

A turbulence closure scheme in the wave boundary layer and its application in a coupled model

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Introduction

The wind stress in current models is estimated by

$$\tau_a(0) = \rho_a C_d |S_{10}| \mathbf{S}_{10}$$

- ρ_a is the air density
- \mathbf{S}_{10} is the mean wind at 10 m
- $C_d = \frac{\kappa^2}{\ln^2(10/z_0)}$ is the drag coefficient

Over the ocean, the roughness length is estimated

$$z_0 = \alpha \frac{u_*^2}{g} + \frac{0.11 \times \nu_a}{\max(u_*, 0.05)},$$

α is the Charnock coefficient (depend on wave states), ν_a is the air kinematic viscosity.



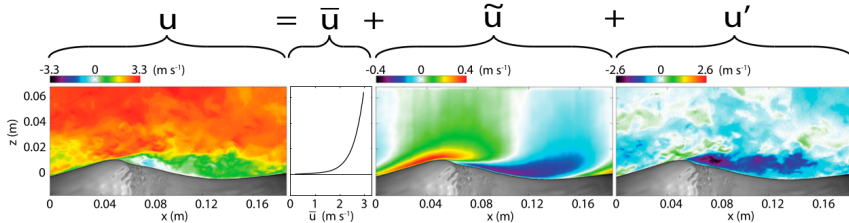
Motivation

Two limitations of current parameterization ($\tau_a(0) = \rho_a C_d |S_{10}| S_{10}$):


1. The wind stress always aligns with wind direction
2. The momentum flux is always from atmosphere to ocean/waves (downward)

Based on eddy-covariance method, $\tau_a = -\overline{u'w'} - \overline{v'w'}$.

In the wave boundary layer,



$$\tau_a = -\overline{u'w'} - \overline{v'w'} - \overline{\tilde{u}\tilde{w}} - \overline{\tilde{v}\tilde{w}}$$

(Buckley and Veron, 2016)  UPPSALA
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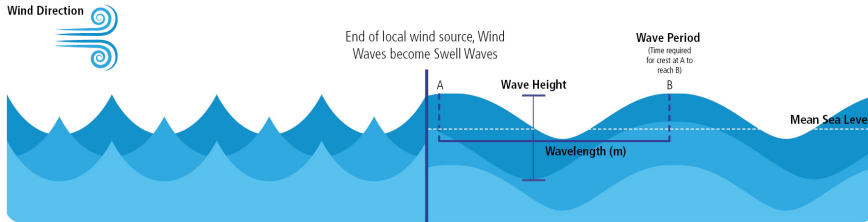
Motivation

WIND WAVES

Wind Waves are generated by immediate local wind. They are not self-sustaining and will die out when the wind stops.

SWELL WAVES

Swell Waves are self-sustaining and generated by energy beneath the ocean's surface, no longer needing local wind.



Waves with long wavelengths and periods arriving from a distant source are considered Swell.

How can we parameterize the stress in WBL?

The wind stress in the wave boundary layer:

$$\tau_a(z) = \tau_t(z) + \tau_v(z) + \tau_{ww}(z) + \tau_{sw}(z),$$

- τ_t shear-induced turbulent stress
- τ_v viscous stress
- τ_{ww} wind wave-induced stress (downward)
- τ_{sw} swell wave-induced stress (upward)

Note:

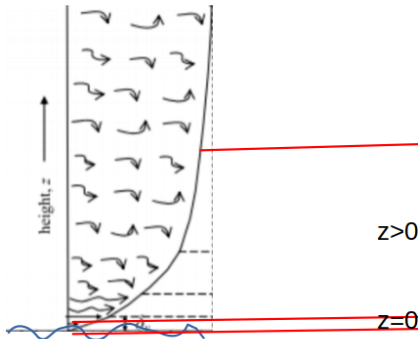
1. Wave-induced stresses can alter from the wind direction.
2. Swell-induced stress is upward (from waves to atmosphere)
3. Wave-induced stress can extend to a certain height.



How can we paramterize the stress in WBL?

The wind stress in the WBL:

$$\tau_a(z) = \tau_t(z) + \tau_v(z) + \tau_{ww}(z) + \tau_{sw}(z),$$



At air-sea interface ($z \approx 0$), the shear-induced stress approaches to 0:, then

$$\tau_a(0) = \tau_v(0) + \tau_{ww}(0) + \tau_{sw}(0)$$

In the wave boundary layer ($z > 0$): $\tau_{ww}(z)$ decay faster and $\tau_v(z)$ approach 0, then

$$\tau_a(z) = \tau_t(z) + \tau_{sw}(z)$$



How can we parameterize the stress in WBL?

The wind stress terms are estimated by:

$$\tau_v(0) = \rho_a C_v |S_{10}| \mathbf{S}_{10}$$

$$\tau_{ww}(0) = \rho_w g \int_0^{2\pi} \int_0^\infty \frac{\mathbf{k}}{\omega} S_{in} d\omega d\theta,$$

$$\tau_{sw}(0) = \rho_w g \int_0^{2\pi} \int_0^\infty \frac{\mathbf{k}}{\omega} S_{out} d\omega d\theta,$$

$$\tau_t(z) = -\rho_a K_m \frac{dS}{dz},$$

$$\tau_{sw}(z) = \tau_{sw}(0) e^{-Ak_p z}$$

Note:

1. $\tau_v(0)$, $\tau_t(z)$ align with the mean wind direction.
2. The direction of $\tau_{ww}(z)$ and $\tau_{sw}(z)$ is determined by 2D wave spectrum.



How can we parameterize the stress in WBL?

In current models, the wind speed at 10 m,

$$S_{log}(z) = \frac{u_*}{\kappa} \left[\ln \frac{z}{z_0} - \psi_m(z/L) \right].$$

After considering the wave-induced stress:

$$U_{10} = S_{log}(10) \cos(\theta_{wind}) - S_{sw}(10) \cos(\theta_{sw})$$

$$V_{10} = S_{log}(10) \sin(\theta_{wind}) - S_{sw}(10) \sin(\theta_{sw}),$$

in which θ_{wind} and θ_{sw} are the wind direction and the direction of the swell-induced stress. and

$$\mathbf{s}_{sw}(z) = \frac{\tau_{sw}(0)}{\rho_a \kappa u_*} \int_{\infty}^z e^{-Ak_p z} / z dz. \quad (1)$$



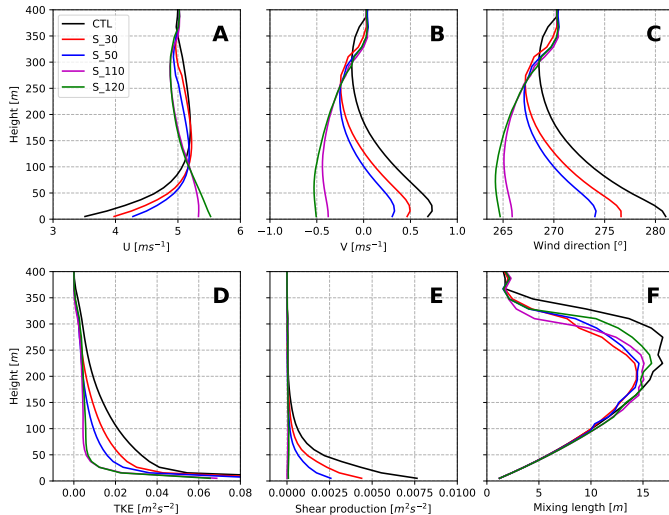
WRF-SCM simulations

Simulations using the single-column version of the Weather Research and Forecasting Model (WRF-SCM)

- MYNN-2.5 turbulence closure scheme
- 100 vertical layers in the bottom 6 km of the atmosphere.
- 5 m in the lowest model level and 16 layers are in the lowest 200 m
- The geostrophic wind is $U_g = 5 \text{ ms}^{-1}$ and $V_g = 0 \text{ ms}^{-1}$.
- The initial conditions of the wind and temperature are from the Large-Eddy simulation (ZN1) in Nilsson et al., 2012.
- The friction velocity is 0.11 ms^{-1} in all simulations.

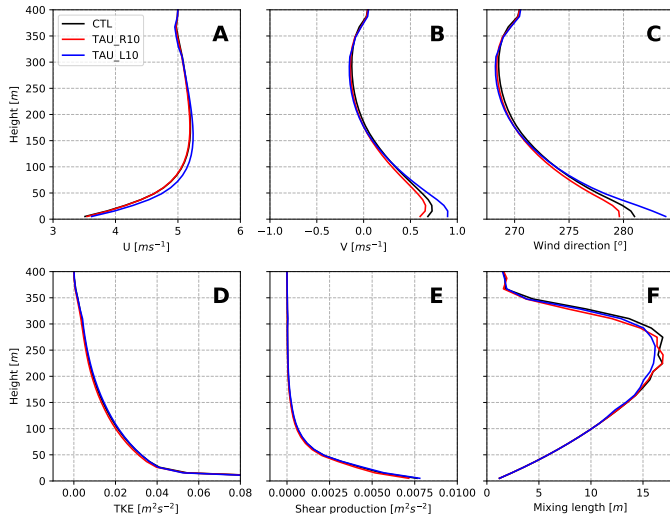


Impact of τ_{sw} :



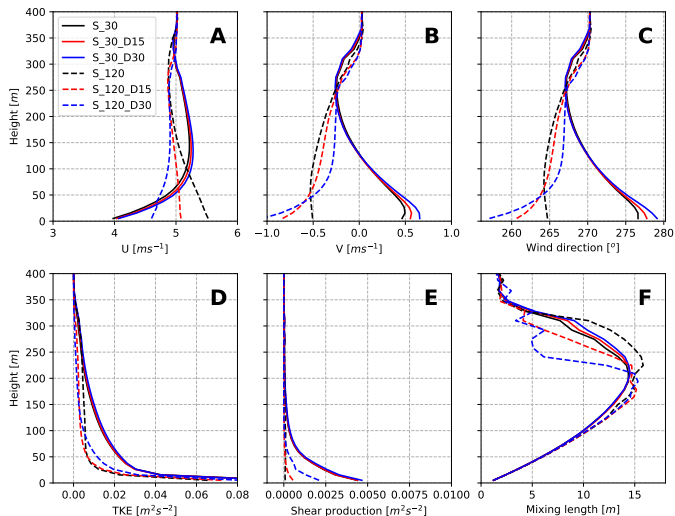
- $\tau_{sw}(0)$ aligns with wind.
- xx in name S_{xx} represents $\tau_{sw}(0)/\tau_l$
 τ_l is the downward momentum flux
- Neutral condition

Impact of the direction difference between τ_I and S_{10} :



- $\tau_{sw}(0) = 0$
- The direction difference between τ_I and S_{10} is 10° on the right and left in R_{10} and L_{10} , respectively
- Neutral condition

Impact of the direction difference between τ_{sw} and S_{10} :

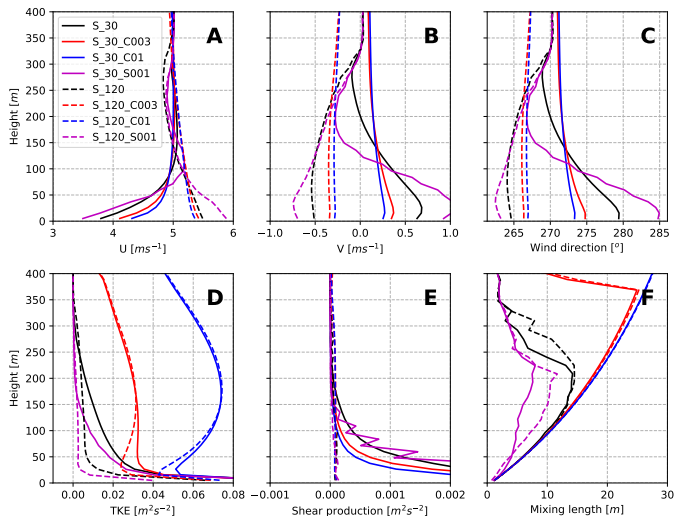


xx and yy in the name
 S_{xx_Dyy}

- xx represent τ_{sw}/τ_I
- yy represent the direction difference between τ_{sw} and τ_I



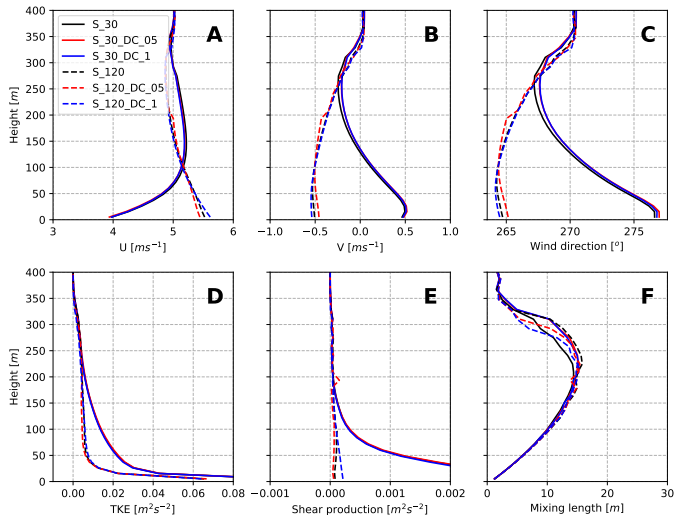
Impact of the atmospheric stability:



xx and yy in the name
 S_{xx_Cyy} or S_{xx_Syy}

- xx represent τ_{sw}/τ_l
- yy represent the heat flux in convective (C) or stable (S) conditions

Impact of the decay coefficient of swell-induced upward momentum flux:



xx and yy in the name
 S_{xx_DCyy}

- xx represent τ_{sw}/τ_I
- yy represent the decay coefficient A in

$$\tau_{sw}(z) = \tau_{sw}(0)e^{-Ak_p z}$$



Real case simulations

One-month long simulations (Jan., 2017) are done over the ocean off California using an atmosphere-wave coupled model (UU-CM).

Control experiment:

$$\tau_a(0) = \rho_a C_d |\mathbf{S}_{10}| \mathbf{S}_{10},$$

$$z_0 = \alpha \frac{u_*^2}{g} + \frac{0.11 \times \nu_a}{\max(u_*, 0.05)},$$

$$\alpha = \frac{0.0095}{\sqrt{1 - \tau_{ww}(0)/\tau_l}}.$$

$$S_{log}(z) = \frac{u_*}{\kappa} \left[\ln \frac{z}{z_0} - \psi_m(z/L) \right].$$



Real case simulations

One-month long simulations (Jan., 2017) are done over the ocean off California using an atmosphere-wave coupled model (UU-CM).

Coupled experiment:

- At air-sea interface ($z \approx 0$)

$$\tau_a(0) = \tau_v(0) + \tau_{ww}(0) + \tau_{sw}(0)$$

- In the wave boundary layer ($z > 0$):

$$\tau_a(z) = \tau_t(z) + \tau_{sw}(z)$$

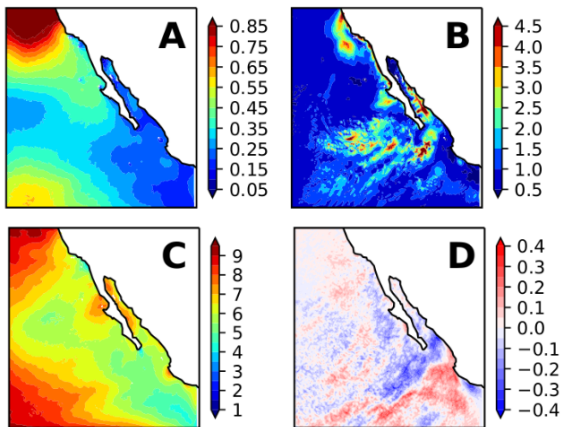
- The wind speed at 10 m:

$$U_{10} = S_{log}(10)\cos(\theta_{wind}) - S_{sw}(10)\cos(\theta_{sw})$$

$$V_{10} = S_{log}(10)\sin(\theta_{wind}) - S_{sw}(10)\sin(\theta_{sw}),$$

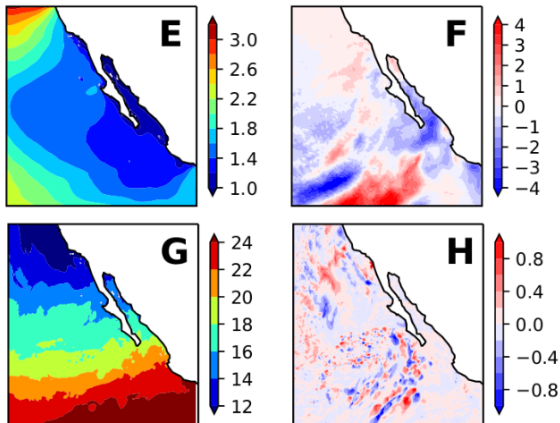


Real case simulations



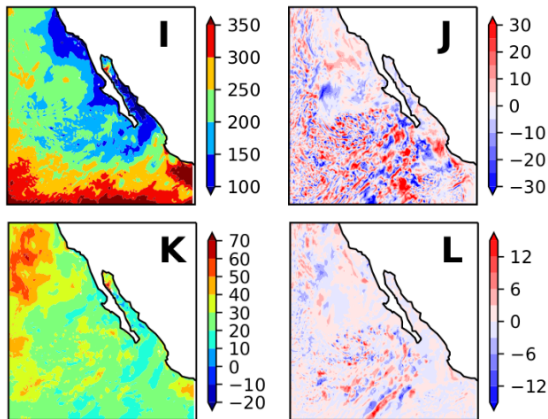
(A): the mean τ_{SW} [$\times 10^{-3} Nm^{-2}$], (B) the ratio of the mean τ_{SW} and τ_I [%]
(C) the mean S_{10} [ms^{-1}], (D) the difference of S_{10} between FUL and CTL [ms^{-1}]

Real case simulations



(E) the mean H_s [m], (F) the difference of H_s between FUL and CTL [cm]
(G) the mean T_2 [°C], (H) the mean difference of T_2 between FUL and CTL [°C]

Real case simulations



(I) the mean latent heat flux [Wm^{-2}], (J) the difference between FUL and CTL [Wm^{-2}]
(K) the mean sensible heat flux [Wm^{-2}], (L) the difference between FUL and CTL [Wm^{-2}].

Conclusions

- The swell-induced upward momentum flux increases the surface wind and changes the wind direction
- The misalignment between the upward momentum flux and wind has a more significant impact on the wind profile than that from the downward momentum flux
- The impact of swell-induced upward momentum flux decreases with atmospheric convection.
- The surface wind can be altered up to 5% by ocean surface gravity waves over the ocean off California.

