



NUMERICAL SIMULATION OF DISSOLVED PFAS TRANSPORT IN UNSATURATED SOIL COLUMNS

Transport Phenomena and Porous Media Laboratory

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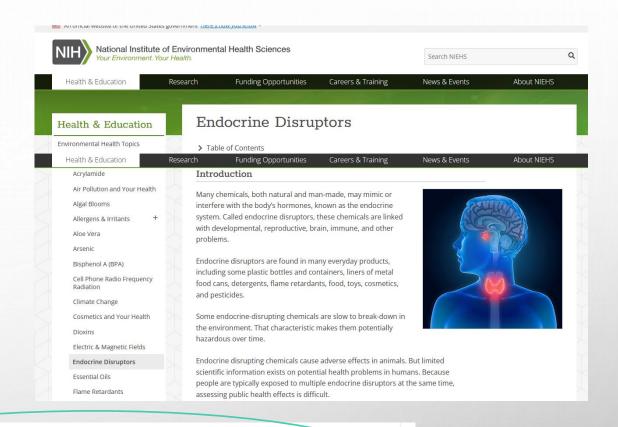




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PFAS





European Chemicals Agency

In addition, the Stockholm Convention regulates the global elimination of perfluorooctanoic acid (PFOA), its salts and PFOA-related compounds. PFOA has been banned under the POPs Regulation since 4 July 2020.

Perfluorohexane sulfonic acid (PFHxS), its salts and related compounds as well as perfluorinated carboxylic acids (C9-14 PFCAs) are being considered for inclusion in the Stockholm Convention and consequent global elimination.

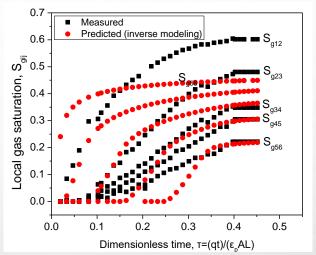
EXPERIMENTAL SETUP & PRELIMINARY RESULTS

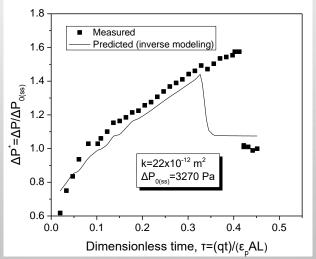
ESTIMATION OF THE WATER/GAS RELATIVE PERMEABILITIES



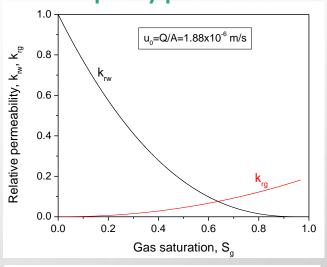
Transient immiscible displacement tests on soil columns

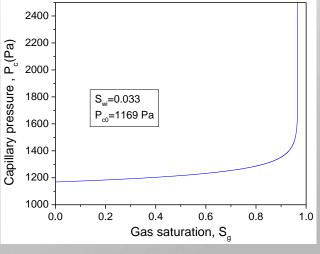
Air injection through a watersaturated sand column





Estimated relative permeability and capillary pressure curves





NUMERICAL MODELS



Case 1: 3D Model simulates the Forced imbibition (two-phase flow) process (without PFOA)

Results: 1. Figure presentation of water volume fraction vs time

2. Flow field

Case 2: 2D PFOA transport (convection, diffusion, dispersion, adsorption)

Results: 1. Figure presentation PFOA concentration distribution over time

2. Figure presentation PFOA vs time at various soil properties

3D-COLUMN MODEL: FORCED IMBIBITION

The purpose of this model is to calculate the volumetric water content over time

Brinkman- Darcy Equation for calculating velocity field inside porous medium

$$\frac{1}{\varepsilon_p} \rho \frac{\partial \overline{u}}{\partial t} = \nabla \left[-P\overline{I} + \overline{k} \right] - \left(\mu k^{-1} + \frac{Q_m}{\varepsilon_p^2} \right) \overline{u} + \rho \overline{g}$$

Phase changes according to Level Set method

$$\frac{\partial \phi}{\partial t} + \overline{u} \nabla \phi = \gamma \nabla \left(\varepsilon_{ls} \nabla \phi - \phi (1 - \phi) \frac{\nabla \phi}{|\nabla \phi|} \right)$$

List of symbols

Ep: porosity

ρ: density

u: Darcy velocity

μ: dynamic viscosity

P: pressure

k: absolute permeability

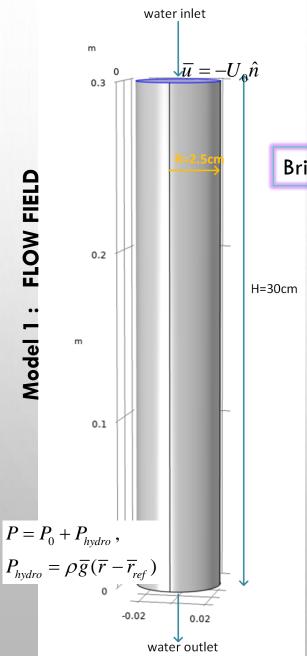
g: gravity acceleration

φ: liquid phase

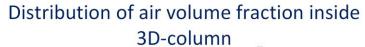
γ:term for numerical

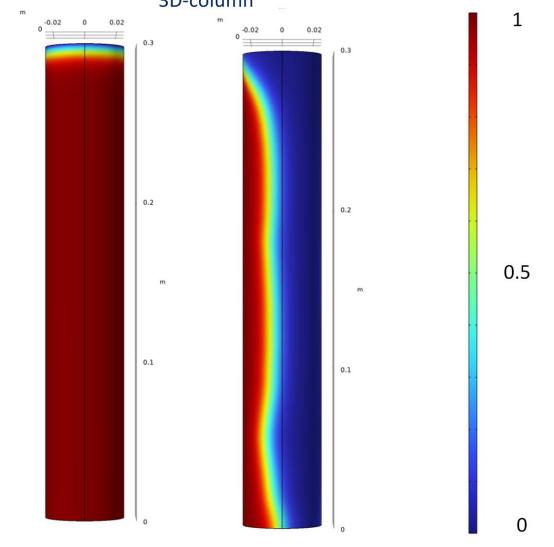
instabilities

Els: interface thickness



AIR & WATER SATURATION CURVE





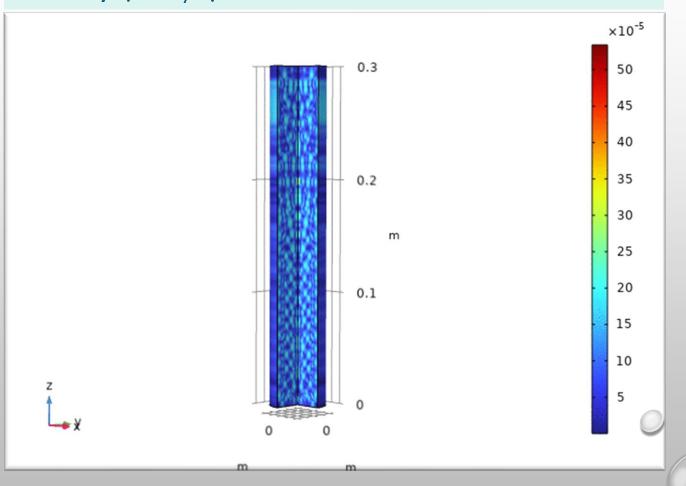
WATER: SATURATION CURVE In 135 min reaches the saturation limit Water fraction

Time in minutes

VELOCITY FIELD VS TIME INSIDE UNSATURATED POROUS MEDIUM

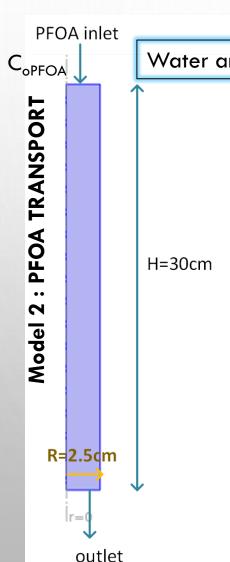
- 0.5 mm/s maximum velocity
- 0.04 mm/s minimum velocity

Velocity (in m/s) distribution inside 3D soil column



2D-COLUMN MODEL BASED ON HYDRAULIC PARAMETERS

The purpose of this model is to simulate the PFOA transport for various rheological properties i.e., hydraulic permeability, saturation curve, fluid compressibility, etc.



Water and dissolved PFOA transport equations in an unsaturated porous medium

$$\rho \left(S_e S_p + \frac{C_m}{\rho g} \right) \frac{\partial p}{\partial t} + \nabla \left(\rho u \right) = 0 \qquad u = -\frac{K}{\rho g} \nabla p$$

$$u = -\frac{K}{\rho g} \nabla p$$

$$\frac{\partial(\varepsilon_{p}c_{i})}{\partial t} + \frac{\partial(\rho c_{p,i})}{\partial t} + \nabla(D_{D} + D_{e})\nabla c_{i} + u\nabla c_{i} = 0$$

Adsorption isotherm Langmuir

$$c_p = c_{p \max} \frac{K_L c}{1 + K_L c}$$

The link between 3D model and the 2D is the saturation term

$$S_e = \frac{\theta - \theta_r}{\theta_s - \theta_r} \qquad K = K_s K_r S_e$$

Lists of Symbols

p: fluid density

Se: effective saturation

Sp: water storage

Ep: porosity

u: Darcy velocity

K: absolute permeability

μ: dynamic viscosity

P: pressure

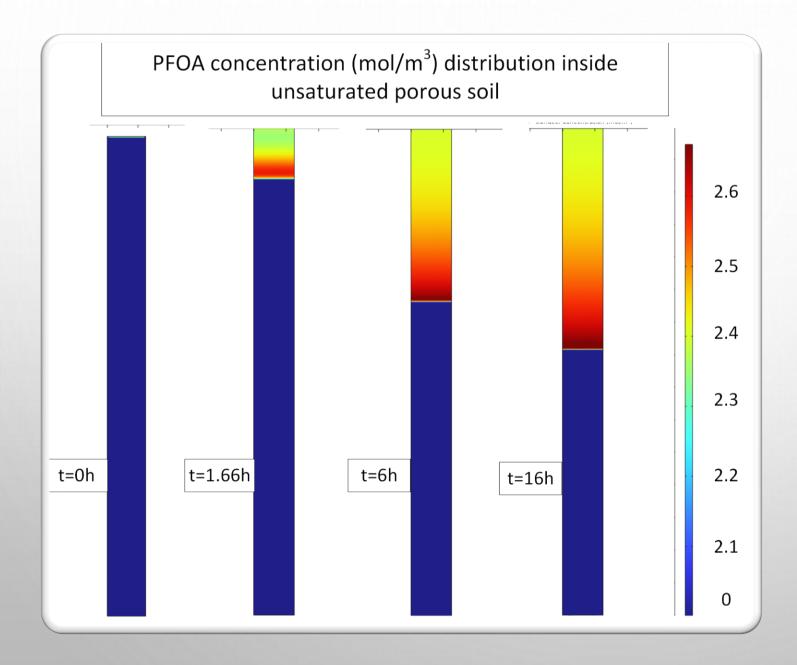
Kr: relative permeability

Ks: hydraulic permeability

θ: vol. water content

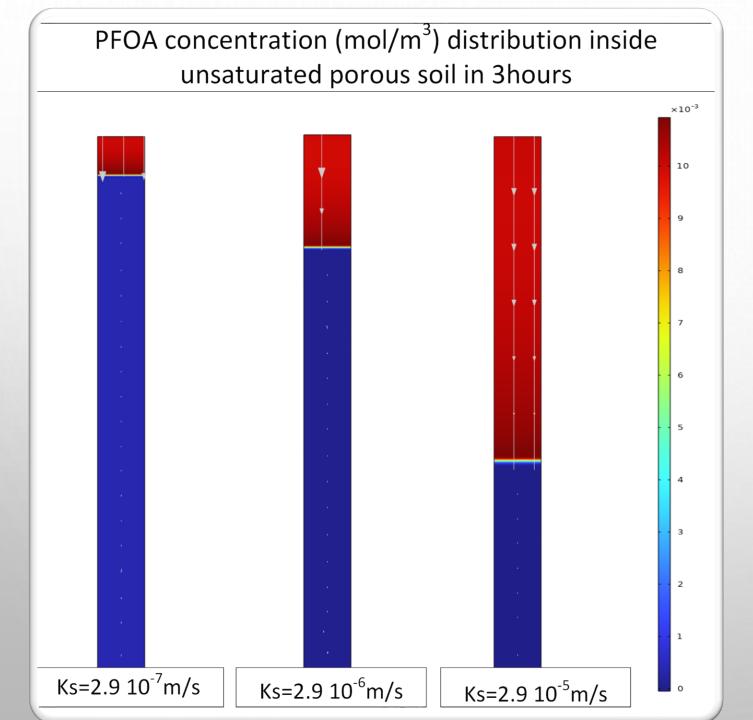
Or: vol. residual water content

θs: saturated vol. water content



VARIANCE OF PFOA CONCENTRATION

- input velocity $u_0 = 3.4 \cdot 10^{-5} \text{ m/s}$
- initial pfoa concentration c₀=2.4mol/m³ or (1g/l)
- initial hydraulic permeability $k_s=2.46 \ 10^{-6} \ m/s$
- dispersivity transverse $\alpha=10^{-5}$ m



DIFFERENT HYDRAULIC PERMEABILITIES AND POROSITIES

- input velocity $u_0=3.4 \ 10^{-5} \ m/s$
- initial pfoa concentration c₀=2.4mol/m³
 or (1g/l)
- dispersivity transverse $\alpha=10^{-5}$ m

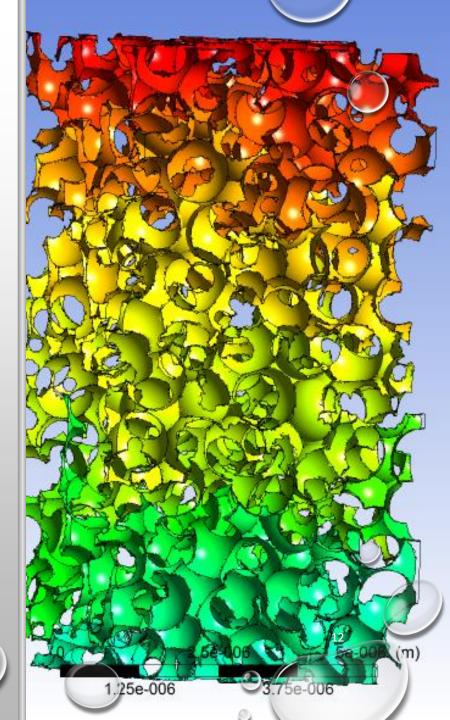


FUTURE WORK

 Calibration of the model based on experiments in column (surface tensions and contact angle with PFAS on the air/water interfaces, PFAS sorption parameters)



Field scale application

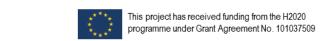


LITERATURE AND MODEL DETAILS

- TSAKIROGLOU, C. D. (2019). "THE CORRELATION OF THE STEADY-STATE GAS/WATER RELATIVE PERMEABILITIES OF POROUS MEDIA WITH GAS AND WATER CAPILLARY NUMBERS." OIL & GAS SCIENCE AND TECHNOLOGY—REVUE D'IFP ENERGIES NOUVELLES 74: 45.
- AGGELOPOULOS, C. AND C. TSAKIROGLOU (2008). "THE EFFECT OF MICRO-HETEROGENEITY AND CAPILLARY NUMBER ON CAPILLARY PRESSURE AND RELATIVE PERMEABILITY CURVES OF SOILS." <u>GEODERMA</u> 148(1): 25-34.
- BRUSSEAU, M. L. AND B. GUO (2021). "AIR-WATER INTERFACIAL AREAS RELEVANT FOR TRANSPORT OF PER AND POLY-FLUOROALKYL SUBSTANCES." WATER RESEARCH **207**: 117785.
- TSAKIROGLOU, C., ET AL. (2012). "FROM APERTURE CHARACTERIZATION TO HYDRAULIC PROPERTIES OF FRACTURES." GEODERMA **181**: 65-77.
- TSAKIROGLOU, C., ET AL. (2003). "NONEQUILIBRIUM CAPILLARY PRESSURE AND RELATIVE PERMEABILITY CURVES OF POROUS MEDIA." <u>AICHE</u> JOURNAL **49**(10): 2472-2486.

COMSOL MULTIPHYSICS®: MODULE CFD (2PHASE FLOW INSIDE POROUS MEDIUM WITH SOME MODIFICATIONS)

ACKNOWLEDGMENTS









ENJOY EGU22

THANKS

Flow-rate dependency of gas/water relative permeabilities

Capillary numbers

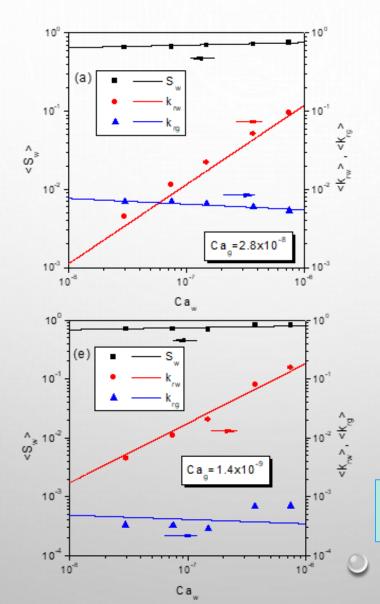
$$Ca_{w} = \mu_{w} q_{w} / (A \gamma_{gw})$$

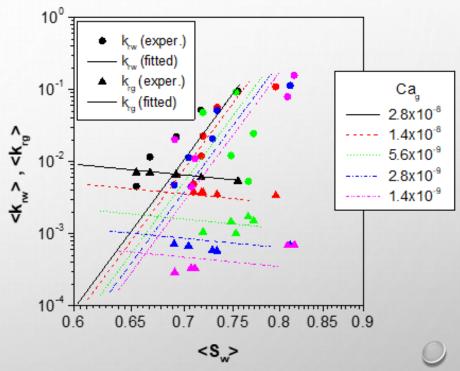
$$Ca_g = \mu_g q_g / (A\gamma_{gw})$$

Power-law dependency

$$\langle k_{rg} \rangle = a_g C a_w^{e_w} C a_g^{e_g}$$
$$\langle k_{rw} \rangle = a_w C a_w^{b_w} C a_g^{b_g}$$

$$\langle S_w \rangle = a_s C a_w^{c_w} C a_g^{c_g}$$





Tsakiroglou, Oil & Gas Science and Technology–Revue d'IFP Energies nouvelles **74**: 45 (2019)