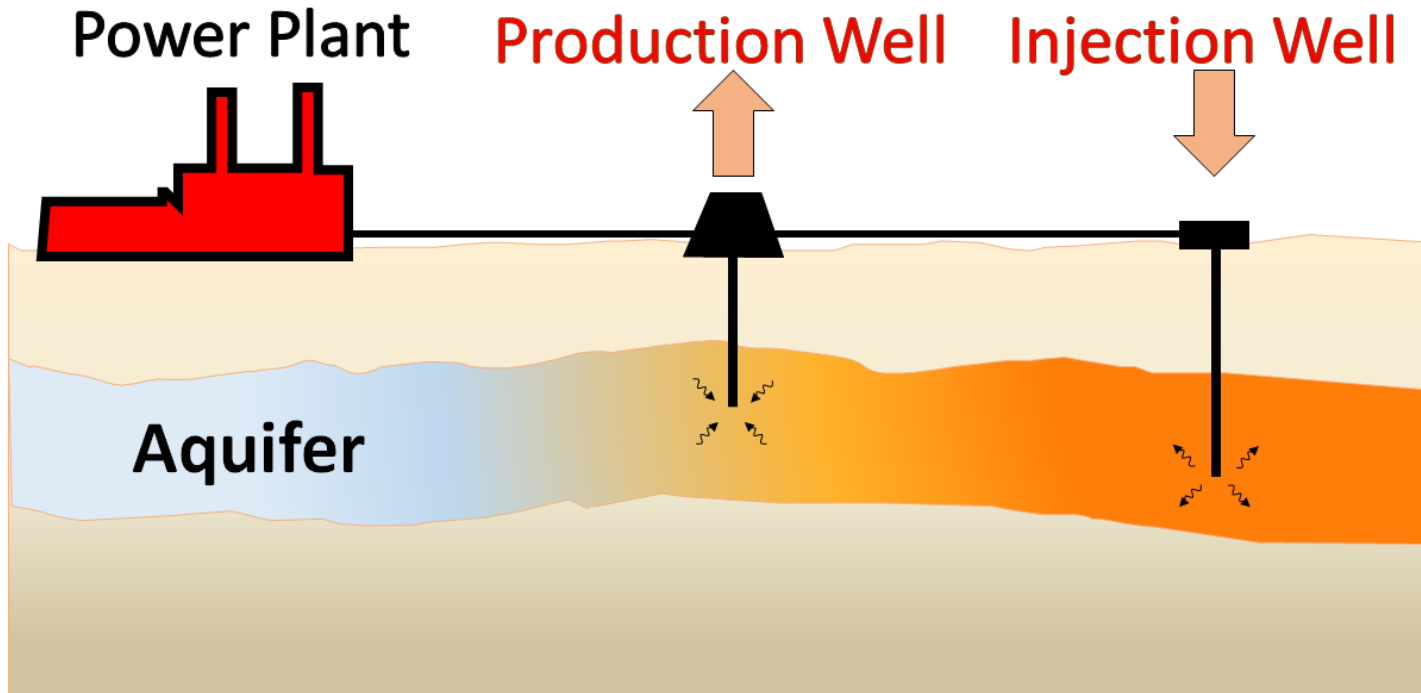


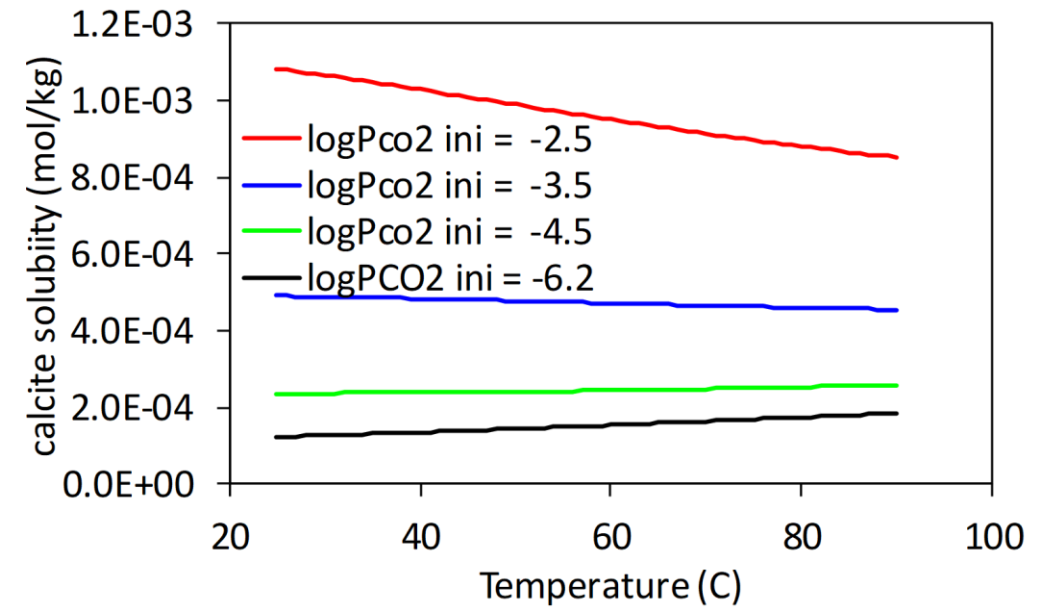
A NOVEL METHOD FOR THC MODELS FOR AQUIFER THERMAL ENERGY STORAGE

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Maarten W. Saaltink

THERMAL IMPACT



**Aquifer Thermal
Energy Storage**



Precipitation / Dissolution

INDEX

- 1. Methodology to obtain a (semi-)analytical solution**
 - Verification of numerical models
 - Understanding thermo-hydro-chemical phenomena
- 2. Application to HT-ATES**
 - HEATSTORE benchmark inspired by Bern project

METHODOLOGY

- Rate of chemical reaction (De Simoni et al., 2007):

$$r = \underbrace{\frac{\partial^2 c}{\partial \alpha^2} (\nabla \alpha)^T}_{\text{Chemistry factor}} \underbrace{\phi \mathbf{D} \nabla \alpha}_{\text{Transport factor}}$$

- Reactive transport for calcite dissolution rate:

$$r_{\text{calcite}} = \phi \frac{\partial (c_{Ca} - c_{Mg})}{\partial t} + \mathbf{q} \cdot \nabla (c_{Ca} - c_{Mg}) - \nabla \cdot (\phi \mathbf{D} \nabla (c_{Ca} - c_{Mg}))$$

- Heat equation for temperature (T):

$$\phi R C_a \frac{\partial T}{\partial t} + C_a \mathbf{q} \cdot \nabla T - \nabla \cdot (\lambda \nabla T) - \nabla \cdot (\phi C_a \mathbf{D}_{dis} \nabla T) = 0$$

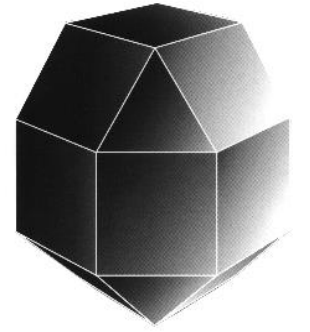
- Heat equation substituted in reactive transport equations:

$$r_{\text{calcite}} = \underbrace{-\frac{\partial^2 (c_{Ca} - c_{Mg})}{\partial T^2} (\nabla T)^T \phi \mathbf{D} \nabla T}_{\text{Mixing}} + \underbrace{\frac{\partial (c_{Ca} - c_{Mg})}{\partial T} \left[(1-R) \phi \frac{\partial T}{\partial t} - \nabla \cdot ((\phi D_{dif} - C_a^{-1} \lambda) \nabla T) \right]}_{\text{Heat retardation} \quad \text{Heat conduction}}$$

ALGORITHM

1. Thermo-hydraulics

$$q \quad T \quad \nabla T \quad \nabla^2 T \quad \frac{\partial T}{\partial t}$$



2. Chemistry: concentration – temperature

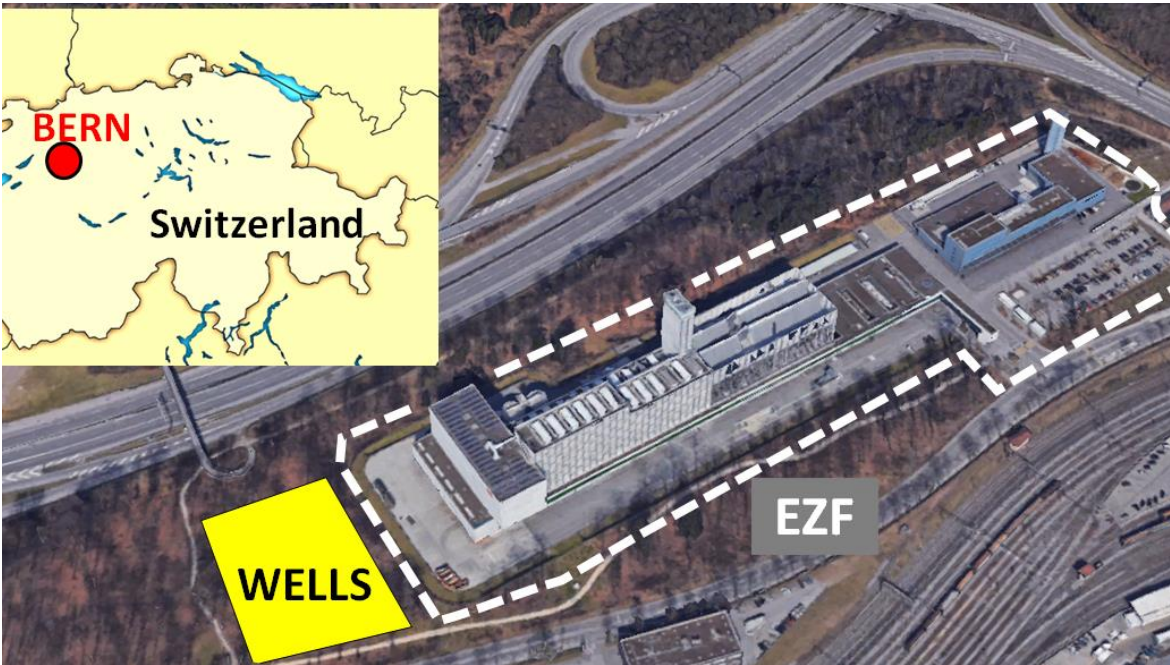
$$c_{Ca} \quad \frac{\partial c_{Ca}}{\partial T} \quad \frac{\partial^2 c_{Ca}}{\partial T^2}$$



3. Dissolution rate (r)

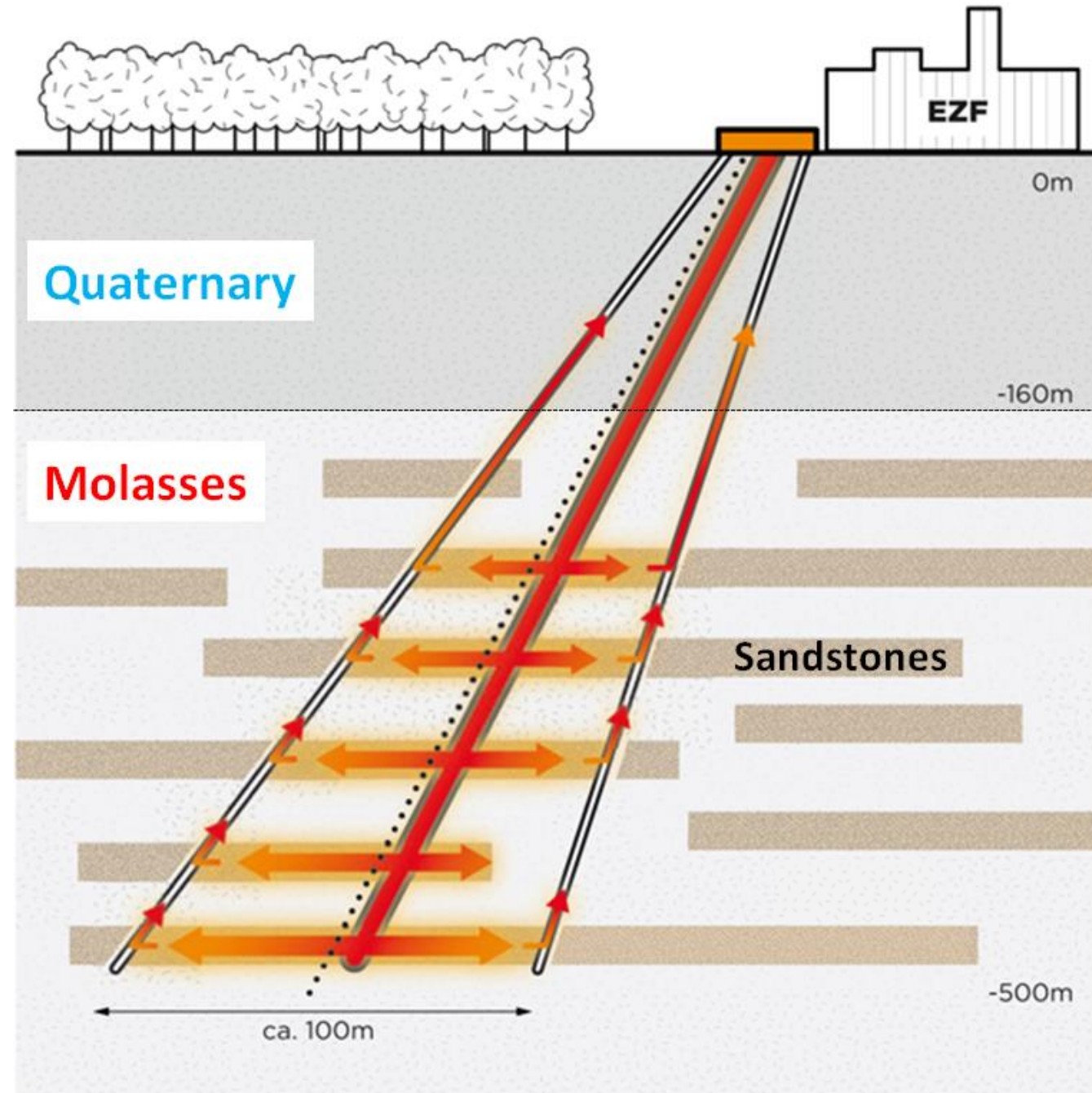
$$r_{calcite} = -\frac{\partial^2 (c_{Ca} - c_{Mg})}{\partial T^2} (\nabla T)^T \phi \mathbf{D} \nabla T + \frac{\partial (c_{Ca} - c_{Mg})}{\partial T} \left[(1 - R) \phi \frac{\partial T}{\partial t} - \nabla \cdot ((\phi D_{dif} - C_a^{-1} \lambda) \nabla T) \right]$$

PILOT PROJECT

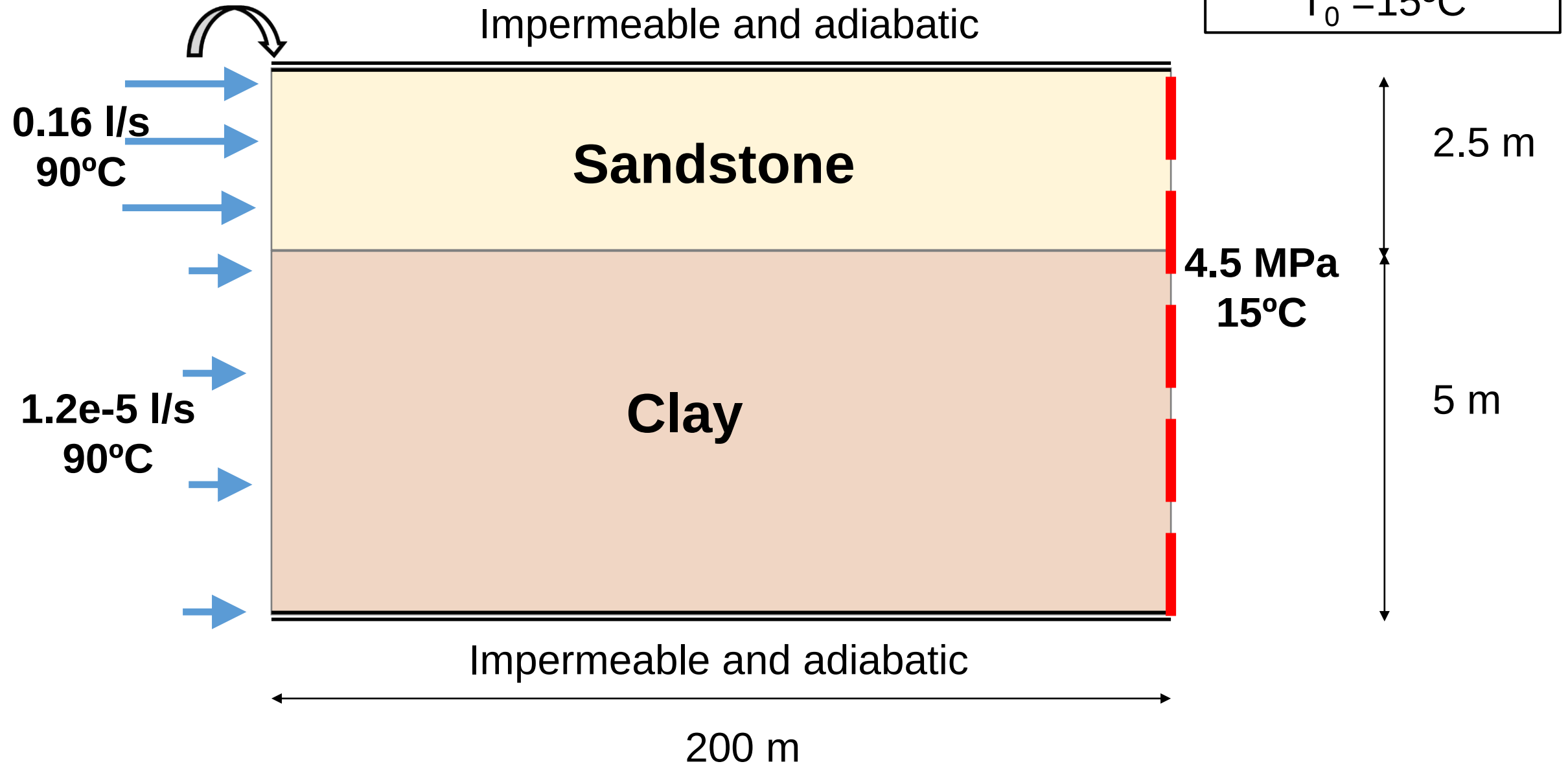


INJECTION: 0 - 216 days

EXTRACTION: 216 - 365 days



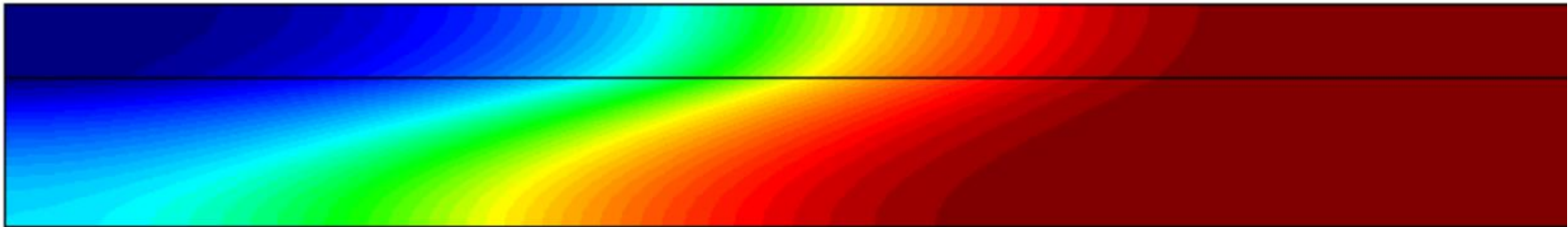
TH MODELLING



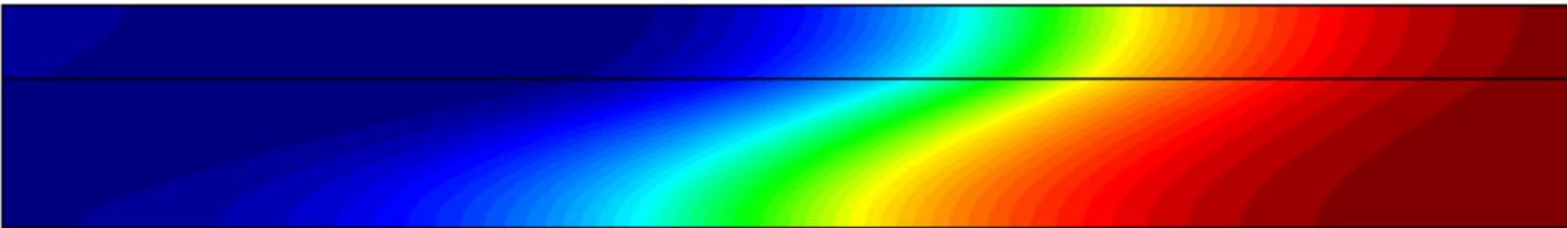
CONCENTRATION

INJECTION (216 days)

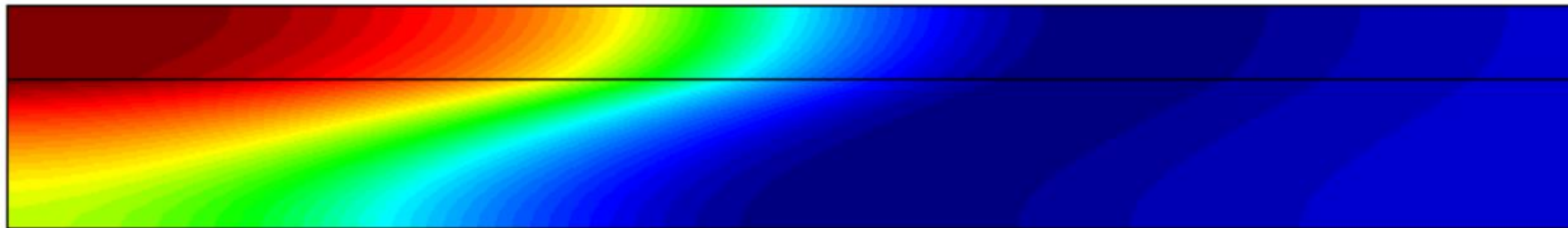
$$c_{Ca}(T)$$



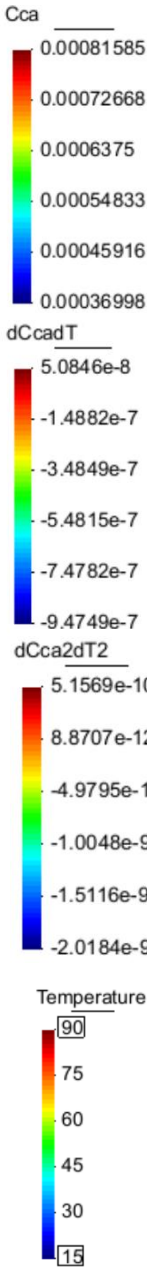
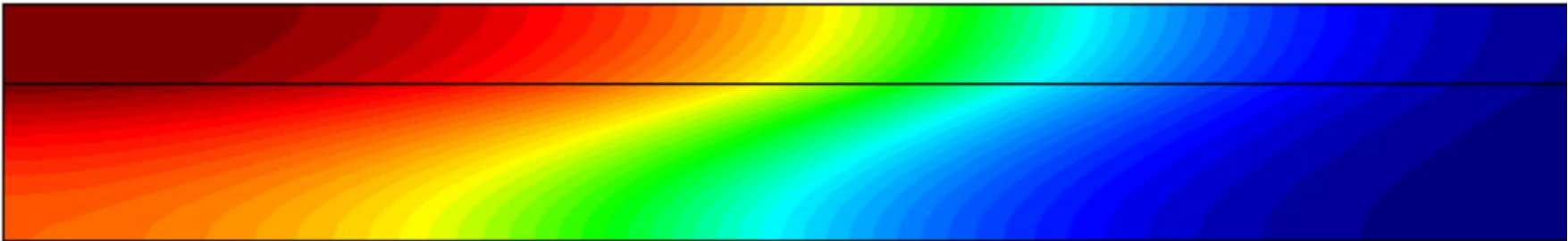
$$\frac{\partial c_{Ca}}{\partial T}(T)$$



$$\frac{\partial^2 c_{Ca}}{\partial T^2}(T)$$



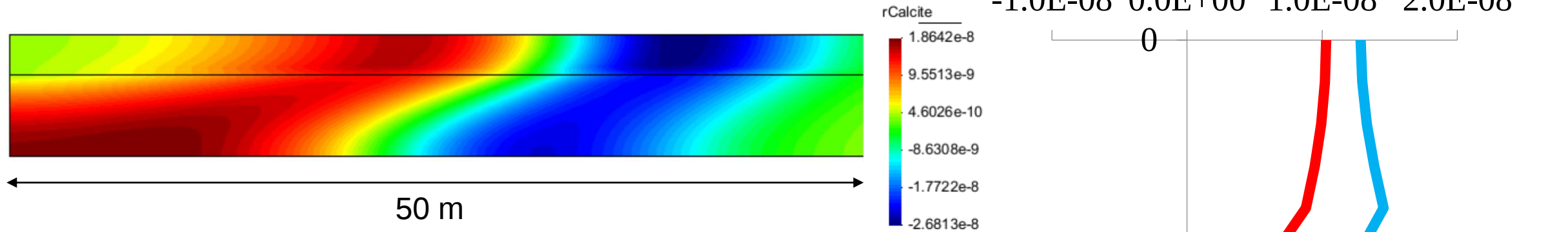
$$T$$



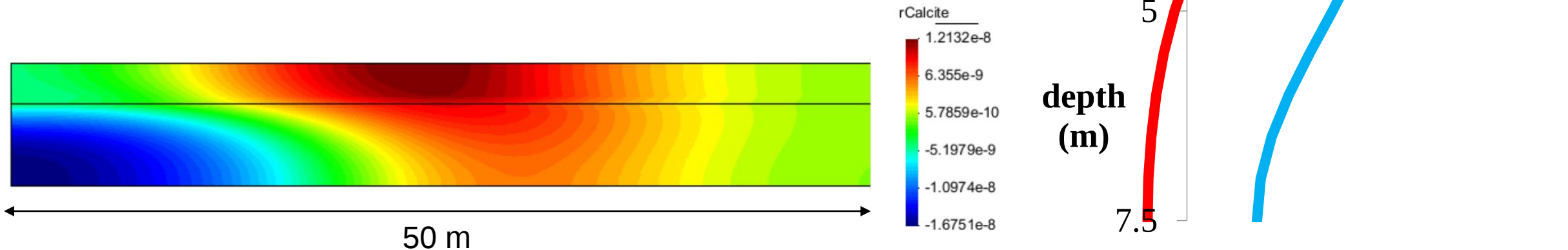
50 m

$$r_{total} = r_{mixing} + r_{heat\ cond} + r_{heat\ retard}$$

INJECTION (216 days)

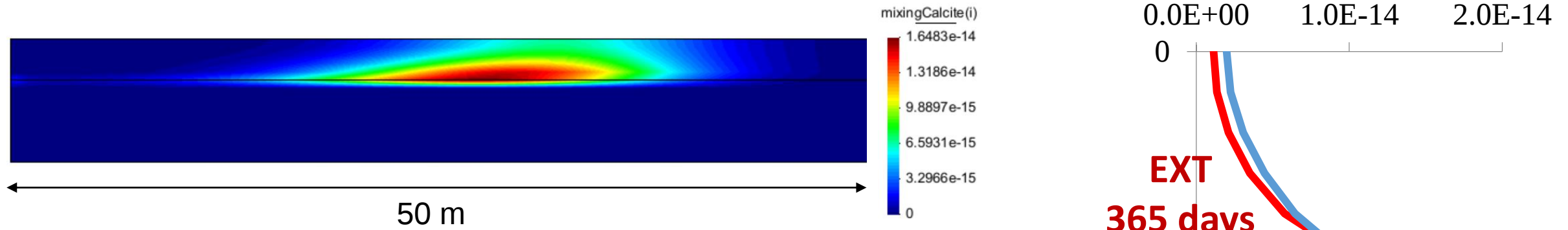


EXTRACTION (365 days)

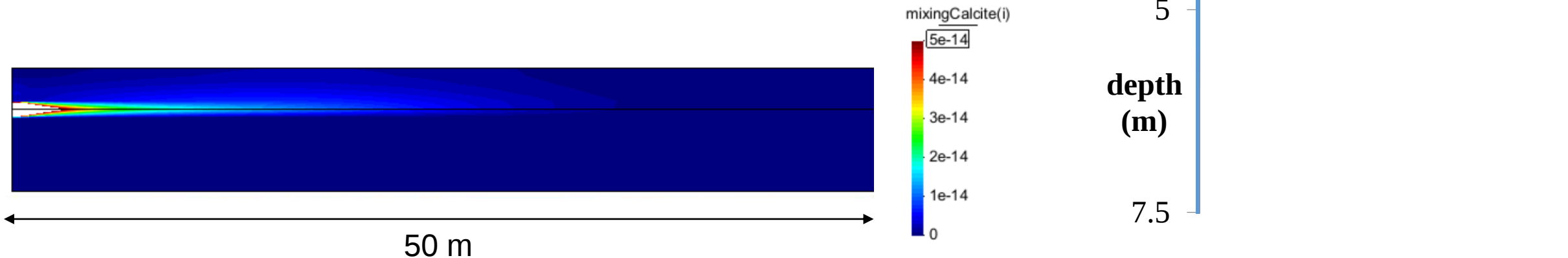


$$r_{total} = \textcolor{red}{r}_{mixing} + r_{heat\ cond} + r_{heat\ retard}$$

INJECTION (216 days)

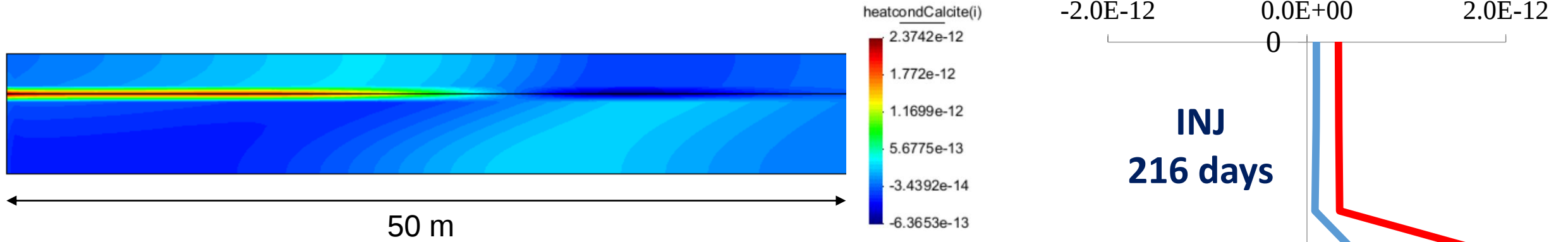


EXTRACTION (365 days)

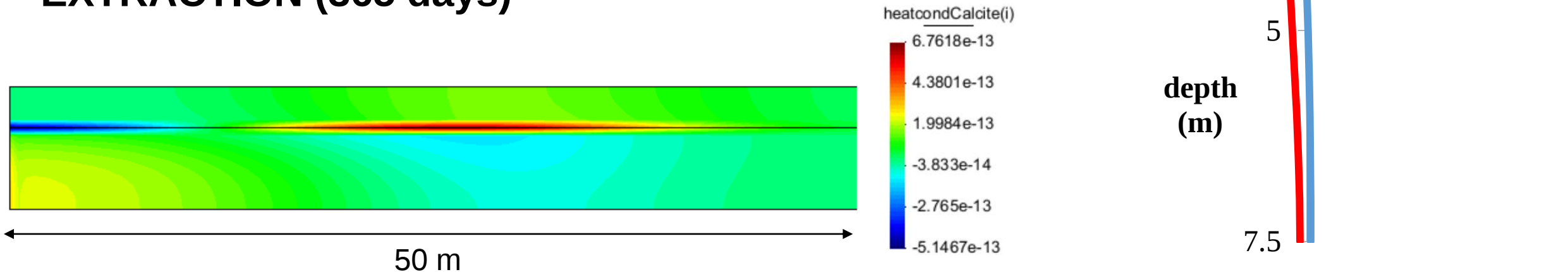


$$r_{total} = r_{mixing} + \textcolor{red}{r_{heat\ cond}} + r_{heat\ retard}$$

INJECTION (216 days)

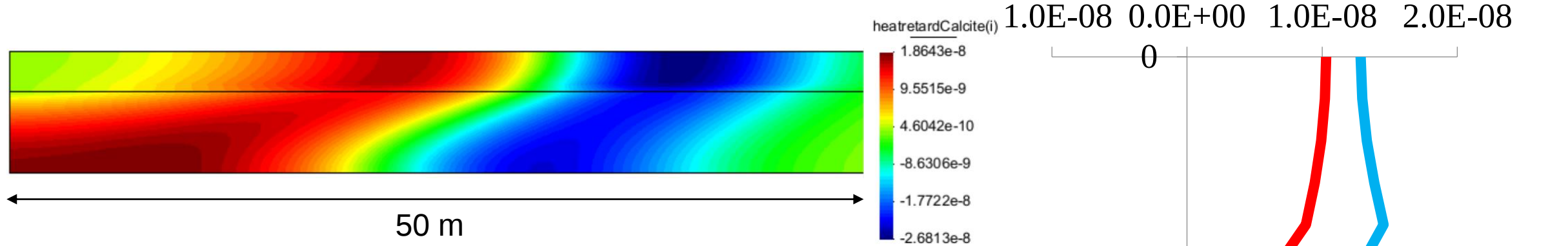


EXTRACTION (365 days)

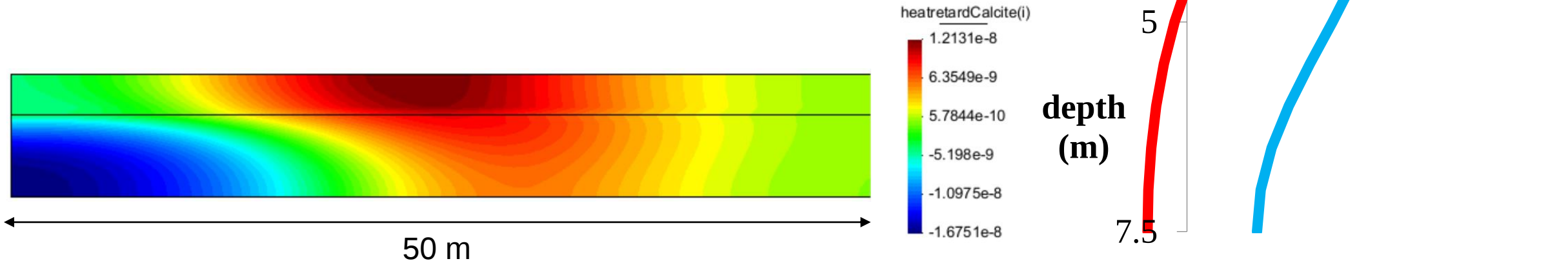


$$r_{total} = r_{mixing} + r_{heat\ cond} + \textcolor{red}{r_{heat\ retard}}$$

INJECTION (216 days)



EXTRACTION (365 days)



CONCLUSIONS

- If there are only aqueous and mineral reactions in equilibrium, we can deduce a (semi-)analytical solution for Thermo-Hydro-Chemical models
- In closed systems (only one end member), the dissolution rate requires the calculation of
 - Thermo-hydraulics ($\partial T / \partial t, \nabla T, \nabla^2 T$)
 - Concentration-temperature relations ($\partial c / \partial T, \partial c^2 / \partial T^2$)
- Three terms in the dissolution rate: Mixing, Heat retardation, Heat conduction
- In general precipitation/dissolution is low, although sometimes it can go to infinity

THANK YOU
