

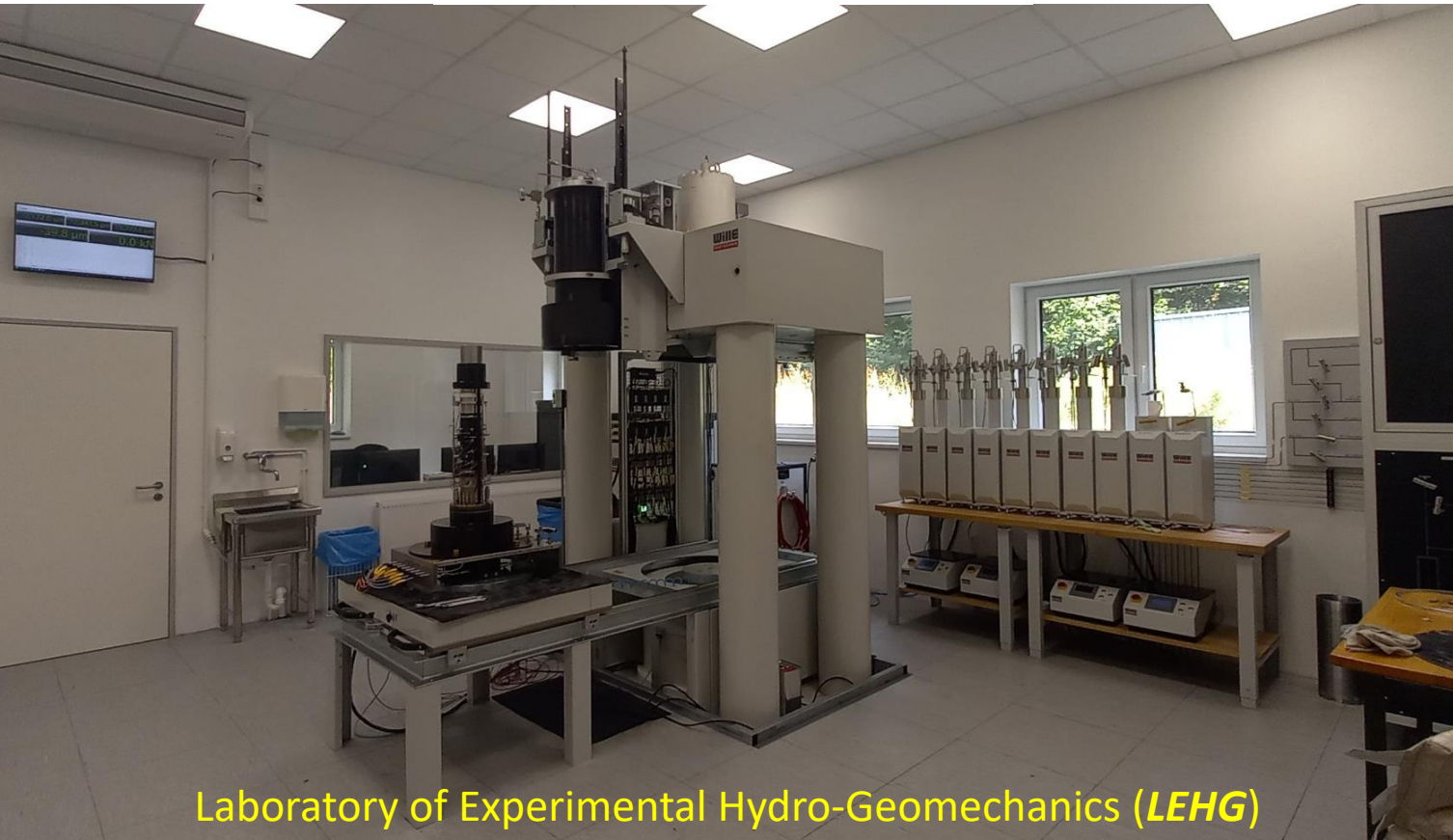


Simulation of different georeservoir conditions on a highly-permeable sandstone

(supplementary
material)

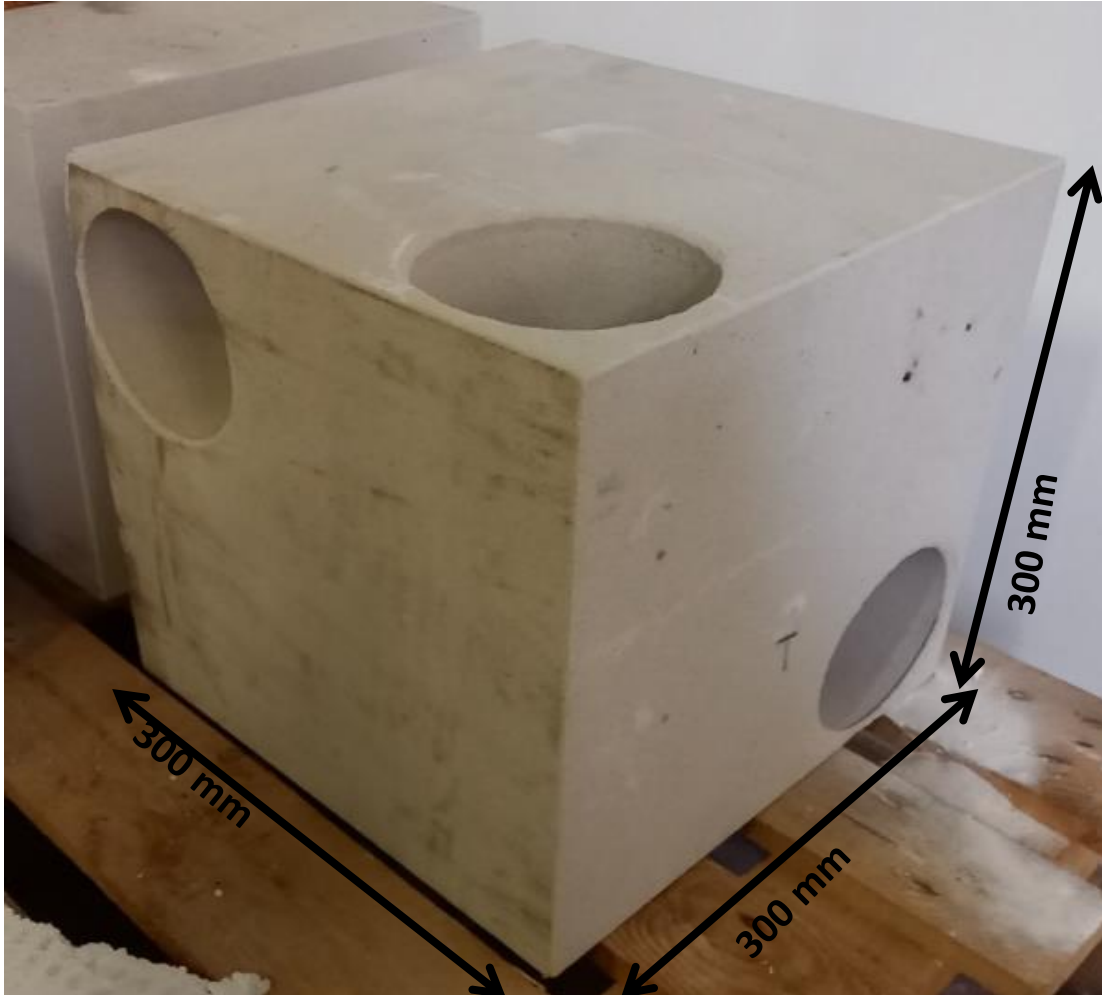
Marco Fazio & Martin Sauter

*EGU, Coupled thermo-hydro-mechanical-chemical (THMC) processes in
geological media, 24.04.2023, Vienna*



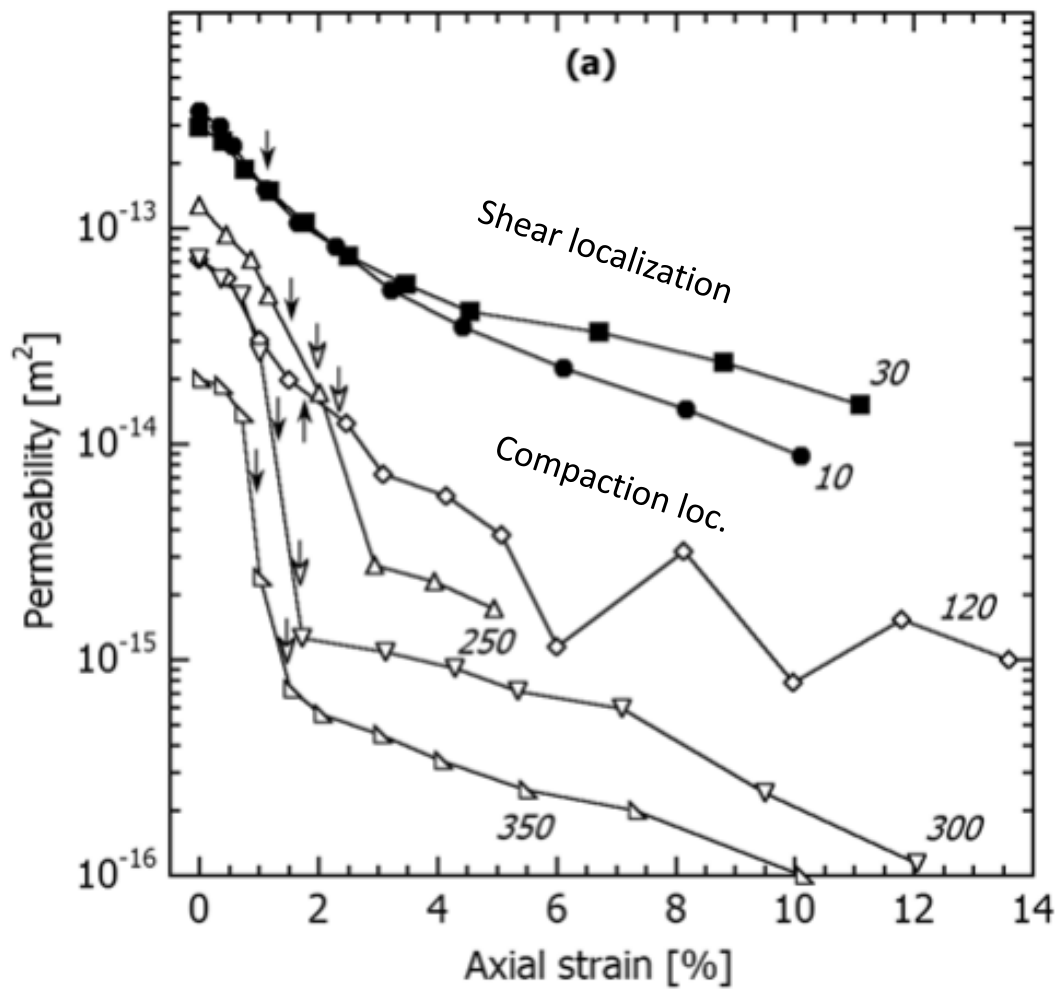
Laboratory of Experimental Hydro-Geomechanics (LEHG)

Homogeneity at the block scale



Sample #	1T	2N	3E
m_d (g)	3830.05	3842.94	3845.14
l (mm)	250.28	250.6	250.36
\emptyset (mm)	99.12	99.17	99.31
ρ_d (g/cm ³)	1.98	1.99	1.98
n (%)	24.34	24.36	24.38

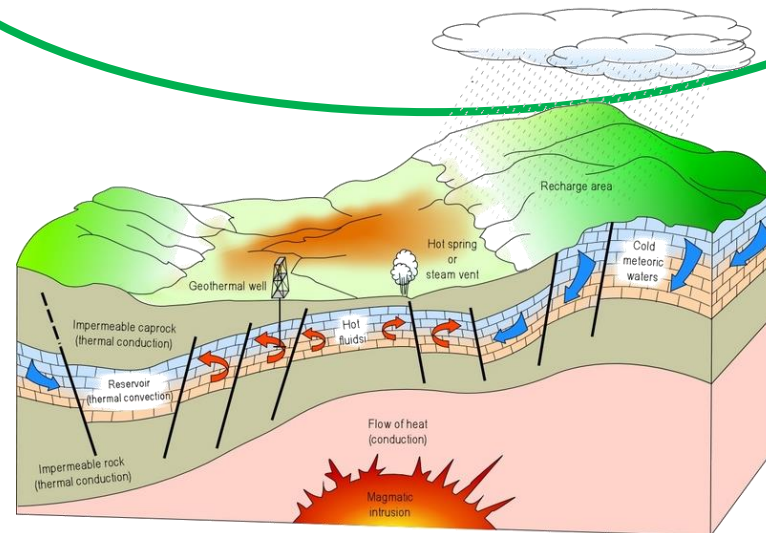
Effect of shear deformation



High shear deformation levels decrease the permeability

BS chosen for

- Deep warm aquifer for potential low-cost geothermal energy in Netherlands
- Case study rock for anhydrite cementification in georeservoirs



Darcy's law

$$k = \frac{Q * \mu * L}{A * (p_u - p_d)}$$

k = permeability (m²)

Q = Volumetric flow rate (m³/s) ($\Delta V/\Delta t$)

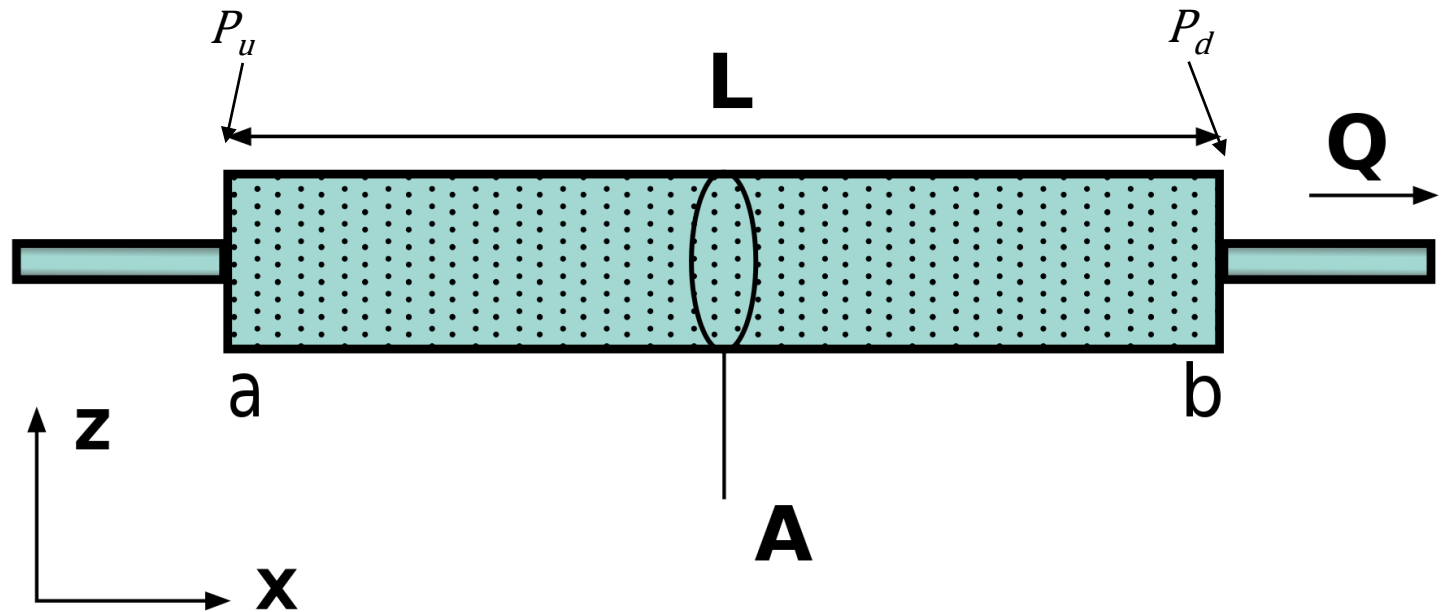
μ = fluid viscosity (Pa*s)

L = length of the sample (m)

A = surface area of the sample (m²)

p_u = upstream pressure (Pa)

p_d = downstream pressure (Pa)



- A and L changes are negligible
- μ calculated through Korson et al. (1969) equation and Schmelzer et al. (2005) tabulated values

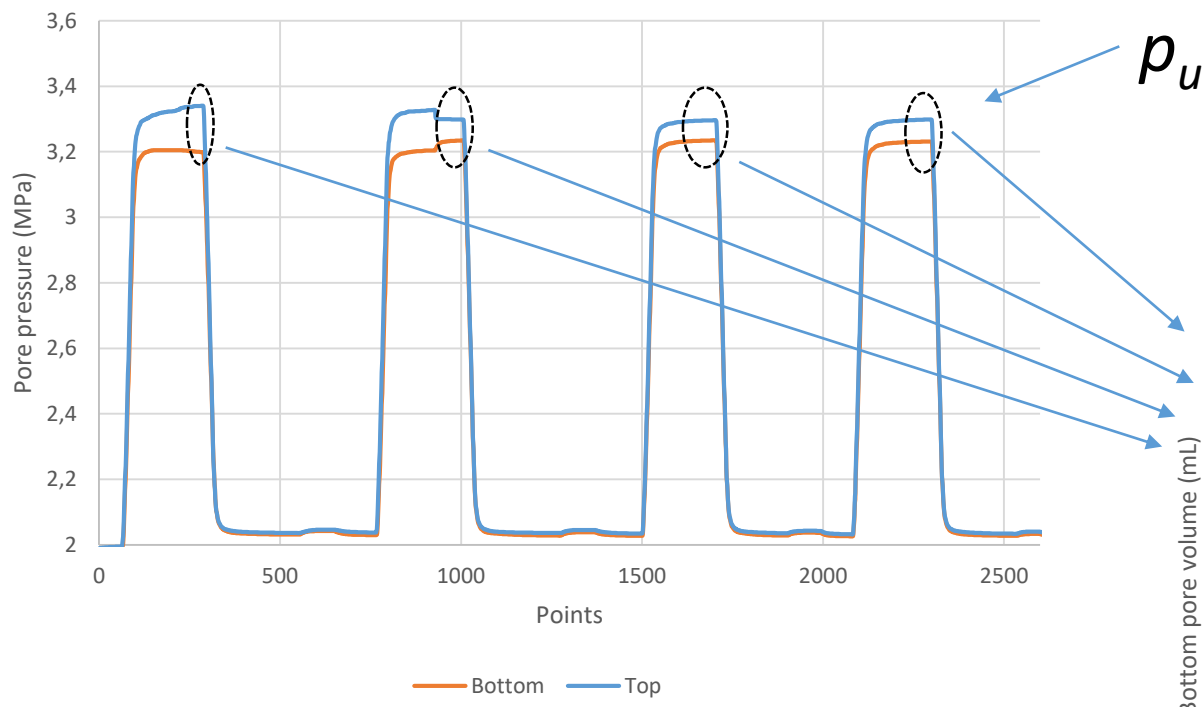
$$\log \frac{\mu_T}{\mu_{20}} = \frac{a(20 - T) - b(T - 20)^2}{T + c}$$

T = temperature (°C)

μ_{20} = water viscosity at 20°C = 1.002x10⁻³ Pa*s

a = 1.1709; b = 0.001827; c = 89.93

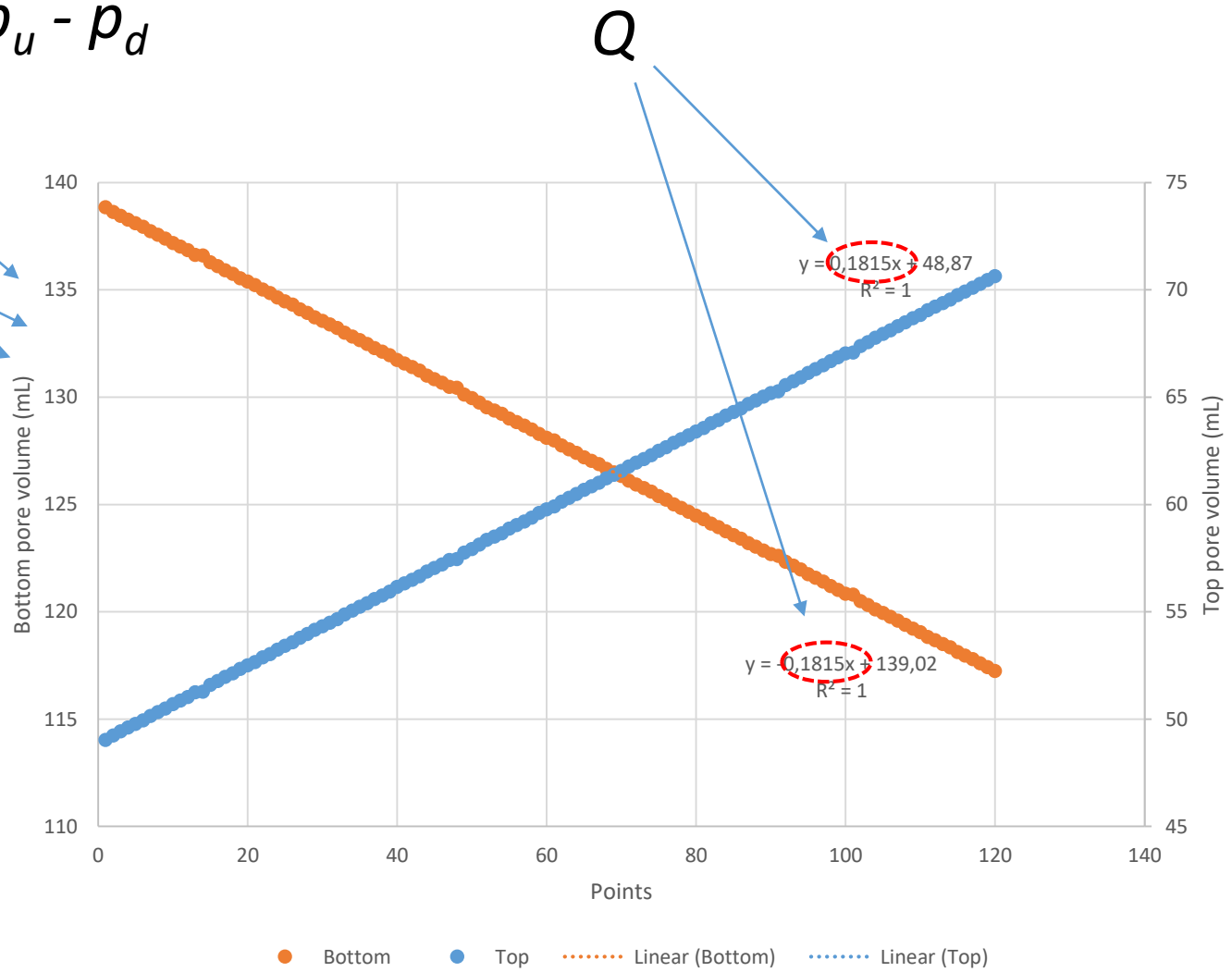
Flow rate & pressure drop



Highly permeable rock

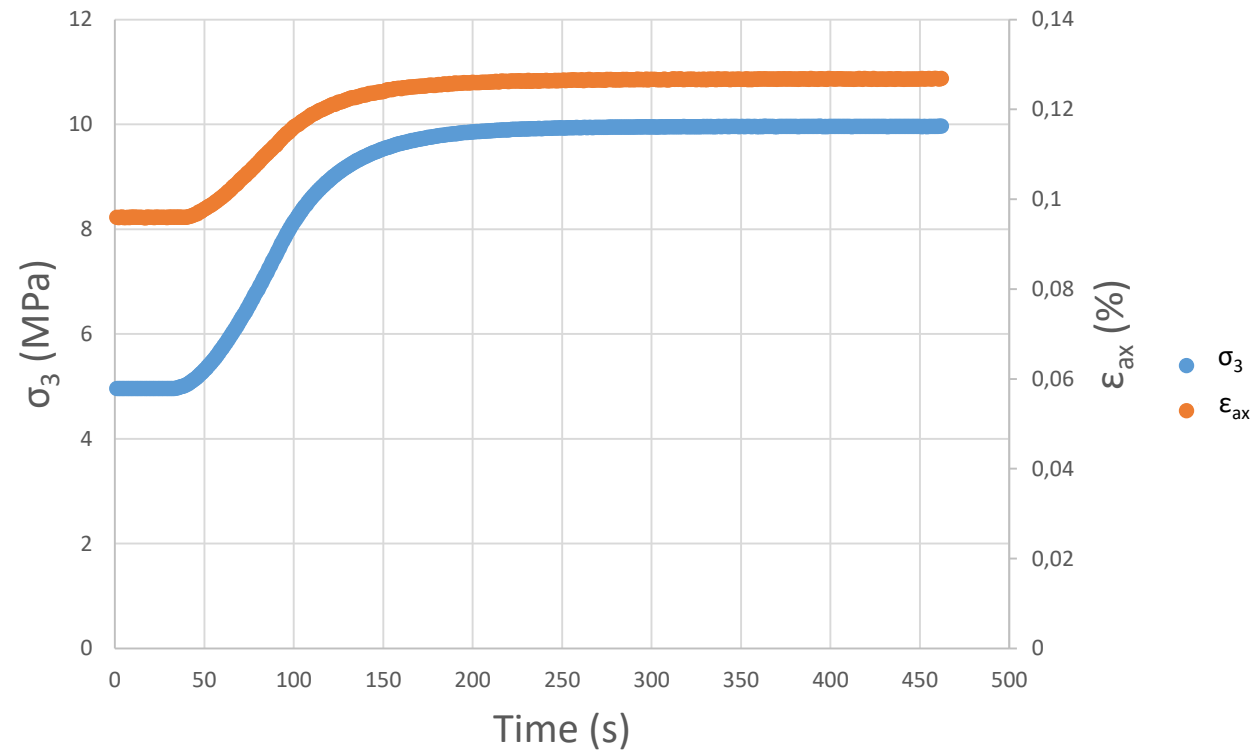


Steady-state-flow method: apply constant **pore pressure gradient** and wait for constant and equal (but opposite sign) **flow rate** at each end of the samples

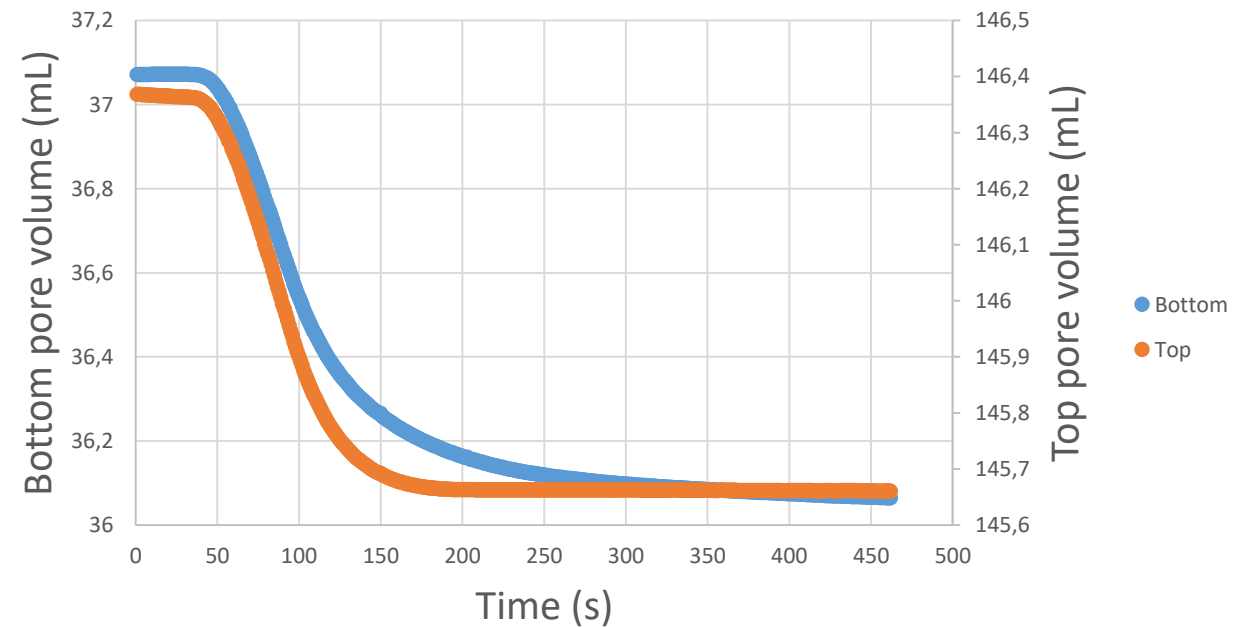


● Bottom ● Top ● Linear (Bottom) ● Linear (Top)

Porosity measurement



For each σ_3 or σ_{diff} increase, both top and bottom pore volume were monitored before and after the step, at constant pore pressure.

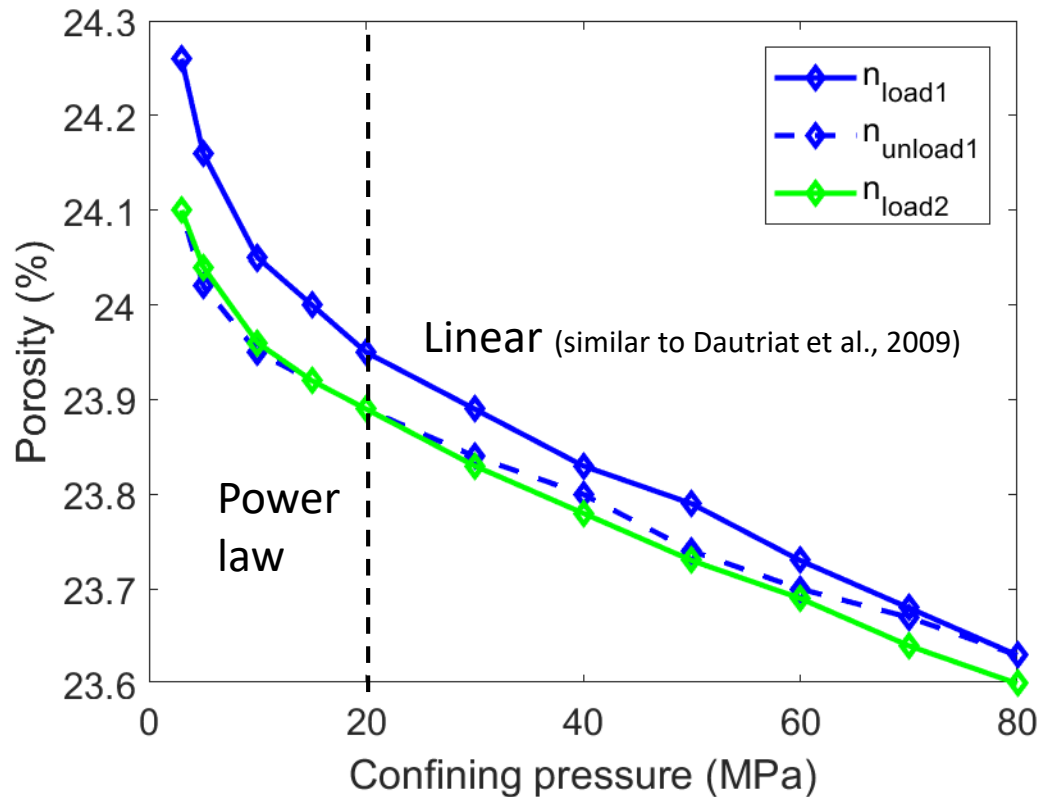


$$V_{p,i} = V_{p,i-1} - \Delta V$$

$$= V_{p,i-1} - [(V_{top,i} - V_{top,i-1}) + (V_{bottom,i} - V_{bottom,i-1})]$$

$$n_i = \frac{V_{p,i}}{V_{dry} + V_{p,i}}$$

Effect of σ_3 on Porosity

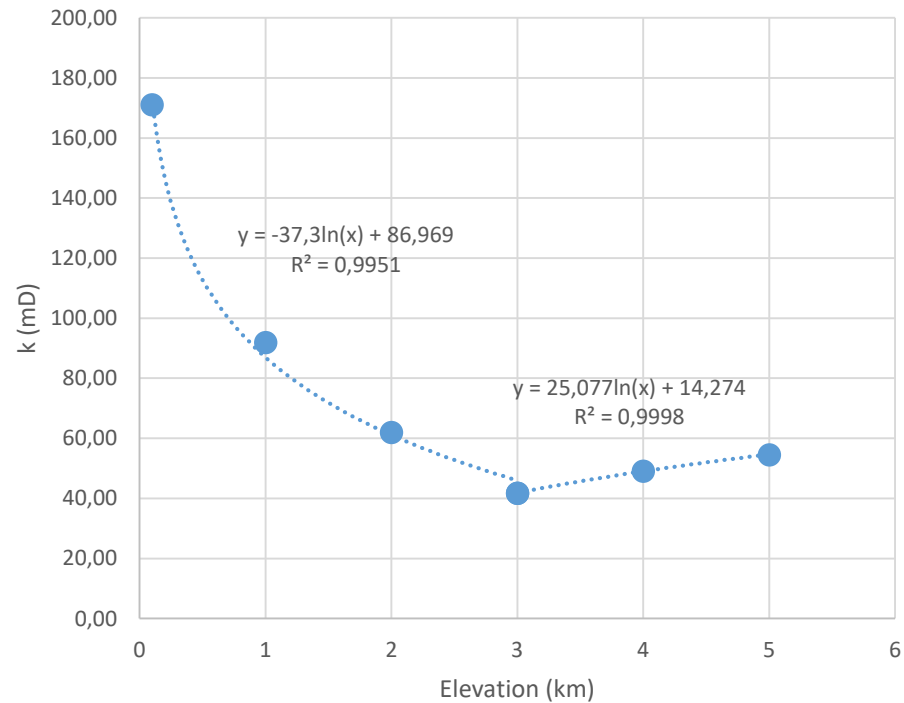


Porosity evolution through pore volume changes (only with $\uparrow \downarrow \sigma_3$)

- n decreases non uniformly with $\uparrow \sigma_3$ and does not fully recover after unloading cycle \rightarrow loss of pore space
- $\rho = 1.98 \text{ kg/m}^3 \rightarrow 80 \text{ MPa}$ corresponds to depth $> 4\text{km}$
- 2.9% loss of porosity, but still highly porous

Depth simulations

⊥ to bedding planes



// to bedding planes

