

SUPPLEMENTARY MATERIAL
TAXONOMY OF CLIFF FAILURE CRITERIA
PHASE FIELD MODELLING AND PARALLELS WITH OTHER MODELS

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STANDARD ICE SHELF MODELS

- Ice assumed to be Maxwell viscoelastic material

$$\sigma = \sigma_e = \sigma_v$$

$$\varepsilon = \varepsilon_e + \varepsilon_v$$

- Viscosity is strain rate dependent - Glen-Nye flow law/Norton material

$$\eta = \eta(\dot{\varepsilon}_v) = \frac{1}{2} A (T')^{-1/n} |\dot{\varepsilon}_v|^{1/n-1}$$

- Long time scale \rightsquigarrow modelled as purely viscous flow - Vectorial p -Stokes system

$$-\nabla \cdot (-p\mathbf{1} + 2\eta(\nabla_s \mathbf{v})\nabla_s \mathbf{v}) = f$$

$$\nabla \cdot \mathbf{v} = 0$$

- Vertical direction usually “ignored” \rightsquigarrow Shallow shelf approximation

$$\frac{\partial v_x}{\partial z} \approx 0, \quad \frac{\partial v_y}{\partial z} \approx 0$$



MAXWELL VE EQUATIONS

- Maxwell viscoelastic material:

$$\sigma = \sigma_e = \sigma_v$$

$$\varepsilon = \varepsilon_e + \varepsilon_v$$

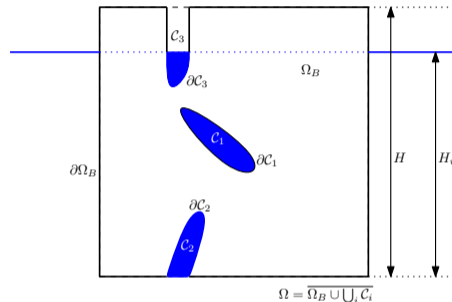
- Rheology:

$$\sigma_e = \lambda \operatorname{tr}(\varepsilon_e) \mathbb{1} + 2\mu \varepsilon_e$$

$$\sigma_v = -p \mathbb{1} + 2\eta(\dot{\varepsilon}_v) \dot{\varepsilon}_v$$

- Glen-Nye flow law:

$$\eta(\dot{\varepsilon}_v) = \frac{1}{2} A(T')^{-1/n} |\dot{\varepsilon}_v|^{1/n-1}$$



MAXWELL VE EQUATIONS

- Maxwell viscoelastic material:

$$\sigma = \sigma_e = \sigma_v$$

$$\varepsilon = \varepsilon_e + \varepsilon_v$$

- Free energy function:

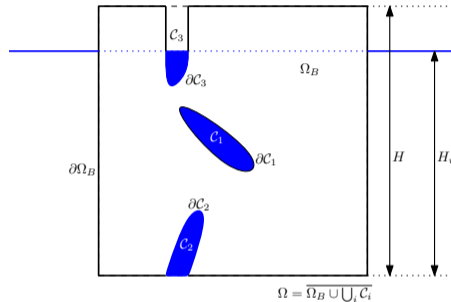
$$\psi_e(\varepsilon_e) = \frac{\lambda}{2} \text{tr}(\varepsilon_e)^2 + \mu \text{tr}(\varepsilon_e^2)$$

- Dissipation function:

$$\phi_v(\dot{\varepsilon}_v) = 2\eta(\text{dev}(\dot{\varepsilon}_v)) \text{dev}(\dot{\varepsilon}_v) : \text{dev}(\dot{\varepsilon}_v)$$

- Small strain, small displacement:

$$\varepsilon = \nabla_s \mathbf{u} = \nabla_s \mathbf{v} + \nabla_s \mathbf{w}$$



MAXWELL VE EQUATIONS

From energy balance:

$$0 = \int_{\Omega_B} [\delta_u \psi_e + \delta_{\dot{u}} \phi - \mathbf{f}] \cdot \dot{\mathbf{u}} + [\delta_w \psi_e + \delta_{\dot{w}} \phi] \cdot \dot{\mathbf{w}} \, dV$$
$$+ \int_{\partial_N \Omega_B} [(\partial_{\nabla_s u} \psi_e + \partial_{\nabla_s \dot{u}} \phi) \cdot \mathbf{n} - \mathbf{t}] \cdot \dot{\mathbf{u}} \, dS + \int_{\partial_N \Omega_B} [(\partial_{\nabla_s w} \psi_e + \partial_{\nabla_s \dot{w}} \phi) \cdot \mathbf{n}] \cdot \dot{\mathbf{w}} \, dS$$

To strong form:

$$-\nabla \cdot (-p \mathbf{1} + 2\mu \operatorname{dev}(\nabla_s(\mathbf{u} - \mathbf{w}))) = \mathbf{f} \quad \text{in } \Omega_B$$

$$2\eta(\operatorname{dev}(\nabla_s \dot{\mathbf{w}})) \operatorname{dev}(\dot{\mathbf{w}}) - 2\mu \operatorname{dev}(\nabla_s(\mathbf{u} - \mathbf{w})) = 0 \quad \text{in } \Omega_B$$

$$\nabla \cdot (\mathbf{u} - \mathbf{w}) + \left(\lambda + \frac{2\mu}{3}\right)^{-1} p = 0 \quad \text{in } \Omega_B$$

$$\nabla \cdot \dot{\mathbf{w}} = 0 \quad \text{in } \Omega_B$$

$$(\lambda \nabla \cdot (\mathbf{u} - \mathbf{w}) \mathbf{1} + 2\mu \nabla_s(\mathbf{u} - \mathbf{w})) \cdot \mathbf{n} = \mathbf{t} \quad \text{on } \partial_E \Omega_B \cup \partial_N \Omega_B.$$



VARIATIONAL FORMULATION OF FRACTURE

Energy balance:

$$\Pi(u, \mathcal{C}) = \Pi_{int}(u, \Omega \setminus \mathcal{C}) - \int_{\Omega \setminus \mathcal{C}} \mathbf{f} \cdot \dot{\mathbf{u}} \, dV - \int_{\partial_N \Omega} \mathbf{t} \cdot \dot{\mathbf{u}} \, dS + G_c \int_{\mathcal{C}} k(\mathbf{x}) \, d\mathcal{H}^{N-1}.$$

Minimisation problem:

$$\begin{aligned} & \inf \Pi(u, \mathcal{C}) \\ & + \textit{crack irreversibility condition} \end{aligned}$$

ISSUE: Numerical implementation is challenging and requires carefully tailored techniques!



VARIATIONAL FORMULATION OF FRACTURE

Energy balance:

$$\Pi(u, \mathcal{C}) = \Pi_{int}(u, \Omega \setminus \mathcal{C}) - \int_{\Omega \setminus \mathcal{C}} f \cdot \dot{u} \, dV - \int_{\partial_N \Omega} t \cdot \dot{u} \, dS + G_c \int_{\mathcal{C}} k(x) \, d\mathcal{H}^{N-1}.$$

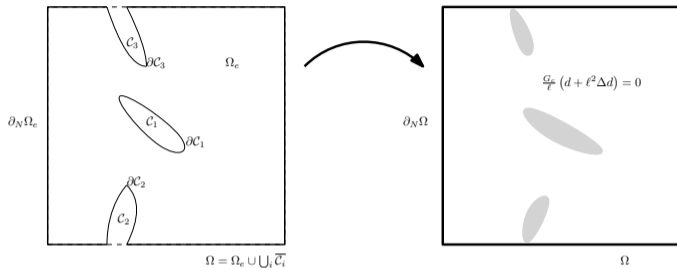
Minimisation problem:

$$\begin{aligned} & \inf \Pi(u, \mathcal{C}) \\ & + \textit{crack irreversibility condition} \end{aligned}$$

IDEA: Regularise the “nasty” stuff by an elliptic functional [Ambrosio, Tortorelli 1990-2].



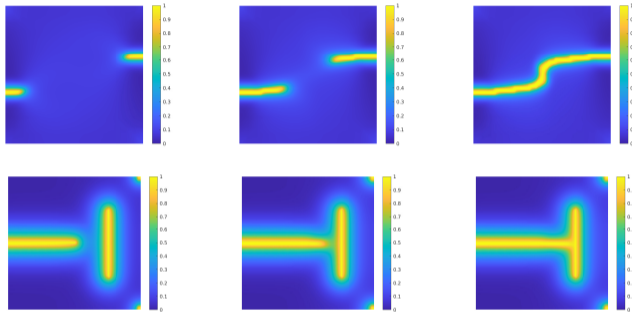
WHY PHASE FIELD?



- Popularised by Fix, Langer, Bourdin, Francfort, Marigo, Miehe, ...
- More recently for ice by Clayton, Duddu, Martinez-Pañeda, Shen, Waisman, Guo, ...
- Elimination of explicit treatment of boundary conditions and evolving geometry
- Replaces them with additional differential equations
- Reproduces curvilinear cracks, kinks, branching, arrest, and crack nucleation.



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PHASE FIELD REGULARISATION

$$d - \ell^2 \Delta d = 0 \text{ in } \Omega, \quad \nabla d \cdot n = 0 \text{ on } \partial\Omega, \quad d = 1 \text{ on } \Gamma$$

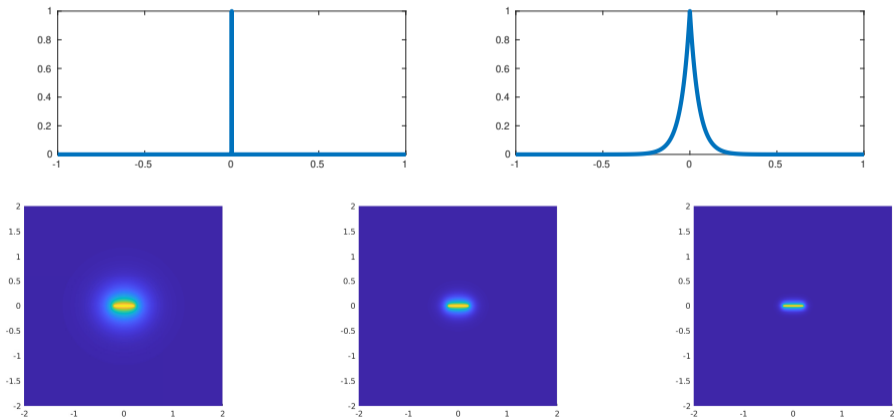


FIGURE: Regularisation of a crack $\Gamma = [-0.2, 0.2] \times 0$ for parameters $\ell = 0.25, 0.10, 0.05$



VARIATIONAL FORMULATION OF FRACTURE

Energy balance:

$$\Pi(u, \mathcal{C}) = \Pi_{int}(u, \Omega \setminus \mathcal{C}) - \int_{\Omega \setminus \mathcal{C}} \mathbf{f} \cdot \dot{\mathbf{u}} \, dV - \int_{\partial_N \Omega} \mathbf{t} \cdot \dot{\mathbf{u}} \, dS + G_c \int_{\mathcal{C}} k(\mathbf{x}) \, d\mathcal{H}^{N-1}$$

Minimisation problem:

$$\inf \Pi(u, \mathcal{C}) \\ + \text{crack irreversibility condition}$$

Regularised energy balance:

$$\Pi_\ell(u, d) = \Pi_{int}(u, d, \Omega) - \int_{\Omega} g(d) \mathbf{f} \cdot \dot{\mathbf{u}} \, dV - \int_{\partial_N \Omega} g(d) \mathbf{t} \cdot \dot{\mathbf{u}} \, dS \\ + G_c \int_{\Omega} \frac{1}{2\ell} (d^2 + \ell^2 |\nabla d|^2) \, dV$$



DEGRADATION OF FUNCTIONS

We want a degradation function $g(d)$ so that

$$g(0) = 1, \quad g(1) = 0, \quad g'(1) = 0.$$

One possibility:

$$g(d) = (1 - d)^2.$$

Q: How do we degrade free energy and degradation functions?

$$(\text{??}) \tilde{\psi}_e(\varepsilon_e, d) = g(d) \left(\frac{\lambda}{2} \text{tr}(\varepsilon_e)^2 + \mu \varepsilon_e : \varepsilon_e \right) (\text{??})$$

ISSUE: Behaves the same under tension and compression.



DEGRADATION OF FUNCTIONS

We want a degradation function $g(d)$ so that

$$g(0) = 1, \quad g(1) = 0, \quad g'(1) = 0.$$

One possibility:

$$g(d) = (1 - d)^2.$$

Q: How do we degrade free energy and degradation functions?

Free energy function:

$$\begin{aligned} \tilde{\psi}_e(\varepsilon_e, d) &= g(d) (\psi_e^+(\varepsilon_e) - \psi_c) + (\psi_e^-(\varepsilon_e) + \psi_c) \\ \psi_e^\pm &= (\lambda/2 + \mu/3) \langle \text{tr}(\varepsilon_e) \rangle_\pm^2 + \mu \text{tr}(\text{dev}(\varepsilon_{e,\pm}))^2 \end{aligned}$$

Dissipation function:

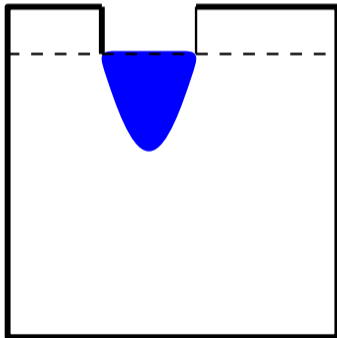
$$\tilde{\phi}(\dot{\varepsilon}_v, d) = g(d) 2\eta(\text{dev}(\dot{\varepsilon}_v)) \text{dev}(\dot{\varepsilon}_v) : \text{dev}(\dot{\varepsilon}_v).$$



HYDROFRACTURE

Inclusion of pressurised cracks:

$$\int_{\cup_i \partial \mathcal{C}_i} p_w n \cdot \dot{u} \, dS = \int_{\Omega_B} \nabla \cdot (p_w \dot{u}) \, dV - \int_{\partial_E \Omega_B} p_w n \cdot \dot{u} \, dS.$$



HYDROFRACTURE

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$$\int_{\cup_i \partial \mathcal{C}_i} p_w n \cdot \dot{u} \, dS = \int_{\Omega_B} \nabla \cdot (p_w \dot{u}) \, dV - \int_{\partial_E \Omega_B} p_w n \cdot \dot{u} \, dS.$$

Extension to Ω :

$$\int_{\Omega_B} \nabla \cdot (p_w \dot{u}) \, dV \approx \int_{\Omega} g(d) \nabla \cdot (p_w \dot{u}) \, dV$$

$$\int_{\partial_E \Omega_B} p_w n \cdot \dot{u} \, dS \approx \int_{\partial_N \Omega} g(d) p_w n \cdot \dot{u} \, dS.$$



HYDROFRACTURE

Inclusion of pressurised cracks:

$$\int_{\cup_i \partial \mathcal{C}_i} p_w n \cdot \dot{u} \, dS = \int_{\Omega_B} \nabla \cdot (p_w \dot{u}) \, dV - \int_{\partial_E \Omega_B} p_w n \cdot \dot{u} \, dS.$$

Thanks to Divergence Theorem:

$$\int_{\Omega_B} \nabla \cdot (p_w \dot{u}) \, dV \approx - \int_{\Omega} p_w \nabla g(d) \cdot \dot{u} \, dV + \int_{\partial_N \Omega} g(d) p_w n \cdot \dot{u} \, dS$$

$$\int_{\partial_E \Omega_B} p_w n \cdot \dot{u} \, dS \approx \int_{\partial_N \Omega} g(d) p_w n \cdot \dot{u} \, dS.$$



HYDROFRACTURE

Inclusion of pressurised cracks:

$$\int_{\cup_i \partial \mathcal{C}_i} p_w \mathbf{n} \cdot \dot{\mathbf{u}} \, dS = \int_{\Omega_B} \nabla \cdot (p_w \dot{\mathbf{u}}) \, dV - \int_{\partial_E \Omega_B} p_w \mathbf{n} \cdot \dot{\mathbf{u}} \, dS.$$

Combined:

$$\int_{\cup_i \partial \mathcal{C}_i} p_w \mathbf{n} \cdot \dot{\mathbf{u}} \, dS \approx \int_{\Omega} 2p_w(1-d) \nabla d \cdot \dot{\mathbf{u}} \, dV.$$

Intuition:

- Term $(1-d)$ acts like an indicator function.
- Term ∇d acts like the unit normal vector.



MAXWELL VISCOELASTIC FRACTURE MODEL

Strong form:

$$-\nabla \cdot (g(d)\sigma_e^+ + \sigma_e^-) = [g(d)f - p_w \nabla g(d)] \quad \text{in } \Omega$$

$$g(d)2\eta(\operatorname{dev}(\nabla_s \dot{w})) \operatorname{dev}(\dot{w}) = [2g(d) \operatorname{dev}(\sigma_e^+) - 2 \operatorname{dev}(\sigma_e^-)] \quad \text{in } \Omega$$

$$\nabla \cdot (u - w) + \mu \left(\lambda + \frac{2\mu}{3} \right)^{-1} p = 0 \quad \text{in } \Omega$$

$$\nabla \cdot \dot{w} = 0 \quad \text{in } \Omega$$

$$(g(d)\sigma_e^+ + \sigma_e^-) \cdot n = g(d)t \quad \text{on } \partial_N \Omega$$

$$d - \ell^2 \Delta d = 2C\ell(1 - d)\mathcal{D} \quad \text{in } \Omega$$

$$\nabla d \cdot n = 0 \quad \text{on } \partial \Omega$$

Stresses: $\sigma_e^\pm := (\langle -p \rangle_\pm \mathbf{1} + 2 \operatorname{dev}(\nabla_s (u - w)_\pm))$

Fracture forcing: $\mathcal{D} = \max_{s \in [0, t]} \langle \psi_e^+(\varepsilon_e(x, s)) - \psi_c \rangle_+$



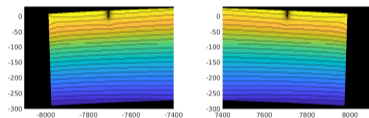
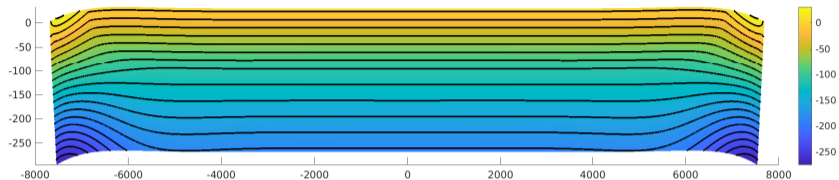
NUMERICAL SETUP

- Mixed finite element solver (2D/3D) - KRAKEN
- Updated Lagrangian formulation
- Alternating minimisation scheme married to inexact Newton to bypass nonconvexity

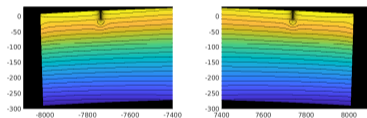


RESULTS

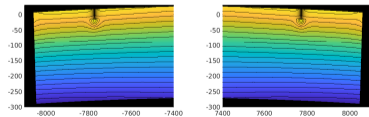
$H = 300m$



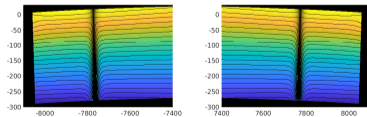
(A) $t = 0$ days



(B) $t = 98$ days



(C) $t = 258$ days



(D) $t = 260$ days



RESULTS

