Influence of the Wind Stress Curl on the Eddy Saturation Behavior of the ACC in a Barotropic Perspective Sima Dogan¹ Caroline Muller¹ Louis-Philippe Nadeau² Antoine Venaille³



I. Introduction

- The strength of zonal transport of the Antarctic Circumpolar Current (ACC) is almost independent of the variations in westerly winds over the Southern Ocean; this phenomenon is called **eddy saturation**.
- The eddy saturation has been studied in both barotropic and baroclinic contexts in the presence of topography, yet many aspects of its dynamics remain elusive. ([1,2,3,4,5,6,7,8,9])
- We focus on barotropic eddy saturation, which occurs in a narrow band of wind stresses where topographic-barotropic instability takes place.
- We investigate whether the amplitude of the wind stress curl relative to that of a constant background wind stress can also modulate barotropic eddy saturation by modifying the global vorticity budget of a doubly periodic quasigeostrophic flow.

Background figure is taken from Vallis, 2017. [10]

II. Barotropic QG Model

- Solved using DEDALUS [11].
- Monoscale topography, L = 775 km, H = 4 km, $h_{rms} = 200$ m [7]

$$\eta = \sqrt{2}\eta_{\rm rms}\cos(14x/L).$$

- Doubly periodic 2D domain, $2\pi L \times 2\pi L$, and 512×512 grid.
- The vorticity equation with the added wind curl term is given as:

$$\partial_t \nabla^2 \psi + J \left(\psi - Uy, \nabla^2 \psi + \eta + \beta y \right) = -D \nabla^2 \psi' - \partial \tau_y$$

The wind curl enters the vorticity equation through the stream function.

$$\psi = \psi' + V_{sv}x$$

where V_{sv} is defined as:

$$V_{sverdrup} = -\frac{-\partial \tau_y}{\beta}$$

We solve for the potential vorticity and the mean zonal velocity equations:

$$\partial_t \nabla^2 \psi' + J \left(\psi' - Uy, \nabla^2 \psi' + \eta + \beta y \right) + V_{SV} \left(\nabla^2 \psi'_y + \beta + \eta_y \right) = \underbrace{-D \nabla^2 \psi}_{\text{ekman drag + hyperviscosity}} - \underbrace{-D \nabla^2 \psi}_{\text{ekman drag + hyperv$$

$$\partial_t U = \underbrace{F}_{\text{wind forcing}} - \underbrace{\mu U}_{\text{bottom drag}} - \underbrace{\langle \psi \partial_x \eta \rangle}_{\text{form stress}}$$

• The eddy kinetic energy is decomposed into the total eddy kinetic energy (EKE) and standing eddy kinetic energy (sEKE).



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III. Eddy Saturation with Uniform Wind

(1)

(2)

(3)

 $\partial \tau_y$

wind cur

(5)

(6)

and F are varying.



Figure 1. (Left) The time-mean large-scale domain averaged zonal nondimensional flow U as a function of nondimensional mean forcing. The highlighted lines show the analytical steady-state solutions of Eq (4) and Eq (5). Three eddy streamfunction snapshots are given for different values of F. [7] (Right corner) The nondimensional EKE and sEKE as a function of the nondimensional wind forcing.

- Lower branch region before the eddy saturation regime is dominated by the form stress and wind forcing terms and shows laminar characteristics.
- In the eddy saturation region, EKE increases, while the mean zonal transport and sEKE stay nearly constant.
- Higher branch region is dominated by **bottom drag and wind forcing** and also exhibits laminar characteristics.

IV. Sensitivity of the Volume Transport and Eddies to the Wind Curl with **Zero Mean Wind Stress**



Figure 2. The mean zonal transport where F = 0, for varying wind stress curl values. On the left, two decomposed eddy streamfunction snapshots are given for negative and positive values of the largest wind stress curl magnitudes.

Take away: Asymmetrical nonzero mean zonal flow solutions exist for zero mean forcing.



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We validate our method against Constantinou (2018) [7] for a uniform wind profile where $\partial_y \tau = 0$

Nonzero Wind Stress $- \times - \partial \tau_v = 1 \times 10^- 6$ $- \times - \partial \tau_v = 2 \times 10^{-7}$ $- \times - \partial \tau_v = 1.5 \times 10^{-1}$ $- \times - \partial \tau_v = 1 \times 10^{-7}$ $- \bullet - \partial \tau_v = 0$ $\partial \tau_v = -1x10^-9$ $-\times - \partial \tau_v = -1x10^{-}7$ $- \times - \partial \tau_v = -1.5 \times 10^{-7}$ $- \times - \partial \tau_v = -2x10^-7$ $- \times - \partial \tau_y = -1x10^{-}6$

V. Sensitivity of the Volume Transport and Eddies to the Wind Curl with We solve equations (4) and (5) with a constant wind curl where F and $\partial_y \tau = constant$ varies.



decomposed eddy streamfunction snapshots are given for various wind curl magnitudes, for nondimensional F = 0.14.

Take away:

- curl values.
- An asymmetry in the system with varying eddy profiles.
- stress curl.



- The source of the asymmetry in the system.
- Further experiments with various topography and wind profiles.
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Figure 3. The mean zonal transport where F varies for varying wind stress curl values. On the left, three

 10^{-2}

 $F/(l_n n_{rms}^2)$

 $\partial au_y = [N/m^3]$

• The lower branch is not observed for positive higher values of wind stress curl. Bifurcation to the upper branch realizes at lower forcing values with increasing wind stress

• We report that the zonal transport and the eddy saturation regime are sensitive to the wind

VI. Future Work

• Analytical solutions for different stable and unstable regimes exist depending on the (1) wind profile and (2) topography with a focus on eddy saturation regime.

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