

# Hydrogeological Characterisation of Sherwood Sandstone using BNMR and Geophysical Logs Sodiq Oguntade<sup>1</sup>, Ulrich Ofterdinger<sup>1</sup>, Jean-Christophe Comte<sup>2</sup>, Ryan Gee<sup>3</sup>, Myles Kynaston<sup>4</sup>, and Robert Raine<sup>5</sup>

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### Introduction

- The Aquifer thermal energy storage ATES system (figure 1) consists of two groundwater wells that operate in a seasonal mode. Water is extracted from one of the wells (cold storage well) during the summer and passes through a heat exchanger to cool a building or facility. The water is then injected into the second well (heat storage well).
- A detailed hydrogeological site characterisation is needed for ATES systems, as they are sensitive to groundwater flow and heterogeneities (Fleuchaus et al., 2018). The porosity of an aquifer is one of the hydrogeological properties that determines its suitability for ATES systems.



Fig. 1: Working principle of an ATES-doublet (Bloemendal and Olsthoorn, 2018)

- The Permo-Triassic Sherwood Sandstone is an essential aquifer in the UK with great potential for geothermal energy, including ATES systems (figure 2).
- The geothermal resource potential of the Sherwood Sandstone in Northern Ireland at a temperature of more than 20°C is about 523 Mtce (million tonnes of coal equivalent) (Downing & Gray, 1986).



Fig. 2: Estimated temperatures and depth to the top of Sherwood Sandstone; indicated in red rectangle is the study area (after Raine et al. 2022)

### Objectives

• This study investigates the porosities of the Sherwood Sandstone Aquifer as encountered in three boreholes completed on the Queen's University Belfast campus using borehole nuclear magnetic resonance (BNMR) and traditional geophysical logs.



Fig. 3: Sectional view of the boreholes for this study

References:

Archie, G. E. (1942). The electrical resistivity log as an aid in determining some reservoir characteristics. Transactions of the AIME, 146(01), 54-62. Bloemendal, M. & Olsthoorn, T. 2018. ATES systems in aquifers with high ambient groundwater flow velocity. Geothermics, 75, 81-92 Downing, R. A., & Gray, D. A. (1986). Review of the geothermal potential of the UK. In R. A. a. G. Downing, D.A (Ed.), (pp. 152-161). Fleuchaus, P., Godschalk, B., Stober, I., & Blum, P. (2018). Worldwide application of aquifer thermal energy storage – A review. Renewable and Sustainable Energy Reviews, 94, 861-876. Larionov, M. (1969). Application of factor analysis to well logging data. Earth Science Journal, 1(1), 113-123. Raine, R, Reay, DM, 2019, A review of geothermal reservoir properties of Triassic, Permian and Carboniferous sandstones in Northern Ireland, Geological Survey of Northern Ireland Internal Report, 19/00/01. 62pp Waxman, M. H., & Smits, L. (1968). Electrical conductivities in oil-bearing shaly sands. Society of Petroleum Engineers Journal, 8(02), 107-122

Methodology

- BNMR logging was completed at the 3 boreholes; the nominal borehole total depth of 100m.
- The most important output of BNMR data processing is the  $T_2$  distribution (a Carr-Purcell-Meiboom-Gill pulse train), which gives the rock's total volume or and the second second porosity (Figure 4).



Fig. 4: The T<sub>2</sub> distribution reflects the volumes of fluid occupying different pore sizes.

- This study also used Archie and Waxman-Smits petrophysical models to calculate porosity from geophysical logging data (resistivity, EC, temperature and natural gamma).
- Archie (1942) assumes that the rock is clay-free and a relationship exists between the formation factor (F) of a completely water-saturated sedimentary rock and its porosity ( $\phi$ ).

Where m and a are the cementation and tortuosity factors, respectively F = --- $d^{-m}$ 

• Archie's method does not account for clay content in rocks, but the Sherwood Sandstone has some clay content. The Waxman-Smits (1968) petrophysical model incorporates it.

$$\sigma_o = \phi^{-m}(\sigma_w + BQ_v)$$
 Where  $\sigma_o, \sigma_w$ , B and  $Q_v$  are the aquifer bulk equivalent counterion mobility and excess charged

• The mass fraction of clay in the rock was calculated from the gamma logs using the linear and Larionov (Larionov, 1969) equations:

$$I_{GR} = \frac{GR_{log} - GR_{min}}{GR_{max} - GR_{min}}$$

Where the I<sub>GR.</sub> GR<sub>log</sub>, GR<sub>max</sub> and GR<sub>min</sub> are the gamma ray index, gamma ray log reading, maximum gamma ray value and minimum gamma ray value, respectively

$$\varphi_w = 0.33 \times \left(2^{\mathrm{I}R} - 1\right)$$



Fig. 6: Mass fraction of clay in one of the boreholes

• The relative fraction of each clay mineral in the rock was obtained from the Geological Survey of Northern Ireland's XRD analysis of clay minerals in the Sherwood Sandstone, which is located within the same geographic location.



alk conductivity, pore water conductivity, equivalent counterion mobility and excess charge per unit pore volume, respectively



## Conclusion and future work

- and gas industry.
- performance of ATES systems in the Sherwood Sandstone of Northern Ireland.



• BNMR confirms the credibility of using the Waxman-Smits model instead of the Archie model to estimate porosity in the Sherwood Sandstone formation. The Archie model overestimates the porosity.

• The results demonstrate the relationship between BNMR and petrophysical-derived porosity and confirm the reliability of using BNMR in hydrogeological investigations similar to its widespread usage in the oil

• This study forms part of the broader research on the impact of subsurface heterogeneities on the

• Further hydrogeologic characteristics such as hydraulic conductivity, transmissivity, and structure delineation will be carried out. Also, thermal injection testing and numerical heat transport modelling.

