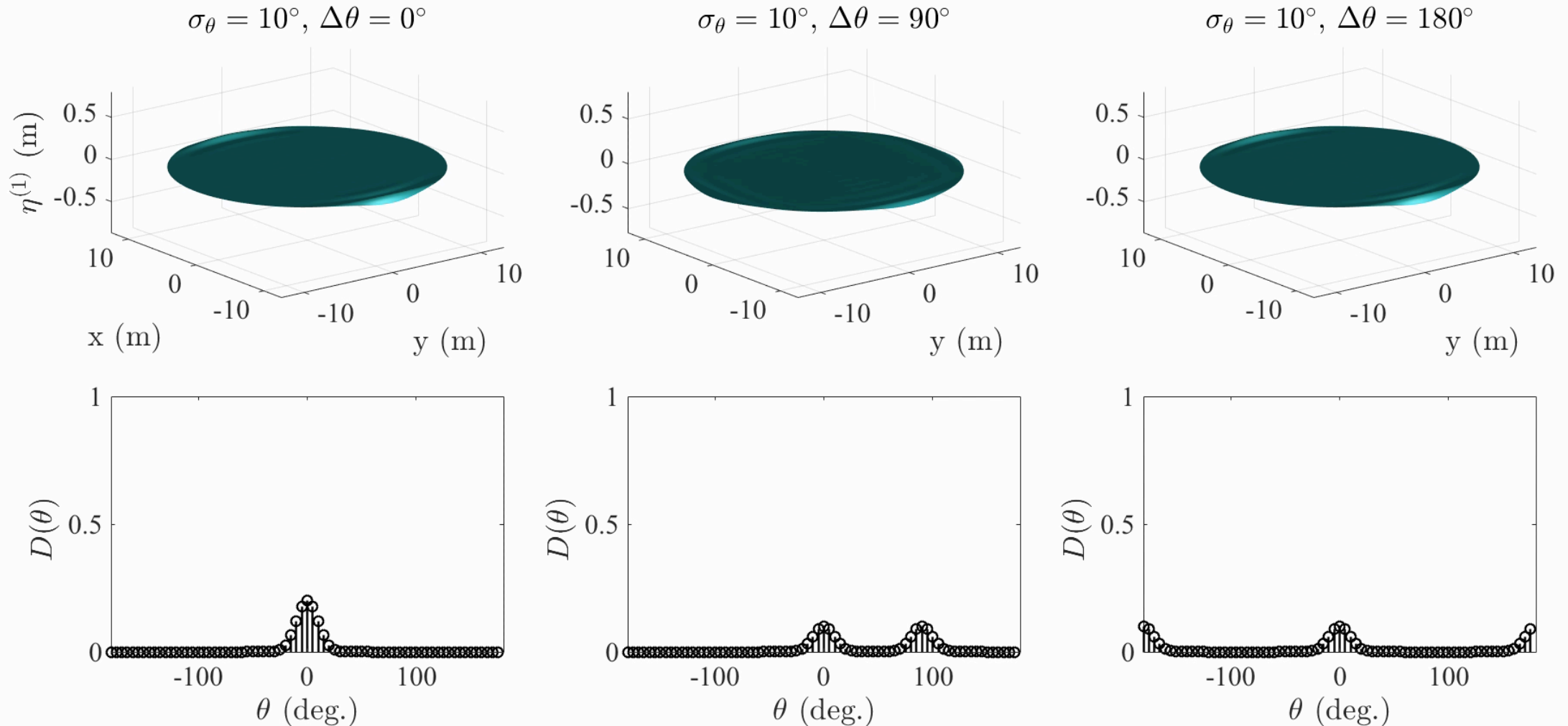


# Second-Order Motion of a Wave-Following Measurement Buoy

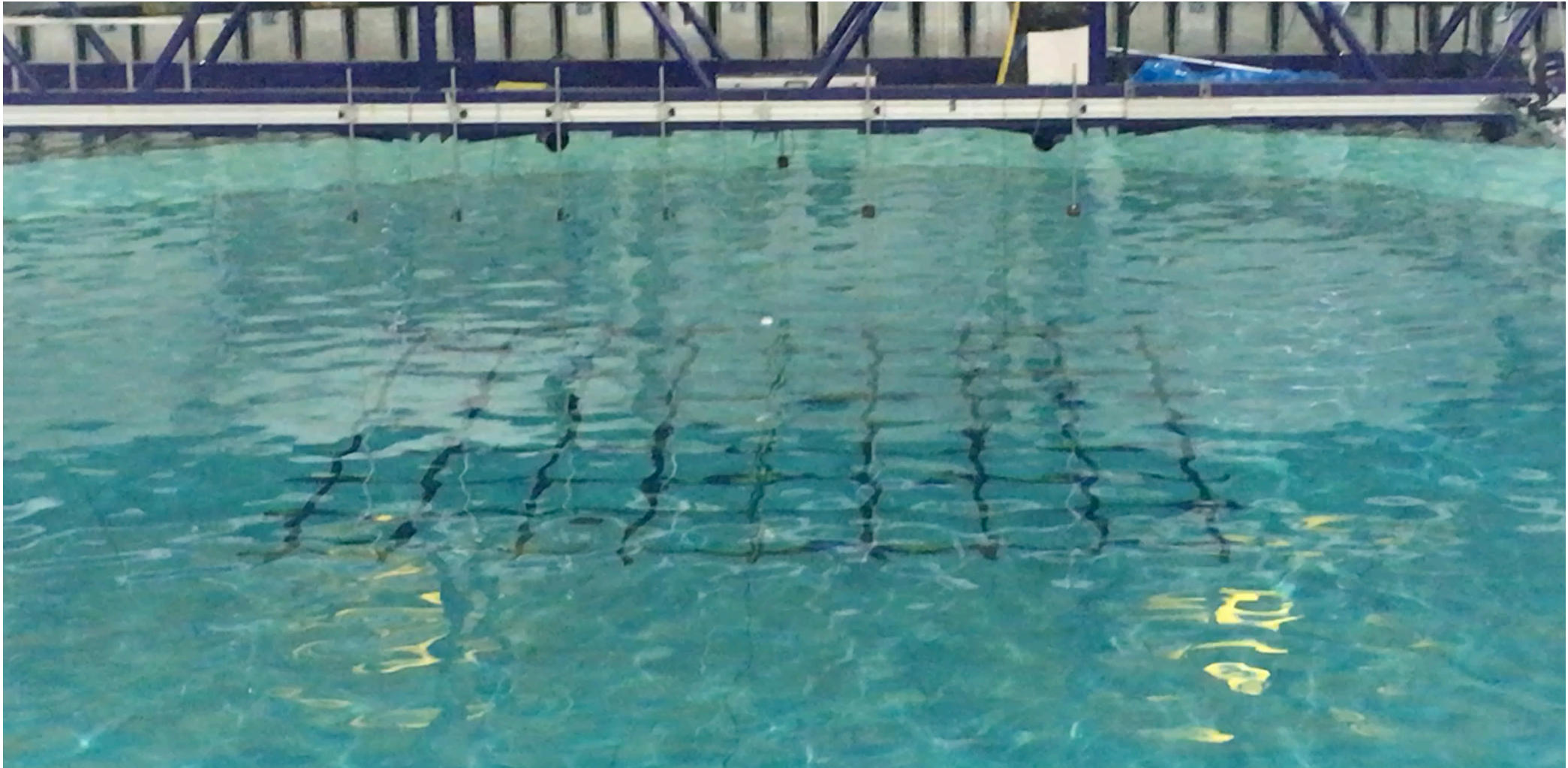
- Diameter 0.07m ( $D/\lambda_0 \ll 1$ )
- Density  $\approx 0.5\rho_w$
- Highly-flexible taught mooring
- Depth 2 m ( $k_0 d = 3 - 4$ )
- Wave amplitude  $\approx 0.2$  m  
( $k_0 a_0 / k_p H_s \approx 0.3$ )



# Second-Order Motion of a Wave-Following Measurement Buoy

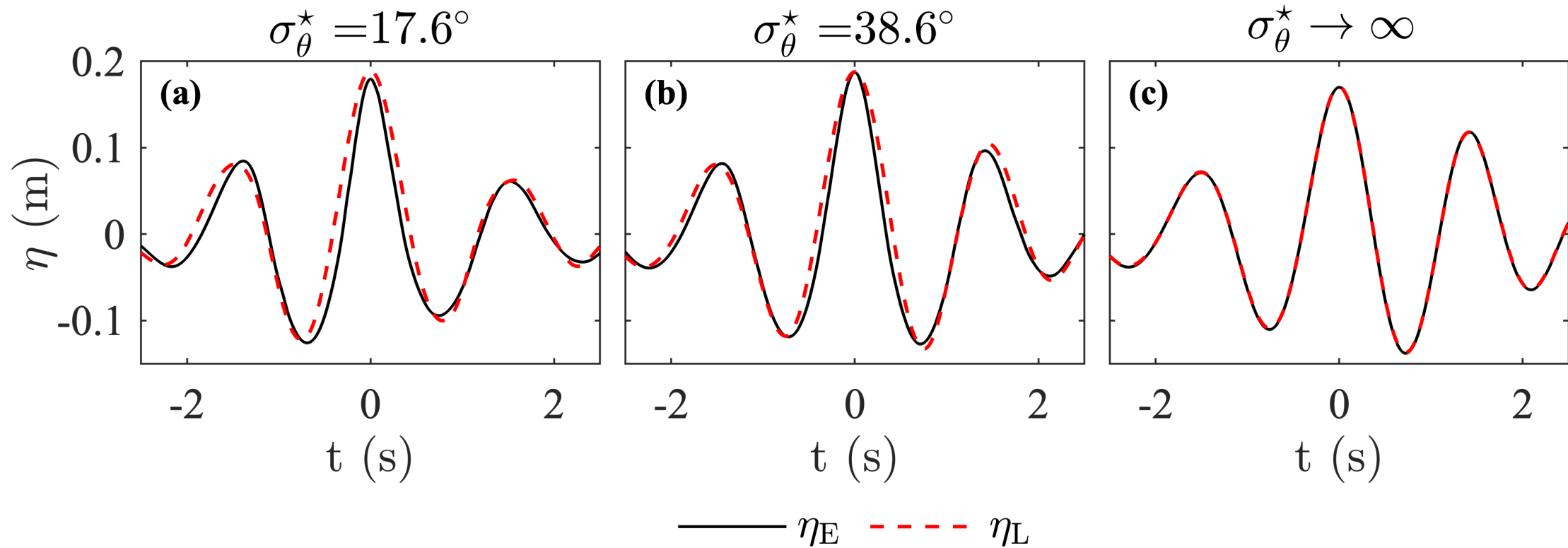


# Second-Order Motion of a Wave-Following Measurement Buoy

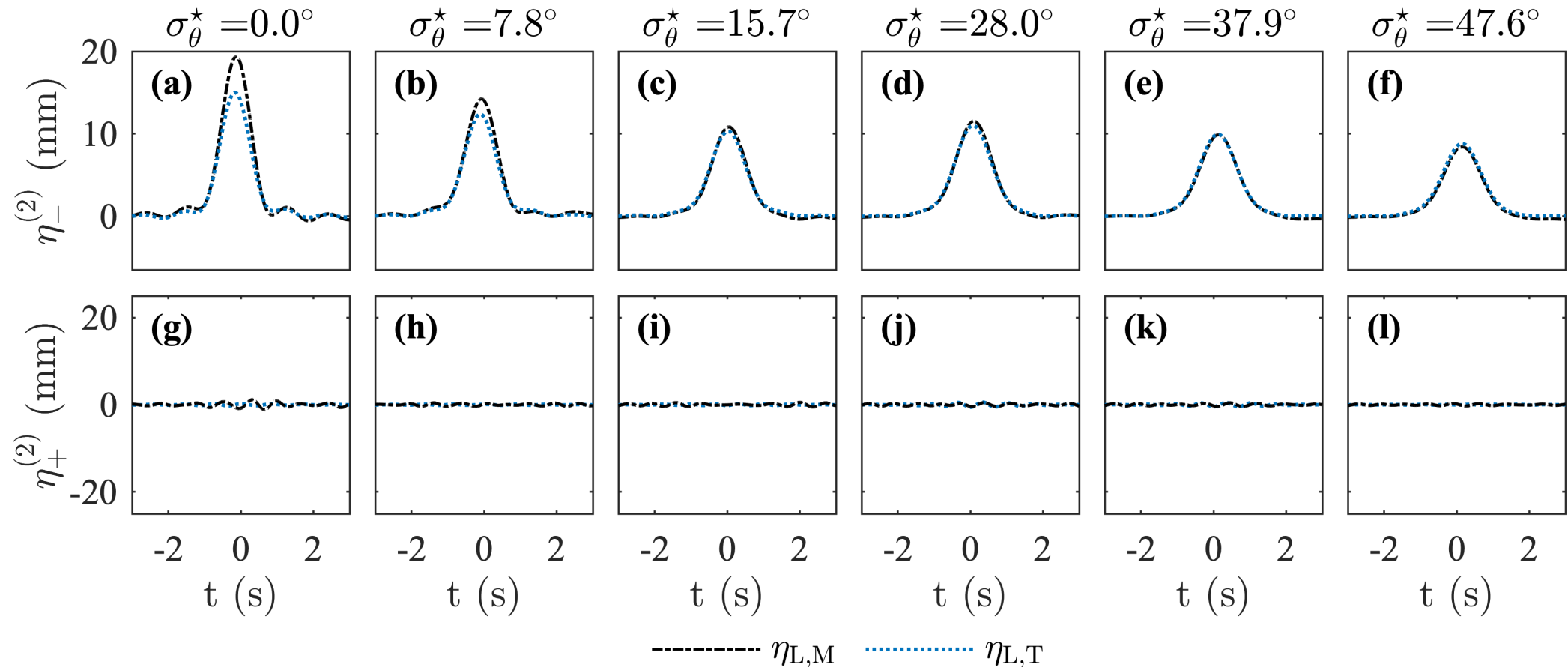




# Second-Order Motion of a Wave-Following Measurement Buoy

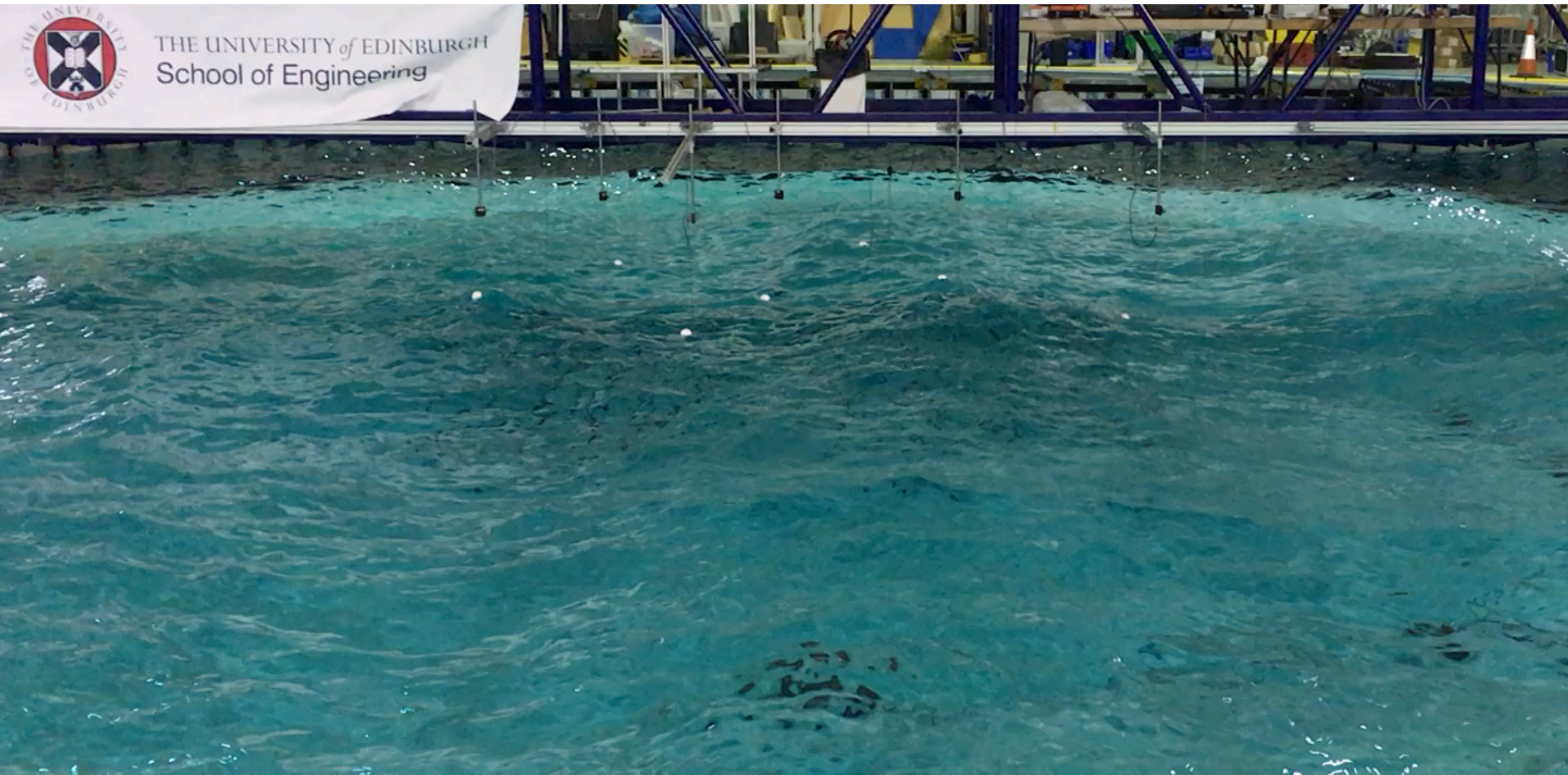


# Second-Order Motion of a Wave-Following Measurement Buoy



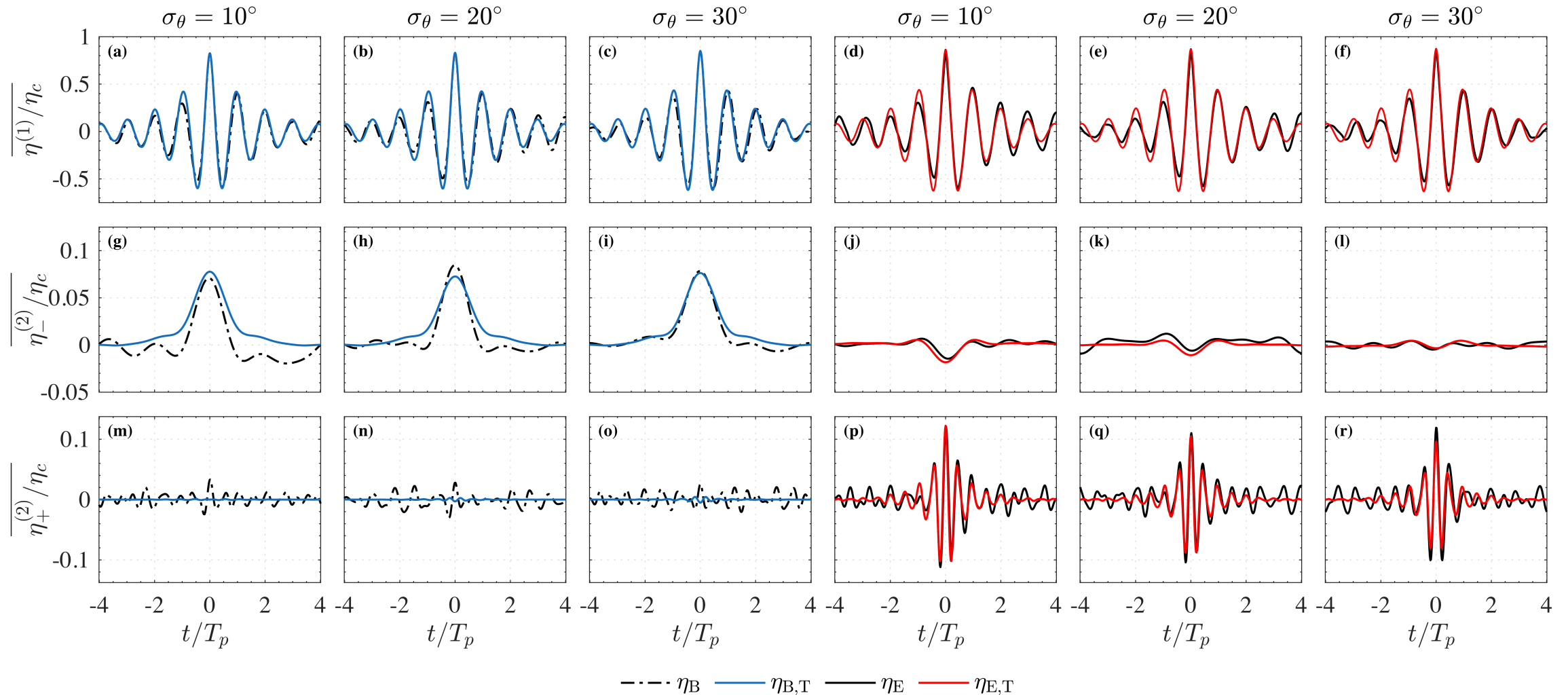


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School of Engineering

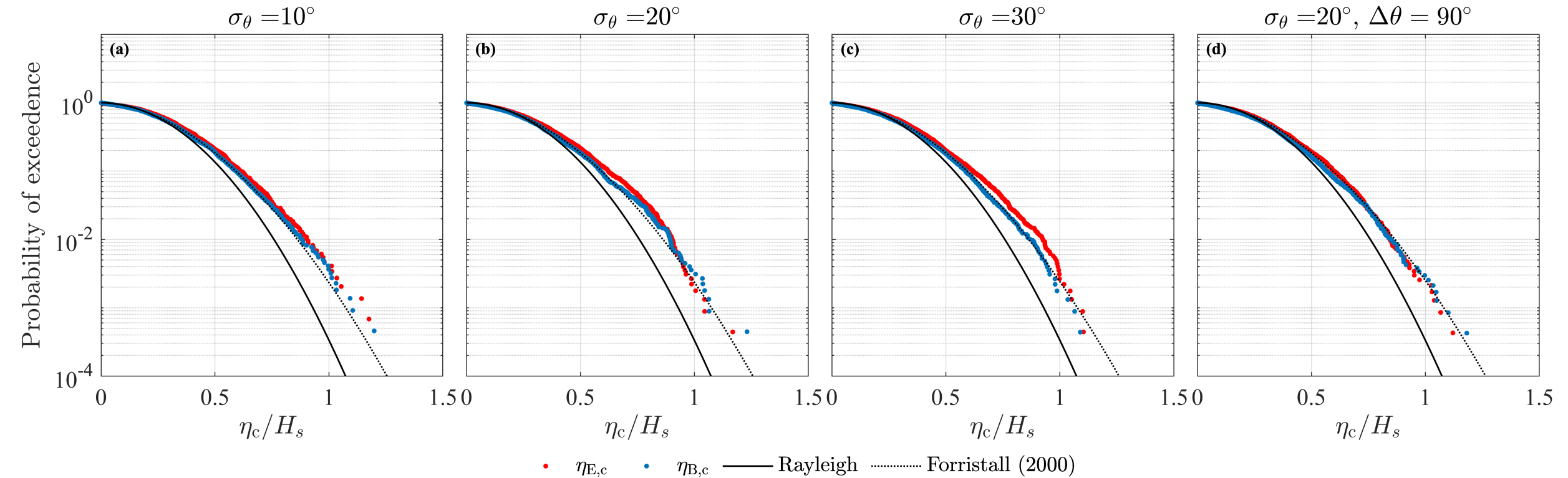




# Statistical Properties of Directionally Spread Ocean Waves Measured by Buoys

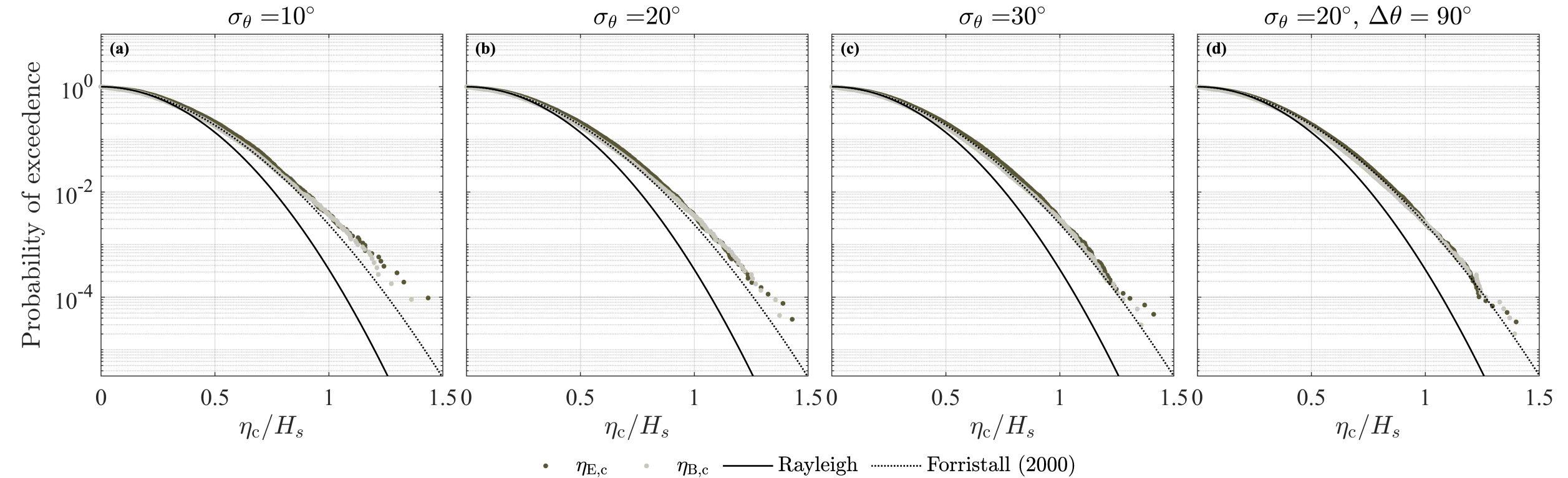


# Statistical Properties of Directionally Spread Ocean Waves Measured by Buoys

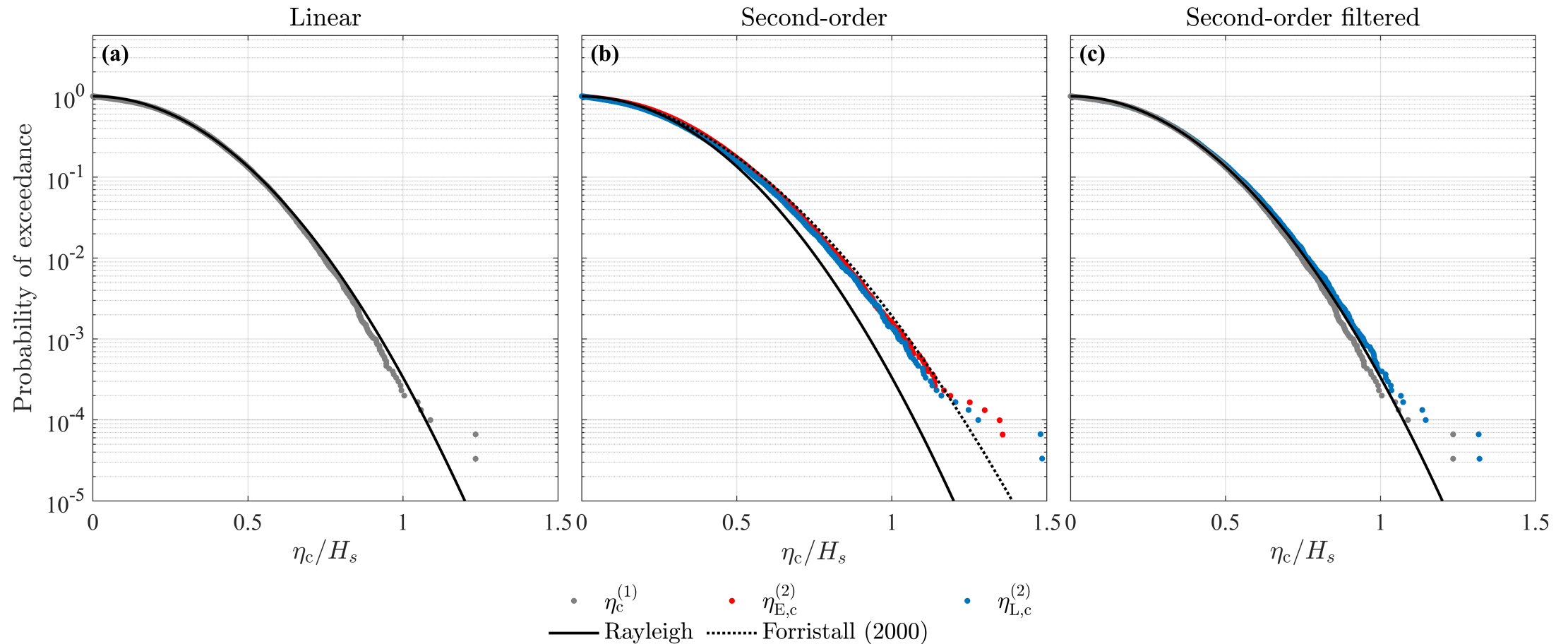




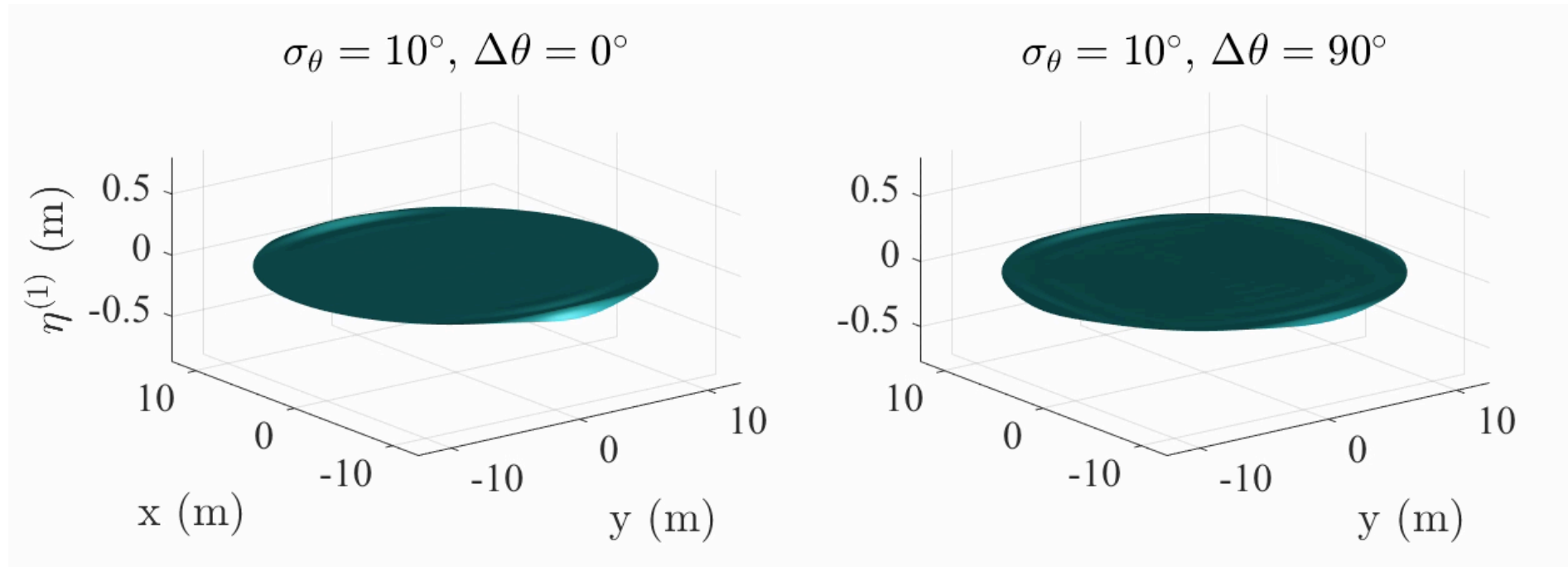
# Statistical Properties of Directionally Spread Ocean Waves Measured by Buoys



# Approximate retrospective correction method for crest heights



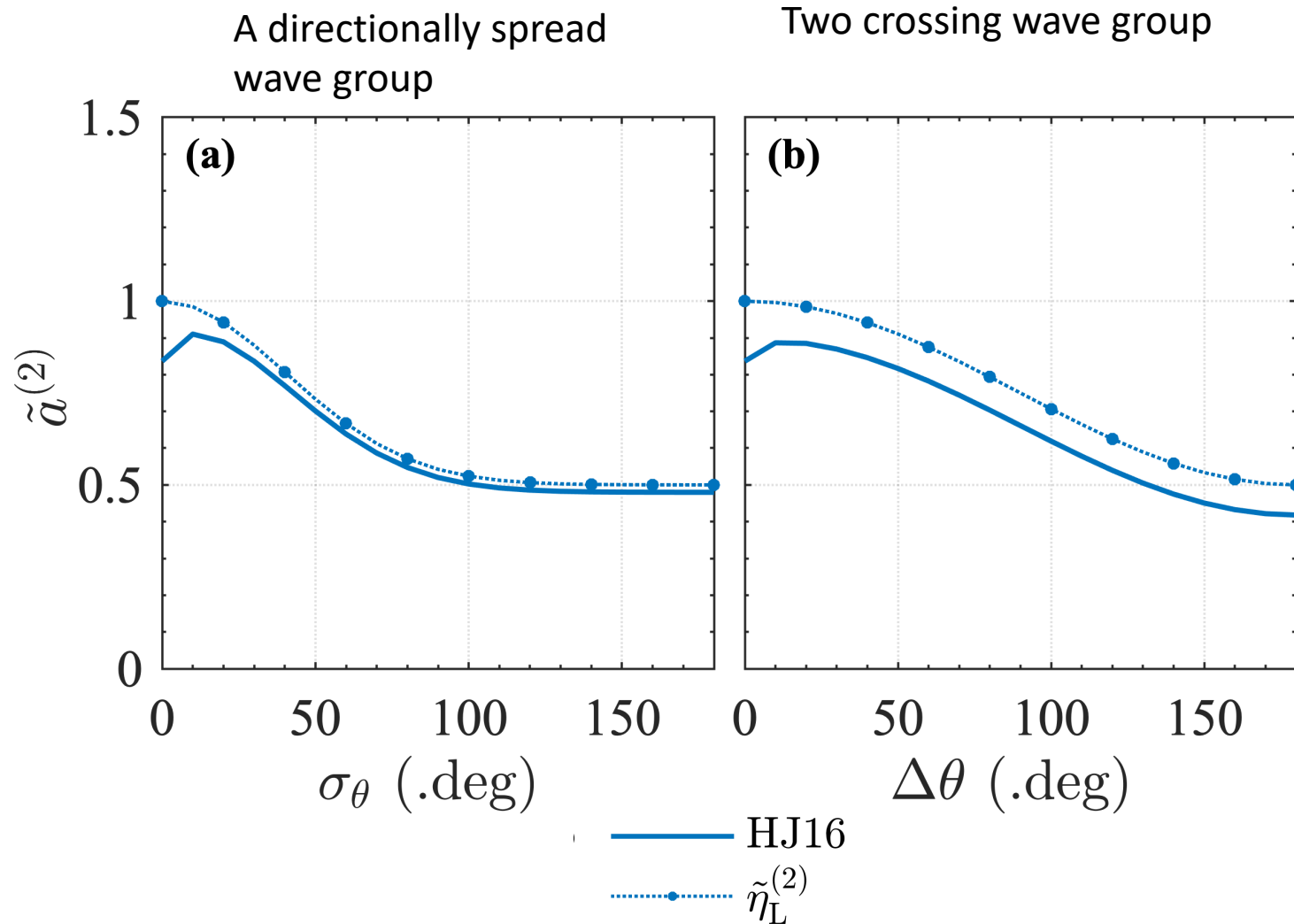
# Approximate retrospective correction method for crest heights



$$\tilde{\eta}^{(2)}(\sigma_\theta) = \frac{1}{2} \left( 1 + e^{-\sigma_\theta^2} \right)$$

$$\tilde{\eta}^{(2)}(\Delta\theta) = \frac{1}{2} + \frac{1}{4} (1 + \cos(\Delta\theta))$$

# Approximate retrospective correction method for crest heights



# Approximate retrospective correction method for crest heights

$$\eta_c \approx \eta_c^{(1)}$$

$$\eta_{Corr,c} = \eta_c + \eta_{c-}^{(2)}$$

# Approximate retrospective correction method for crest heights

$$\eta_c \approx \eta_c^{(1)}$$

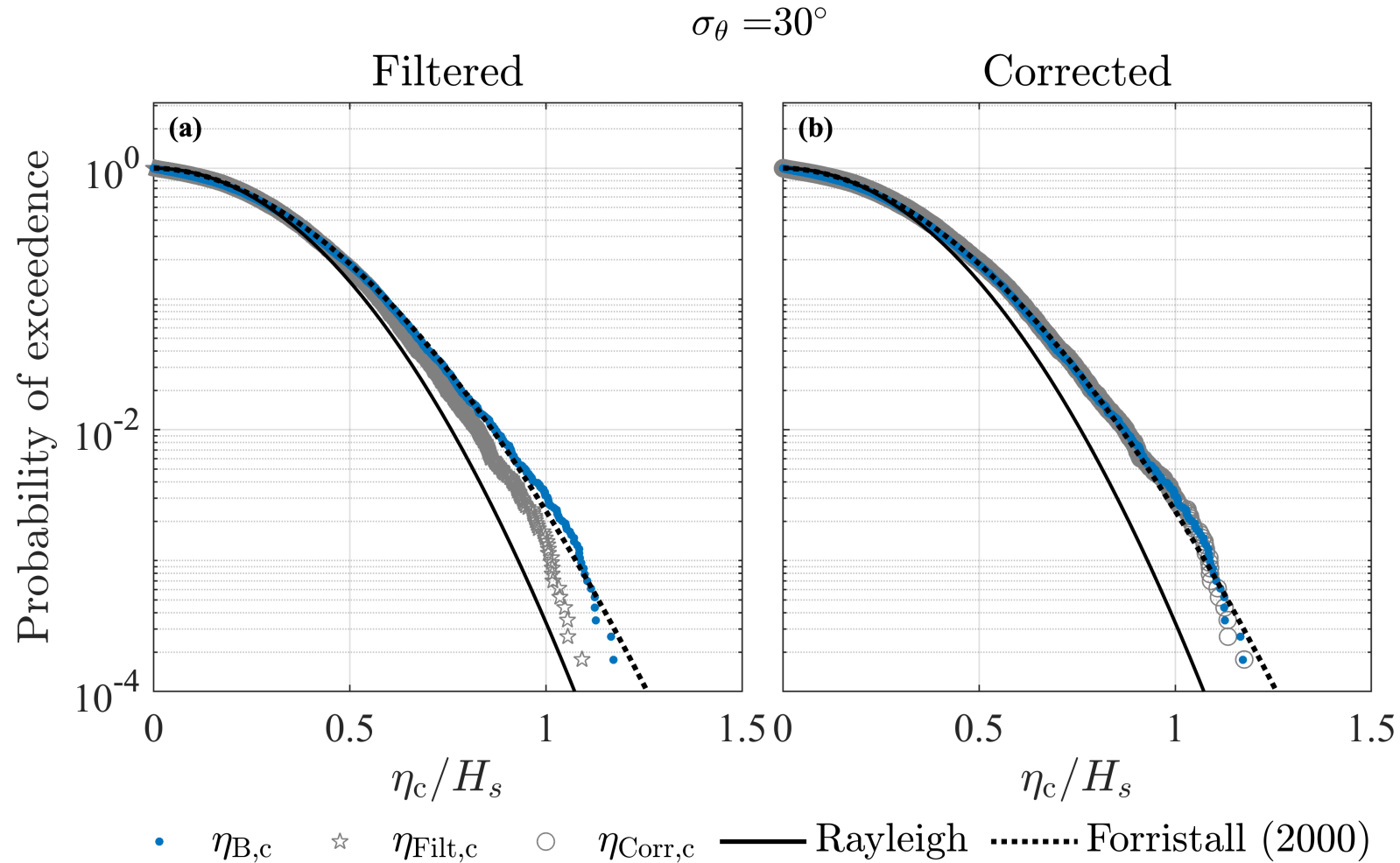
$$\eta_{corr,c} = \eta_c + \eta_{c-}^{(2)}$$

$$\eta_{c-}^{(2)} = \frac{1}{2}(\eta_c)^2 k_0 \tilde{\eta}^{(2)}(\sigma_\theta, \Delta\theta)(1 - \varepsilon_{hpf})$$

$$\tilde{\eta}^{(2)}(\sigma_\theta) = \frac{1}{2} \left( 1 + e^{-\sigma_\theta^2} \right)$$

$$\tilde{\eta}^{(2)}(\Delta\theta) = \frac{1}{2} + \frac{1}{4} (1 + \cos(\Delta\theta))$$

# Approximate retrospective correction method for crest heights





# Conclusions

- In deep water (ocean waves), second-order Lagrangian motion causes the cancellation of super-harmonic ( $\sigma \theta \rightarrow 0$ ) and an increase in sub-harmonic contribution to crest height
- $O(2)$  effects alone will not result in a change to crest height, however, this constitutes a shifting of bound energy from low to high
- For deterministic extreme (non breaking) wave groups buoy motion is essentially purely Lagrangian
- Spectral parameters ( $H_s$ ,  $T_p$ . Etc.) are not significantly different between buoys and gauge measurements
- Filtering slightly affects measured  $H_s$ , and significantly reduces measured skewness  $\lambda^3$
- Wave and crest height measured by buoys and gauges follow the same distributions
- Simplified expressions for second-order contribution to crest height can be used to retrospectively correct measurements and remove the effects of filtering
- These experiments do not consider a realistic mooring configuration, however, if a lack of mooring compliance was to cause an underestimation of crests we believe this would also affect measured wave heights



# Thanks for your attention!

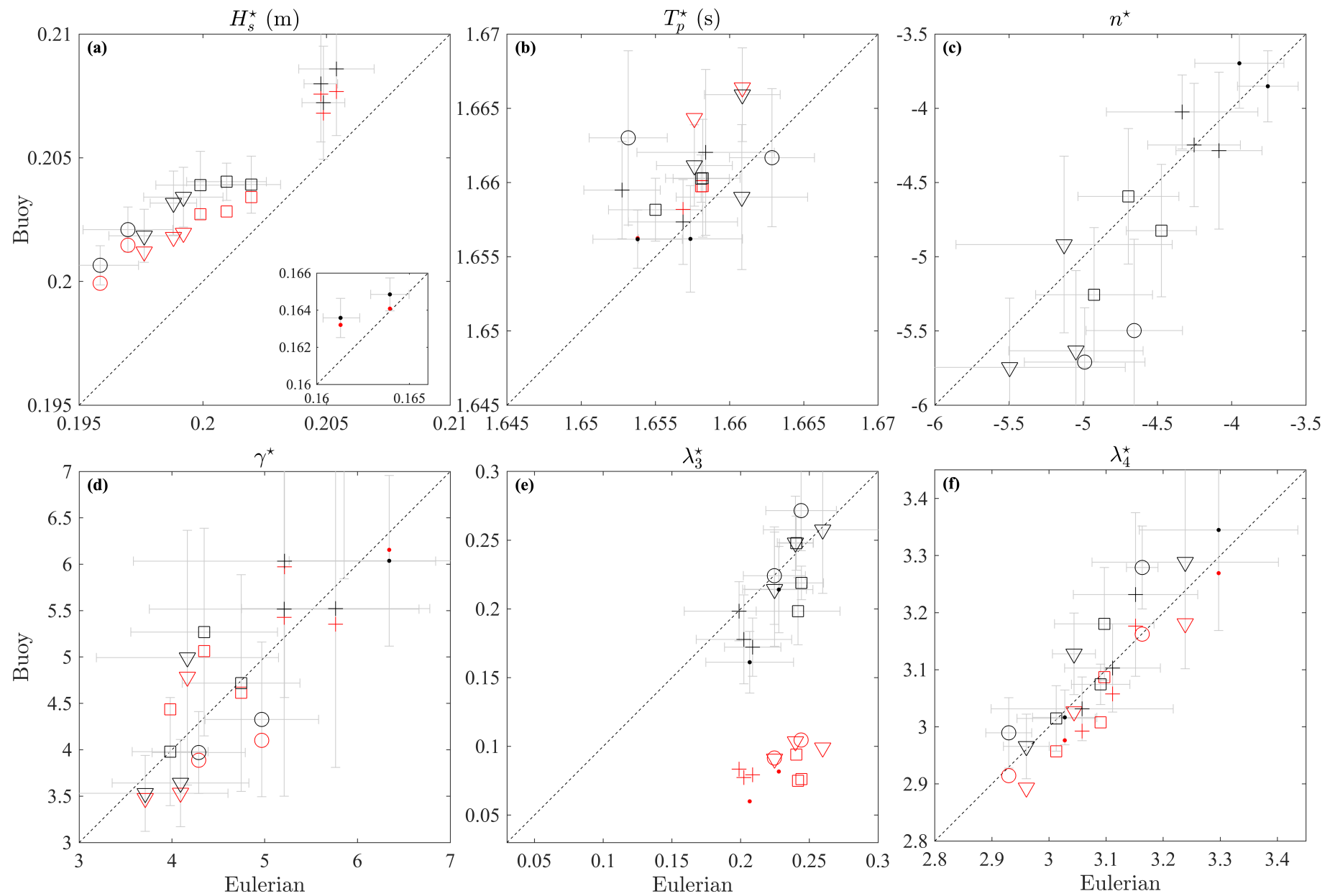
1. M. L. McAllister, and T. S. van den Bremer “Lagrangian Measurement of Steep Directionally Spread Ocean Waves: Second-Order Motion of a Wave-Following Measurement Buoy” **J. Phys. Oceanogr. (in press)**
2. M. L. McAllister, T. S. van den Bremer “Experimental Study of the Statistical Properties of Directionally Spread Ocean Waves Measured by Buoys” **J. Phys. Oceanogr. (in press)**



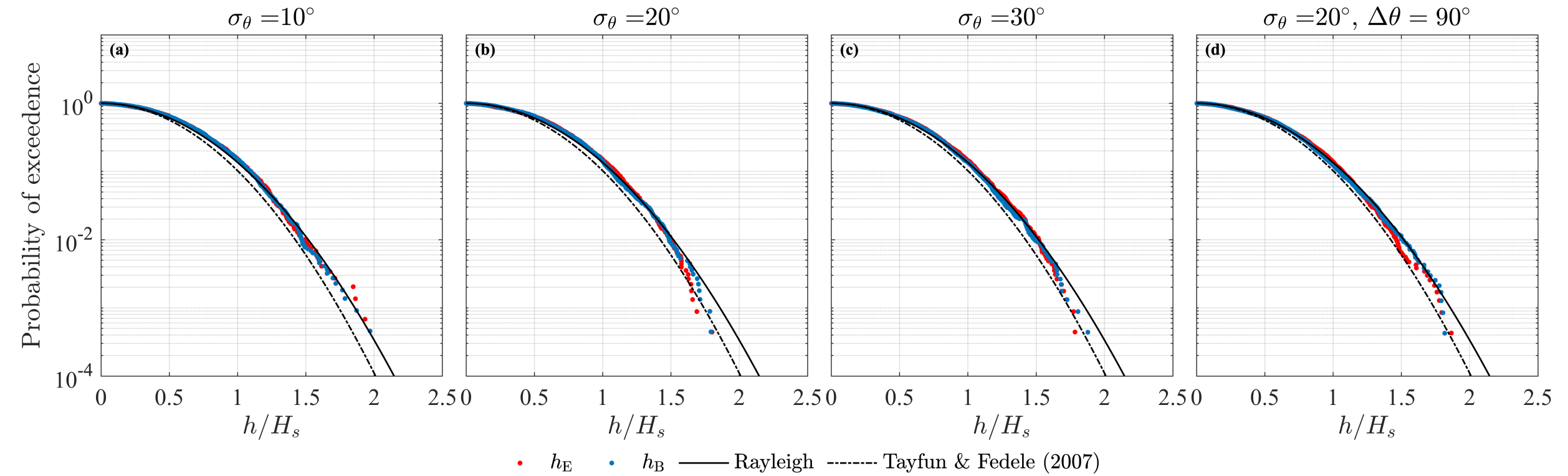
Photo credit: CDIP



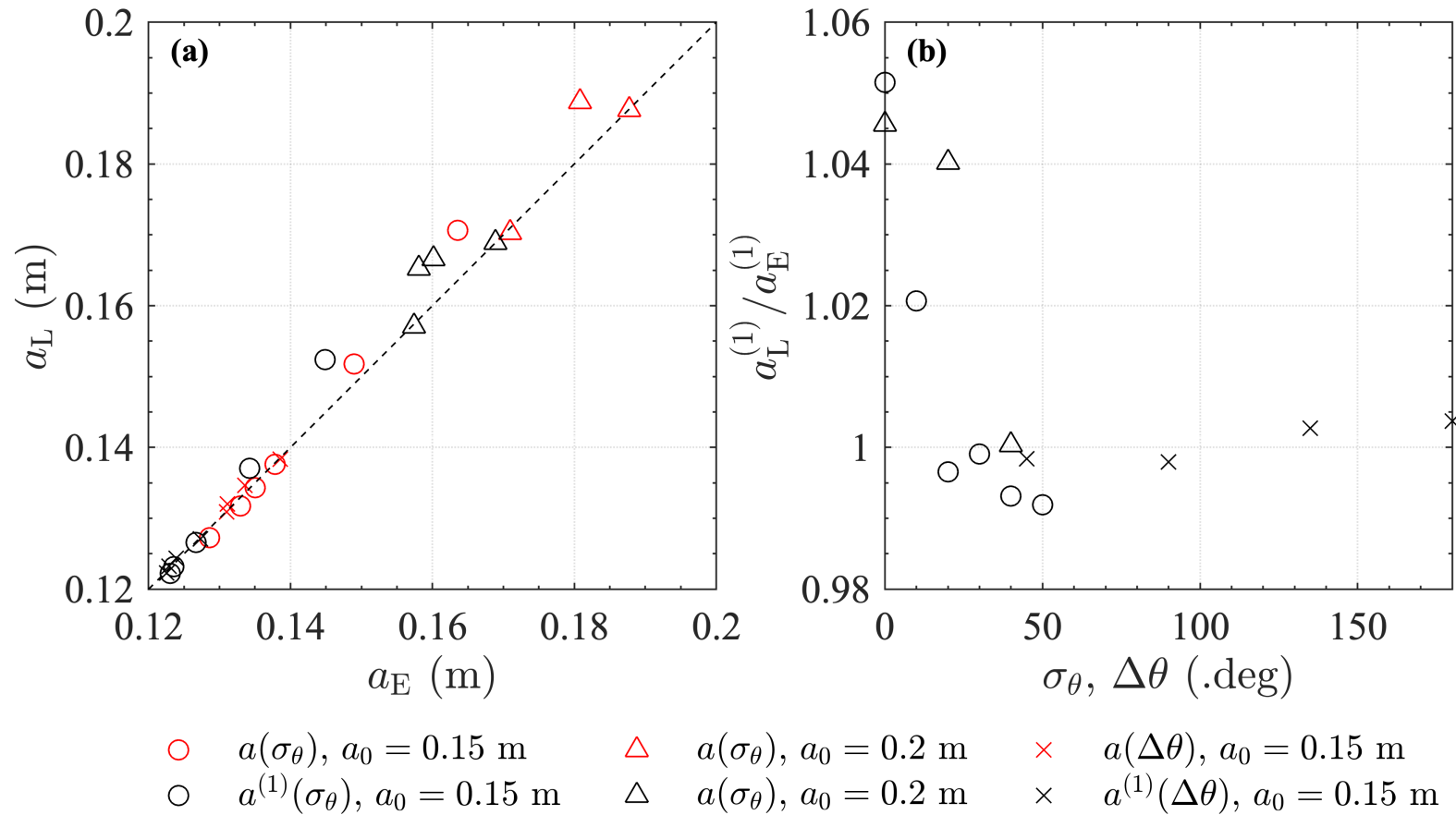
# Spectral Parameters



# Wave height



# Amplitude/Period





# Frequency attenuation

