

1 **Contrasts in two- and three-dimensional system**
2 **behaviour in the modelling of compositionally**
3 **originating LLSVPs and a mantle featuring dynamically**
4 **obtained plates**

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10 **Running Title:**

11 Modelling LLSVPs and plates in mantle convection models

SUMMARY More than two decades of systematic investigation has made steady progress towards generating plate-like surface behaviour in models of vigorous mantle convection. Accordingly, properties required to obtain dynamic plates from mantle convection have become widely recognized and employed in both 2D and 3D geometries. Improving our understanding of the properties required to obtain durable (or replenishable) deep mantle features with LLSVP-like characteristics has received interest for a period with similar longevity. Investigation ultimately focusses on discovering the properties able to produce the presence of a detached pair of three-dimensional features, distinct from the ambient mantle. Here, we assume the LLSVPs have a chemical origin by incorporating a Compositionally Anomalous and Intrinsically Dense (CAID) mantle component comprising 2-3.5% of the total mantle volume. The feedback between plate formation and the presence of a CAID mantle component is investigated in both 2D and 3D spherical geometries. We explore the impact of both an intrinsic contrast in density and viscosity for the CAID component, with the objective of finding system parameter values that encourage the formation of a pair of LLSVP-like assemblages and a surface that exhibits the principle features of terrestrial plate tectonics; including recognizable and narrowly focussed divergent, convergent and (in 3D) transform plate boundaries that separate 8-16 distinct plate interiors. We present the results of nine two-dimensional and eleven three-dimensional calculations and show that for some of the cases examined, a pair of CAID material provinces can be freely obtained in two-dimensional cases while maintaining a surface characterized by plate-like behaviour. However, specifying the same system parameters in the three-dimensional model does not readily yield a pair of enduring provinces for any values of the parameters investigated. Moreover, the inclusion of the CAID component in the mantle can affect the global geotherm so that in comparison to the surface behaviour obtained for the initial condition isochemical model, the surface behaviour of the cases incorporating the dense component are less exemplary of plate tectonics. In general, CAID material components that are 3.75%-5% denser than the surrounding mantle (at surface temperatures), and up to a factor of 100 times greater in intrinsic viscosity, form layers populated by voids, or nodes connected by tendril-like ridges that reach across the core-mantle-boundary, rather than distinct piles resembling LLSVPs. Due to its inherently heavy and stiff character, in equilibrated systems, we find the CAID material becomes especially hot so that the temperature-dependence of its density and viscosity results in reduced distinction between the intrinsically dense assemblages and the ambient mantle. Accordingly, the CAID material forms masses on the CMB that are relatively less

45 dense (0.625%-1.5%) and viscous than the adjacent mantle material, in comparison to the
 46 percentage differences obtained at common temperatures. We find that by adjusting our
 47 yield stress model to account for the influence of the CAID material on the geotherm, a
 48 highly satisfactory plate-like surface can be re-attained, however, the formation of a pair of
 49 LLSVP-shaped masses remains elusive.

50 **keywords:**

51 convection currents, and mantle plumes; composition and structure of the mantle;

52 dynamics of lithosphere and mantle; mantle rheology; mantle processes

53 **1 Introduction**

54 The Large Low Shear-wave Velocity Provinces (LLSVPs) observed below Africa and
 55 the Pacific Ocean (Ritsema et al., 1998; Ni et al., 2002; To et al., 2005; Garnero & Mc-
 56 Namara, 2008; Hernlund & Houser, 2008; Auer et al., 2014) comprise first order physical
 57 features in the lower mantle. Evidence that supports an at least partial chemical origin for
 58 the LLSVPs includes seismic observations of broadly spanning velocity-magnitude anomalies
 59 and the sharp shear-wave velocity gradient boundaries that confine these regions (Ritsema
 60 et al., 1998; Ni et al., 2002; To et al., 2005; Garnero & McNamara, 2008; Lekic et al.,
 61 2012). However, the inferred densities of the volumes encompassed within the LLSVPs
 62 vary. Evidence from the analysis of solid Earth tides (Lau et al., 2017) permits density
 63 anomaly excess of little more than a half percent in the LLSVPs, relative to the adjacent
 64 mantle. The Stonely modes of free oscillation data (Koelemeijer et al., 2017) suggest that
 65 the provinces are less dense overall than the surrounding mantle, despite their deep location.
 66 Such findings may hint at LLSVP evolution that is consistent with marginally stable, chem-
 67 ically dense but relatively hot, transient sluggish masses (Li et al., 2019) rising from the core
 68 mantle boundary (CMB). In any case, the conflicting observations add to the uncertainty
 69 in resolving the physical parameters responsible for the LLSVPs (e.g., McNamara, 2019).
 70 Indeed, several studies have shown that the morphology of the seismically slow provinces
 71 might be explained by thermal anomalies in isochemical models (Schuberth et al., 2009,
 72 2012; Davies et al., 2015). However, although arguments for purely thermal origins for
 73 the LLSVPs are credible, the observation of an anticorrelation between bulk sound and
 74 shear modulus (Su & Dziewonski, 1997; Ishii & Tromp, 1999; Masters et al., 2000; Tram-
 75 pert et al., 2004; Moulik & Ekström, 2016) makes a compositional origin for the LLSVPs

76 a compelling hypothesis. Accordingly, thermochemical modelling of the evolution of the
77 deep mantle requires obtaining discrete compositionally originating piles on the CMB that
78 spend at least part of their existence coalesced into a pair of roughly diametrically opposed,
79 steep-sided, hot but intrinsically dense provinces. Moreover, the detached chemically dis-
80 tinct volumes comprising the piles may reach over a thousand kilometres in height above
81 the CMB (Cottaar & Lekic, 2016).

82 The longevity of this arrangement may exceed several mantle transit times (the time
83 required for a parcel of mantle material to traverse the depth of the mantle at the mean
84 velocity of the plates). Previous studies have concluded that the LLSVPs have occupied
85 their current positions for several hundred million years (Burke & Torsvik, 2004; Dziewonski
86 et al., 2010; Torsvik et al., 2010). The location of large igneous provinces (LIPs) suggests
87 a correlation with the peripheries of the LLSVPs which have been argued to be the site
88 of plume generation zones (PGZs) formed by the influence of a sharp lateral temperature
89 gradient at the edges of thermochemical provinces (Torsvik et al., 2006; Burke et al., 2008;
90 Li & Zhong, 2017; Heyn et al., 2020). Given this connection, the age and positioning of the
91 LIPs suggests that the LLSVPs are both stable and relatively immobile (at least some of the
92 time) for periods in excess of 200 Myr. However, intermittent mobility of the LLSVPs, as well
93 as changes in their morphology, in response to plate motion and subduction zone migration
94 is evident in thermochemical convection studies that have imposed plate reconstruction
95 histories as surface boundary conditions (McNamara & Zhong, 2005; Zhang et al., 2010;
96 Flament et al., 2017). These studies have incorporated intrinsically dense components that
97 produce a pair of LLSVP-configuration provinces in response to the imposition of an evolving
98 plate velocity field that agrees with inferred records for the past 200+ Myr and speculative
99 histories extending back hundreds of millions of years before that. Although two current-
100 day LLSVP-type thermochemical features can be obtained on the CMB when recent plate
101 history is simulated, it is not clear that broad chemically distinct provinces on the CMB
102 can be obtained when full feedback between a thermochemical mantle component and the
103 plates is modelled.

104 Adhering to the hypothesis that the LLSVPs are compositional in nature (Humayun
105 et al., 2004; Tackley et al., 2005; Boyet & Carlson, 2006; Labrosse et al., 2007; Deschamps
106 et al., 2011), we investigate the feedback between a dynamically evolving plate-like surface
107 velocity field in two- and three-dimensional thermochemical mantle convection models and
108 the distribution of a compositionally anomalous and intrinsically dense (CAID) component

109 introduced into the deep mantle of vigorously convecting systems (e.g., Trim et al., 2014;
110 Trim & Lowman, 2016; Stein et al., 2020). With plates being absent, previous findings
111 (e.g., Hansen & Yuen, 1989; Tackley, 1998; LeBars & Devaille, 2004; McNamara & Zhong,
112 2004; Li et al., 2014; Tan et al., 2011) demonstrated the ability of a compositionally dense
113 mantle component to aggregate into a small number of stable piles that may interact with
114 the ambient mantle by responding to downwelling flow or influencing upwelling location.
115 The primary controlling influence over pile durability and longevity is the contrast in den-
116 sity between the ambient and enriched mantle. In addition, pile stability and morphology
117 has been shown to be dependent on the thermally derived viscosity contrast within the
118 convecting system (Li et al., 2014) as well as the intrinsic viscosity contrast between the
119 ambient mantle and CAID material (McNamara & Zhong, 2004; Heyn et al., 2018). The
120 rheological properties of a compositionally distinct component comprising the LLSVPs is
121 not known but it has been proposed that the LLSVPs are either enriched in Bridgmanite
122 and iron (Trampert et al., 2004) or depleted of ferropericlase (Yamazaki & Karato, 2001).
123 Given that an absence of interconnected regions of lower viscosity ferropericlase would have
124 a lower viscosity than a nearly pure Bridgmanite component (Ballmer et al., 2017), it may be
125 that the LLSVPs are inherently more viscous than the material in the surrounding mantle.

126 Due to feedback, the simultaneous modelling of dynamically obtained plates and an
127 intrinsically dense component in the deep mantle is a problem that is distinct from the mod-
128 elling of either a system that features compositionally dense piles while lacking plates or
129 the obtaining of a plate-like surface over-lying an interior where dense provinces are absent.
130 For example, previous studies have shown that, when they form, dense piles become mobile
131 or susceptible to breakup as a result of the impact of slab-like downwellings (Hansen and
132 Yuen, 1989; McNamara & Zhong, 2005; Langemeyer et al., 2020). Plate-like surface char-
133 acteristics produce especially focussed sheet-like downwellings and can also have a strong
134 effect on heat flow and the temperature profile of the mantle (Lowman et al., 2001); poten-
135 tially changing the requirements for pile formation. Similarly, the presence of compositional
136 provinces influences heat flow (Amit & Olson, 2015; Li et al., 2018; Langemeyer et al., 2020)
137 at the core mantle boundary (CMB), altering the thermal profile of the system and there-
138 fore a property upon which the obtaining of a plate-like surface behaviour strongly depends
139 (e.g., Stein & Hansen, 2008). Accordingly, the addition of a CAID component to a mantle
140 convection model exhibiting self-consistently generated plates can, potentially, result in the
141 cessation of the plate behaviour (Trim et al., 2014). Moreover, LLSVP-emulating provinces

142 can influence the positioning of thermal plumes which, in turn, can disrupt the stability of
143 the plates and the quiescence of their interiors. However, the converse is similarly applica-
144 ble. The inclusion of CAID material in the convecting system has the potential to be the
145 ingredient that alters the thermal field in a way that can allow plates to form when other
146 system parameters would otherwise not be conducive to their generation. Determining the
147 physical requirements for the generation of plates and LLSVP-like compositionally origi-
148 nating provinces is thus a problem that simultaneously requires satisfying two requirements
149 influenced by the same parameters.

150 Recognizing that the existence of plate tectonics and the LLSVPs are distinct but
151 coupled features simultaneously required by a global mantle convection model presents con-
152 straints and the potential for discovering limits on the composition of the LLSVPs. A small
153 number of studies of the dynamic interaction between these two first-order features at the
154 surface and base of the mantle have been presented (Trim et al., 2014; 2016) but continued
155 investigation may provide important further insight into important physical mechanisms
156 governing the Earth’s evolution. For example, two-dimensional modelling has shown that
157 the formation of a pair of CAID material provinces with LLSVP-type morphologies is not
158 guaranteed by the inclusion of a dense component in a fully dynamic model, but that
159 two stable, non-transient, piles can be obtained if the CAID material has specific qualities
160 (Langemeyer et al., 2018, 2020; Li et al., 2019). Previous studies (Trim et al., 2016) have
161 also shown that when a small number (1-3) of durable provinces are obtained, they can be
162 as mobile on the CMB as continents on the surface. Understanding whether CAID material
163 provinces are inherently stationary or prone to episodic bouts of translation also requires
164 modelling in conjunction with the existence of dynamic plates.

165 In this study we further investigate the feasibility of and requirements for distributing
166 a compositionally anomalous component of the mantle into two distinct and detached large
167 provinces. Previous work employing two-dimensional calculations (Langemeyer et al., 2020)
168 showed that in systems featuring self-consistently evolving plates, the formation of a small
169 number (i.e., 1-3) of provinces was just one possible outcome for the distribution of a dense
170 component comprising between 3 and 5% of the mantle’s volume. Following the examples
171 of previous studies, these authors varied both the relative intrinsic density and viscosity of
172 the dense mantle component (e.g., Heyn et al., 2018; Li et al, 2014; Deschamps & Tackley,
173 2008) and found that specific combinations of these parameters were conducive to producing
174 a durable and persistent pair of provinces that yielded periods in which LLSVP-like topo-

175 graphic profiles were obtained. (Alternative formations of the dense components range from
 176 a basal layer to multiple lower-volume piles.) In this study, we continue the approach of the
 177 previous work by first examining the influence of the stress-dependence of the lithosphere's
 178 rheology on the formation of the plate boundaries and the distribution of the CAID material
 179 in two-dimensional calculations and, subsequently, we model full 3D spherical shell systems
 180 featuring evolving plates and an intrinsically dense component.

181 2 Methods

182 2.1 Governing Equations

183 Thermochemical convection is modelled in a spherical geometry using a finite volume
 184 code (Tackley, 2000) for solving the dimensionless equations of mass, momentum and energy
 185 conservation in a bi-modally heated infinite Prandtl number Boussinesq fluid. Advection of
 186 the compositional field is calculated using the tracer-ratio method (Tackley & King, 2003).
 187 Thus, we specify

$$\nabla \cdot \mathbf{u} = 0 \quad (1)$$

$$\nabla \cdot [\eta(\nabla \mathbf{u} + (\nabla \mathbf{u})^T)] - \nabla P = (-\text{Ra}_T T + \text{Ra}_c C) \hat{r} \quad (2)$$

$$\frac{\partial T}{\partial t} = \nabla^2 T - \mathbf{u} \cdot \nabla T + H \quad (3)$$

188 and

$$\frac{\partial C}{\partial t} = -\mathbf{u} \cdot \nabla C \quad (4)$$

189 where \mathbf{u} is velocity, η is dynamic viscosity, P is the non-hydrostatic pressure, T is tempera-
 190 ture, t is time, H is the non-dimensional internal heating rate, Ra_T is the reference thermal
 191 Rayleigh number, Ra_c is the compositional Rayleigh number and C is the compositional
 192 field. The compositional field tracks the distribution of the intrinsically dense material such
 193 that $0 \leq C \leq 1$ and the value of C gives the ratio of the mass of the CAID material to the
 194 total mass, per unit volume. A region featuring a compositional value of $C = 1$ is entirely

195 comprised of enriched material, while $C = 0$ represents the ambient mantle. Equations (1)
 196 - (4) have been non-dimensionalised utilizing a thermal diffusion timescale. Furthermore,
 197 $\eta = \bar{\eta}/\eta^*$, where $\bar{\eta}$ is the dimensional field and η^* is the dimensional reference viscosity.

198 The thermal Rayleigh number and compositional Rayleigh number are defined as:

$$\text{Ra}_T = \frac{\rho_0 g \alpha \Delta T d^3}{\kappa \eta^*} \quad (5)$$

199 and

$$\text{Ra}_C = \frac{\Delta \rho_C g d^3}{\kappa \eta^*}, \quad (6)$$

200 where ρ_0 is the reference density defined as $\rho_0 = \rho(T_0)$, α is the thermal expansivity, d is the
 201 thickness of the mantle, $\Delta T = T_b - T_0$ is the difference between the superadiabatic isothermal
 202 basal temperature (T_b) and the isothermal surface temperature (T_0), g is acceleration due
 203 to gravity, $\Delta \rho_C$ is the contrast in density between intrinsically dense and ambient mantle
 204 material and κ is the thermal diffusivity.

205 The contrast in the Rayleigh numbers is described by the value of the buoyancy num-
 206 ber $B = \text{Ra}_C / \text{Ra}_T = \Delta \rho_C / (\rho_0 \alpha \Delta T)$ (representing the relative influence of thermal and
 207 compositional effects on the density of the mantle material). For example, with a buoyancy
 208 number of 0.5 the Boussinesq approximation results in an enriched mantle component at
 209 a non-dimensional temperature of 0.5 having the same density as the ambient mantle at a
 210 non-dimensional temperature of 0.0. (In general, for constant thermal expansion coefficient,
 211 $\rho(T = B, C = 1.0) = \rho(T = 0.0, C = 0.0)$).

212 The governing equations (1) - (4) are thus completed by the incorporation of a lin-
 213 earized equation of state

$$\rho(T, C) = \rho_0 [1 + \alpha \Delta T (BC - T)]. \quad (7)$$

214 The non-dimensional internal heating rate is defined as:

$$H = \frac{\rho_0 \epsilon d^2}{k \Delta T} \quad (8)$$

Table 1. Dimensional quantities adopted for this study.

Quantity	Dimensional Value
η^*	$4.5 \times 10^{19} \text{ Pa} \cdot \text{s}$
κ	$1 \times 10^{-6} \text{ m}^2 \text{ s}^{-1}$
d	$2.89 \times 10^6 \text{ m}$
ΔT	2500 K
diffusion time, d^2/κ	265 Gyr
ρ_0	3700 kg m^{-3}
g	10 m s^{-2}
α	$2 \times 10^{-5} \text{ K}^{-1}$
k	$4.3 \text{ W m}^{-1} \text{ K}^{-1}$

215 where ϵ is the dimensional heating rate per unit mass (specified here as uniform throughout
 216 the mantle) and k is the thermal conductivity. The dimensional values corresponding to the
 217 reference Rayleigh number and assumed in the dimensional interpretation of the results are
 218 provided in Table 1.

219 2.2 Rheology

220 A mobile surface is attained through the implementation of a temperature-dependent
 221 viscosity combined with viscoplastic yielding. The viscosity temperature-dependence is spec-
 222 ified using a non-dimensional Arrhenius-type law, where

$$\eta_T = \exp\left(\frac{E_a}{T+1} - \frac{E_a}{2}\right) \quad (9)$$

223 where E_a is a non-dimensional activation energy, determining the magnitude of the viscosity
 224 contrast due to temperature alone, between material at the surface and the core mantle
 225 boundary (CMB). This study uses a set value of $E_a = 29.96$ to generate a thermal viscosity
 226 contrast, ΔT , of 3.2×10^6 .

227 A non-dimensional yield stress, σ_{yield} , is implemented by prescribing a surface yield
 228 stress value, σ_{surf} , and a mantle yield stress value, σ_{mantle} , that defines the yielding point

229 below a prescribed non-dimensional depth, d_l . The prescribed depth-dependent yield stress
 230 is

$$\sigma_{\text{yield}} = \min[\sigma_{\text{mantle}}, \sigma_{\text{surf}} + \frac{D(\sigma_{\text{mantle}} - \sigma_{\text{surf}})}{d_l}], \quad (10)$$

231 where D is a non-dimensional depth below the model surface and d_l is the depth below
 232 which the mantle is prescribed a fixed yield stress value of σ_{mantle} .

233 We incorporate plastic yielding by utilizing a linearly proportional relationship between
 234 yield stress and yield viscosity, such that

$$\eta_{\text{yield}} = \frac{\sigma_{\text{yield}}}{2\dot{\epsilon}} \quad (11)$$

235 where $\dot{\epsilon}$ is the second invariant of the strain rate tensor, $\sqrt{\frac{1}{2}\epsilon_{ij}^i\epsilon_{ij}^i}$.

236 In addition to the influences of temperature and stress, the variation in the rheological
 237 behaviour of the system is augmented by the inclusion of a specified increase in lower mantle
 238 viscosity. A number of geophysical observables have inferred an increase in mantle viscosity
 239 by a factor of 30 or greater at a depth corresponding to the phase transition from spinel
 240 to Bridgmanite + magnesiowüstite (Boehler, 2000; Hager, 1984; Richards & Hager, 1984;
 241 King & Masters, 1992; Mitrovica & Forte, 2004). Therefore, we specify an increase in lower
 242 mantle viscosity so that

$$\eta_{\text{TD}} = \eta_{\text{T}} \times \eta_{\text{D}}, \quad (12)$$

243 where

$$\eta_{\text{D}} = 1 \quad \text{for} \quad z \geq 1 - 0.227 \quad \text{and} \quad \eta_{\text{D}} = 30 \quad \text{for} \quad z \leq 1 - 0.227, \quad (13)$$

244 where z represents the non-dimensional height above the core mantle boundary with $z =$
 245 $1 - 0.227$ corresponding to a dimensional depth of 660km.

246 To account for the impact on viscosity of temperature, depth and stress dependence,
 247 we define a composite viscosity that considers the relative importance of the contributing
 248 influences

$$\eta_{\text{comp}} = 1/[1/\eta_{\text{TD}} + 1/\eta_{\text{yield}}]. \quad (14)$$

249 The final effect on viscosity, specifically explored in this study, is the specification of an
 250 intrinsic viscosity contrast owing to composition, $\Delta\eta_c$. The two component fluid has a
 251 viscosity given by $\eta_{\text{comp}} \times (\Delta\eta_c)^C$, where C is the local value of the composition field.

252 **2.3 Thermal steadiness**

253 In this study, we vary $\Delta\eta_c$, the buoyancy number, B , the yield-stress value as a func-
 254 tion of depth and the volume of the intrinsically dense component in the systems. All cases
 255 featuring a CAID material component are initiated from snapshots taken from statistically
 256 steady systems that feature no CAID component. Details of the initial conditions are given
 257 in the following section. The calculations incorporating CAID material are each a continu-
 258 ation of the calculation used to obtain the initial condition, with the addition of a uniform
 259 thickness layer of CAID material enveloping the core at the start of the new experiment.
 260 Subsequently, these new systems converge to statistically steady states themselves.

261 Calculations are considered to have reached a statistically steady-state when heat flow
 262 from the surface is balanced by the sum of the heat flow from the core to the mantle and
 263 the internally generated heat. Specifically, a steady-state is considered to be established
 264 when the time-averaged non-dimensional internal heating rate (set to 30 in all calculations)
 265 is equal to the difference in non-dimensional heat flows:

$$\frac{3(F_s - F_b f^2)}{1 + f + f^2}, \quad (15)$$

266 where F_s and F_b are the mean non-dimensional surface and basal heat fluxes and f is
 267 the ratio of core to planetary radius (we specify a terrestrial value of 0.547 in this study).
 268 Convergence to a temporally averaged steady-state condition is obtained for the initial
 269 condition used in both the 2D and 3D calculations.

270 **3 Results**

271 **3.1 Yield stress and model dimension**

272 We first consider the behaviour of two-dimensional systems with a uniform non-
 273 dimensional yield stress of 2×10^7 (110 MPa). Previously, Langemeyer et al. (2020) described

274 the evolution of two-dimensional calculations featuring a yield stress of 1×10^7 in other-
 275 wise identical systems. However, employing the same values for the system parameters,
 276 Langemeyer et al. (2021) showed that in isochemical three-dimensional systems, a uniform
 277 yield stress of 2×10^7 results in a more plate-like surface behaviour, with time-dependent
 278 boundaries that commonly exhibit Earth-like structure; namely, the appearance of spread-
 279 ing boundaries comprised of divergent segments and transform-like offsets coexisting with
 280 contrasting arcuate convergent boundaries. The primary objective of the study presented
 281 here is to examine the feedback between plate-like surface behaviour and a CAID compo-
 282 nent in the lower mantle, and to gain insight into any differences arising from the system
 283 dimensionality. Accordingly, we employ the higher yield stress in all calculations by first
 284 re-examining the behaviour of 2D systems. In later sections we present 3D calculations
 285 featuring a CAID component with other system parameter values matching those employed
 286 by Langemeyer et al. (2021).

287 The impact of the higher yield stress is to reduce the number of surface weak zones
 288 associated with subduction and divergence. The distribution of CAID material and the
 289 internal thermal structure are affected. As in the previous two-dimensional modelling work
 290 (Langemeyer et al., 2020) the buoyancy number of the CAID material as well as its viscosity
 291 relative to the ambient material are both varied, in order to determine their influence on
 292 the distribution of the CAID material.

293 We introduce a naming convention to simplify the discussion. Model names follow the
 294 format #DBbbDdd, where bb is the buoyancy number of the intrinsically dense material,
 295 dd is the contrast in viscosity between ambient and intrinsically dense material (at the same
 296 temperature and depth), represented as a multiplicative factor, and # is the number of
 297 dimensions used in the calculation. For example a three-dimensional calculation featuring a
 298 buoyancy number of 0.85 and a CAID material intrinsic viscosity that is a factor of 10 times
 299 greater than the viscosity of the ambient mantle material is designated: Model 3DB0.85D10.

300 **3.2 Initial condition**

301 Figure 1 shows the initial condition fields used for all 2D calculations presented. Cor-
 302 responding temperature and viscosity are shown and reveal a pair of distinct downwellings.
 303 The initial condition is generated using an isochemical model. The surface features spread-
 304 ing centres and downwelling generating zones of focussed plate convergence, while the base

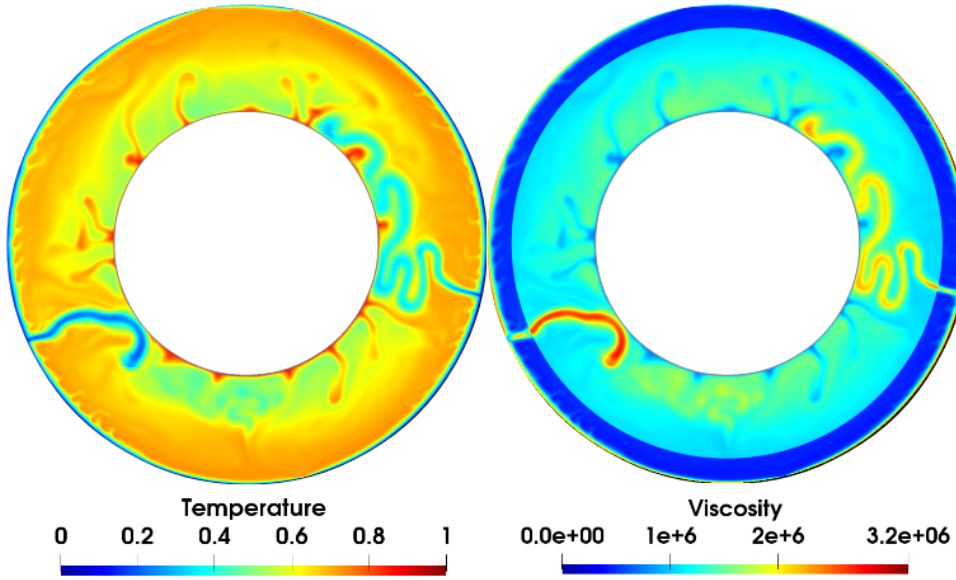


Figure 1. The initial condition non-dimensional temperature and viscosity fields used for all 2D calculations presented in this study. All two-dimensional calculations presented are obtained for a spherical annulus geometry with a resolution of 128×1024 . The CAID material advection is modelled with the tracer ratio method (Tackley & King, 2003) using approximately 4.2 million tracers in each case.

305 of the mantle produces multiple active upwellings. The 2D calculations presented in the
 306 remainder of this study are initiated by adding a uniform height layer of CAID material
 307 enveloping the CMB, into the fields shown in Fig. 1. The evolution of this material is then
 308 analysed with time 0.0 corresponding to the initial condition.

309 **3.3 Distribution of the CAID material in 2D calculations**

310 Figure 2 shows temperature and composition field snapshots from nine calculations
 311 in which all parameters are identical, with the exception of the buoyancy number of the
 312 CAID material and its viscosity relative to the ambient mantle ($\Delta\eta_C$). The CAID material
 313 comprises 3.5% of the mantle volume in all calculations. The snapshots show the presence
 314 of either one or two downwellings that are formed by surface convergence at a high-stress
 315 originating weak zone. In general, these downwellings persist for approximately one to

316 several mantle transit times before waning. Upwellings forming in regions devoid of CAID
 317 material, as well as on top of CAID provinces, lack the vigour to reach the base of the
 318 plates. For cases where $\Delta\eta_c = 1$ or 10, upwellings commonly occur at the edges or highest
 319 elevation points of the dense provinces. In cases where $\Delta\eta_c = 100$ upwelling formation is
 320 often coincident with the points of highest elevation above CAID material piles. Regardless
 321 of the location of upwelling formation, at no point are upwellings observed to impinge upon
 322 the lower lithosphere.

323 Throughout the evolution of these calculations the intrinsically denser component is
 324 often distributed into one large pile with intermittent episodes characterized by the forma-
 325 tion of two piles (often diametrically opposed). The cases shown exhibit a single pile (with
 326 small secondary piles in some cases) when $\Delta\eta_c \geq 10$ or 100. In contrast, two diametrically
 327 opposed piles are common when $\Delta\eta_c = 1$. We also find that a pair of diametrically opposed
 328 piles of similar size are often present early in model evolution (e.g., in Models 2DB0.75D100
 329 and 2DB1.0D100), but eventually a single pile is formed. In general, when the intrinsic
 330 viscosity of the CAID material is lower, transient piles tend to collapse and spread over
 331 the CMB following interaction with downwellings that push the dense component into high
 332 structures. As the intrinsic viscosity contrast, $\Delta\eta_C$ is increased, events leading to compres-
 333 sion, and to higher and less wide piles (e.g., due to the impact of neighbouring downwellings),
 334 leave longer-lived signatures in stiffer piles. An inverse trend is also observed between the
 335 buoyancy number and the height of CAID material piles so that cases with a buoyancy
 336 number of 0.75 typically feature greater height piles than cases with a buoyancy number of
 337 1.0. A potential impact on the dynamics responsible for the formation of the plates results
 338 from a decrease in the relative viscosity of the CAID material (e.g., when it is hot and not
 339 intrinsically higher in viscosity) or an increase in buoyancy number. Both factors lead to
 340 an increase in CMB blanketing by the dense component. Increased coverage of the CMB
 341 can lead to a cooler mantle in comparison to an isochemical case. For example, a blanket-
 342 ing layer, or discrete piles, can inhibit heat flow from the core. As a result, mean global
 343 viscosity is affected by both the buoyancy number and the intrinsic viscosity of the CAID
 344 material and, in turn, a resulting difference in plate behaviour can determine the number of
 345 downwellings able to form and therefore whether CAID material disperses into one or more
 346 piles. In summary, the findings from our 2D calculations indicate that a higher intrinsic
 347 viscosity for the CAID material promotes degree-1 mantle flow, especially for cases with
 348 reduced buoyancy ratio.

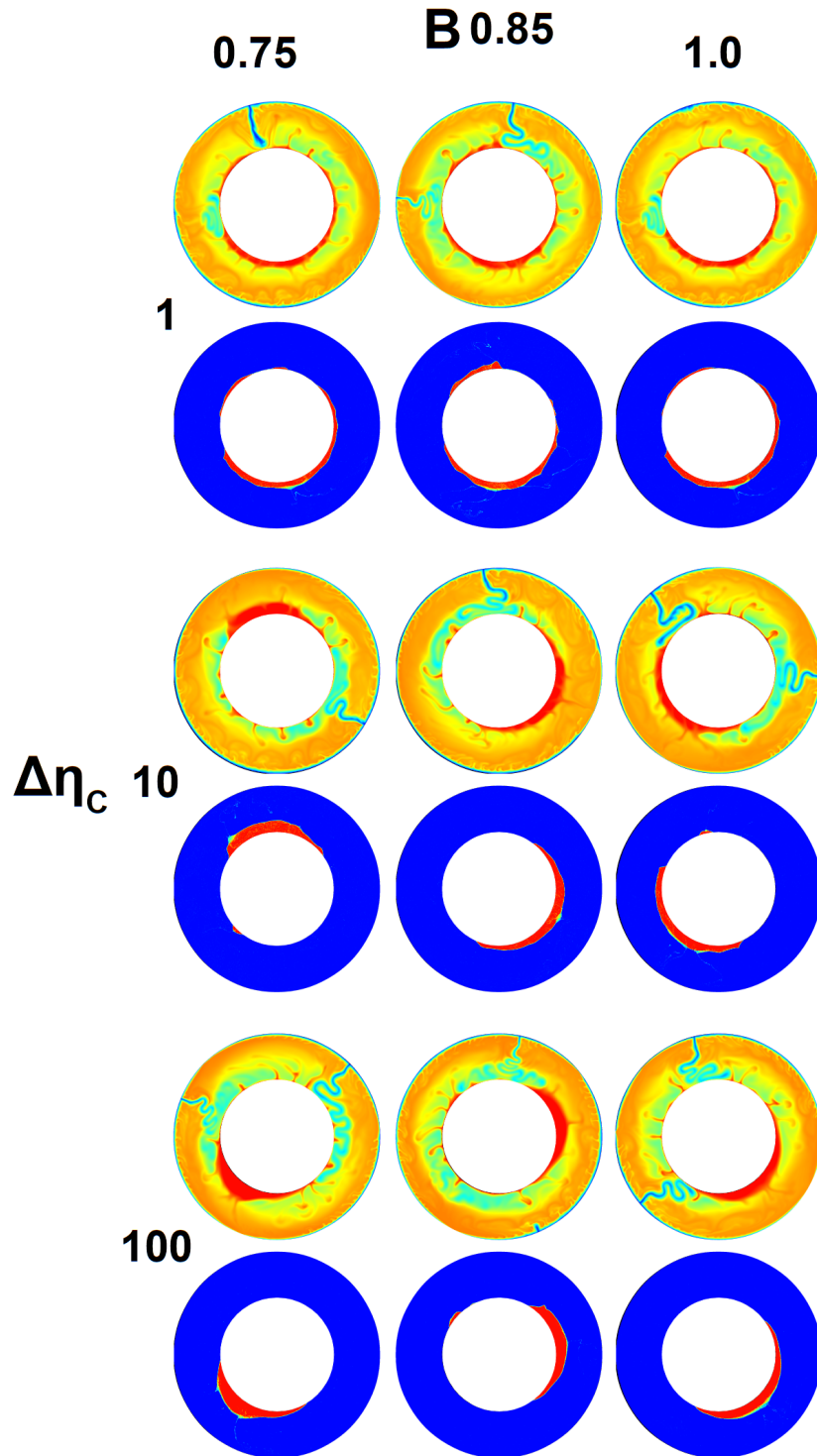


Figure 2. Temperature (top) and composition (bottom) field snapshots featuring a range of buoyancy numbers (columns) and CAID material intrinsic viscosities (rows). The temperature scale is the same as in Fig. 1. Red and blue in the composition fields correspond to values of 1.0 and 0.0, respectively.

3.4 Thermal state time-dependence and CAID material distribution

Figure 3 presents snapshots of the thermal and compositional fields from Models 2DB0.75D100 and 2DB0.75D10, as well as basal and surface heat flux time series for the three cases from Fig. 2 featuring a buoyancy number of 0.75. In general, mean heat flux is minimally influenced by the intrinsic viscosity of the CAID material, however, variation between maximum and minimum surface heat flux values is reduced when there is no intrinsic contrast in viscosity between the different compositions (most likely because the predominantly degree-one-flow cases are more impacted by the opening and closing of a smaller number of plate boundaries). Red and blue vertical lines are annotated on the heat flux time series, indicating the timing of the snapshots shown. Both times are selected for their relation to a spike in surface heat flux, which occurs following the transition from a system with a single downwelling to periods featuring the development of a new surface weak zone (resulting in the formation of second downwellings that supersede the existing downwellings which subsequently dissipate). Pre-existing long lasting downwellings appear in the southern and northern hemispheres for cases 2DB0.75D100 and 2DB0.75D10, respectively, while young downwellings are seen to form in the northern and southern hemispheres in the same cases. For case 2DB0.75D100 it is observed that mean surface heat flux increases by approximately 21 mW/m^2 following the initiation of a downwelling in the northern hemisphere. The basal heat flux is observed to have a similar response to the development of new downwellings. However, throughout the period modelled, the basal heat flux varies over a narrower range of values with a slightly delayed response.

Sudden variations in heat flux associated with the development and loss of surface downwelling regions indicate the transient nature of these calculations. A similar frequency in the rate of heat flux variation is observed for all three cases presented in Figure 3 with each case experiencing at least one rapid increase in surface heat flux per Gyr, indicating the formation of a new zone of convergence forms in the calculations at intervals of 1 Gyr or less. Generally, changes in the amplitude of the heat flux time variations also coincide with changes in the nature of the CAID material's distribution due to the feedback between the surface motion and intrinsically dense component.

Figure 4 is similar to Figure 3, but illustrates the evolution of cases where $\Delta\eta_c = 100$. For reference, Model 2DB0.75D100 appears (in red) again. Solid vertical lines are used to indicate the time corresponding to each snapshot at the left. The snapshot of Model

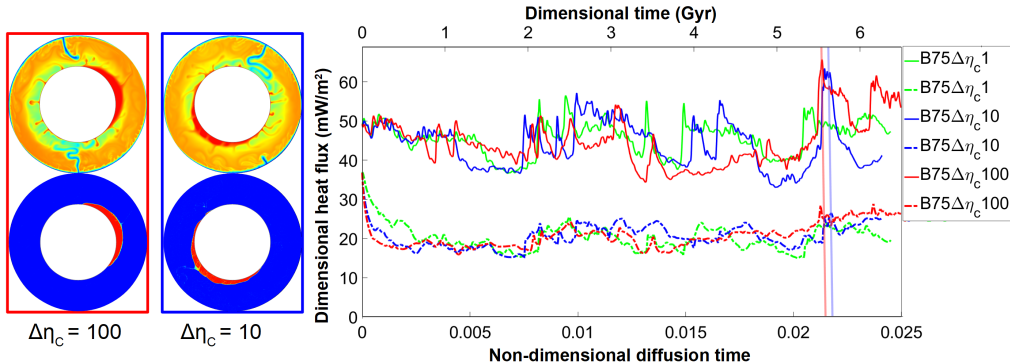


Figure 3. (Thermal and compositional field snapshots from Models 2DB0.75D100 (left) and 2DB0.75D10 (right) and the corresponding CMB (dashed) and surface (solid) mean heat flux time series. Heat flux is shown in dimensional units of mW/m^2 by using the values from Table 1, while dimensional time is provided on the top x -axis and non-dimensional (diffusion) time is given on the bottom axis. The times corresponding to each snapshot are indicated on the heat flux plots by a vertical line of the same colour as the associated heat flux curves.

381 2DB0.75D100 features a high surface heat flux and two downwellings, while the snapshot
 382 from Model 2DB1.0D100 corresponds to a period of low heat flux and the existence of only
 383 a single region of subduction. In comparison to Model 2DB0.75D100, Model 2DB1.0D100
 384 exhibits significantly lower minimum surface heat flux values during its evolution. These
 385 are associated with the intermittent cessation of surface convergence, and therefore down-
 386 wellings, and the replacement of a continually mobile surface with an episodic regime of
 387 convection. Correspondingly, this case features the highest average internal temperatures
 388 of all of the 2D calculations presented. Thus we find that in a 2D system, a combined high
 389 buoyancy number and intrinsic viscosity contrast can lead to a disruption of the large scale
 390 flow owing to intermittent stagnation of the surface.

391 Figure 5 shows the thermal and compositional field evolution for Models 2DB0.75D100
 392 and 2DB1.0D100. The sequence on the left depicts two distinct piles of anomalously dense
 393 material occupying opposite hemispheres throughout the illustrated period. Additionally,
 394 the surface of this system features two zones of localized convergence that result in the
 395 consistent preservation of widely separated regions of downwelling. The focused subducting
 396 material impinges upon the CAID material near the core mantle boundary, forming voids
 397 in which no CAID material is present above the CMB. Additionally, as exhibited by the

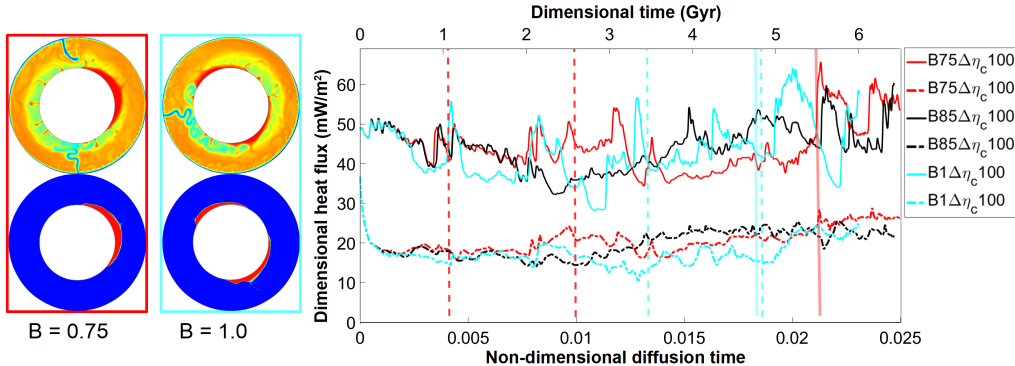


Figure 4. (Thermal and compositional field snapshots for Models 2DB0.75D100 (left) and 2DB1.0D100 (right) and the corresponding CMB (dashed) and surface (solid) mean heat flux time series. Heat flux is plotted in dimensional units of mW/m^2 while dimensional time is provided on the top x -axis and non-dimensional (diffusion) time is shown on the bottom axis. The times corresponding to each snapshot are indicated by a solid vertical line of the same colour as the associated heat flux curve. Dashed vertical lines bound the time ranges presented in Figure 5.

398 northern hemisphere evolution between 0.95 and 1.58 Gyr, downwelling lithosphere can act
 399 to further shape CAID material into narrower piles with steeper sides. Moreover, the height
 400 of the piles in the two hemispheres can differ by roughly a factor of two.

401 Model 2DB1.0D100 displays a greater transience in the CAID material distribution
 402 over a slightly shorter period; initially two diametrically opposed piles are present, which
 403 coalesce into a single pile before breaking apart again. Unlike Model 2DB0.75D100, the sur-
 404 face of Model 2DB1.0D100, features only a single region of focused convergence throughout
 405 the illustrated period. Accordingly, the system is less efficiently cooled by subduction and
 406 is persistently hotter. At time 0 Gyr, downwelling material originating near "two o'clock"
 407 sinks to the core mantle boundary driving the CAID material to move laterally about the
 408 CMB. At time 0.52 Gyr, the downwelling material has spread over the CMB forcing the
 409 CAID material into a single pile covering most of the CMB in the opposite hemisphere. At
 410 0.78 Gyr, downwelling at two o'clock ceases and a new region of downwelling forms above
 411 the centre of the CAID province. By 1.04 Gyr, the downwelling has generated a new void
 412 in the CAID material coverage of the CMB and has re-established a two pile distribution.

413 These two cases illustrate the impact of plate convergence on the formation of diamet-
 414 rically opposed provinces. More than one persistent downwelling is required for long term

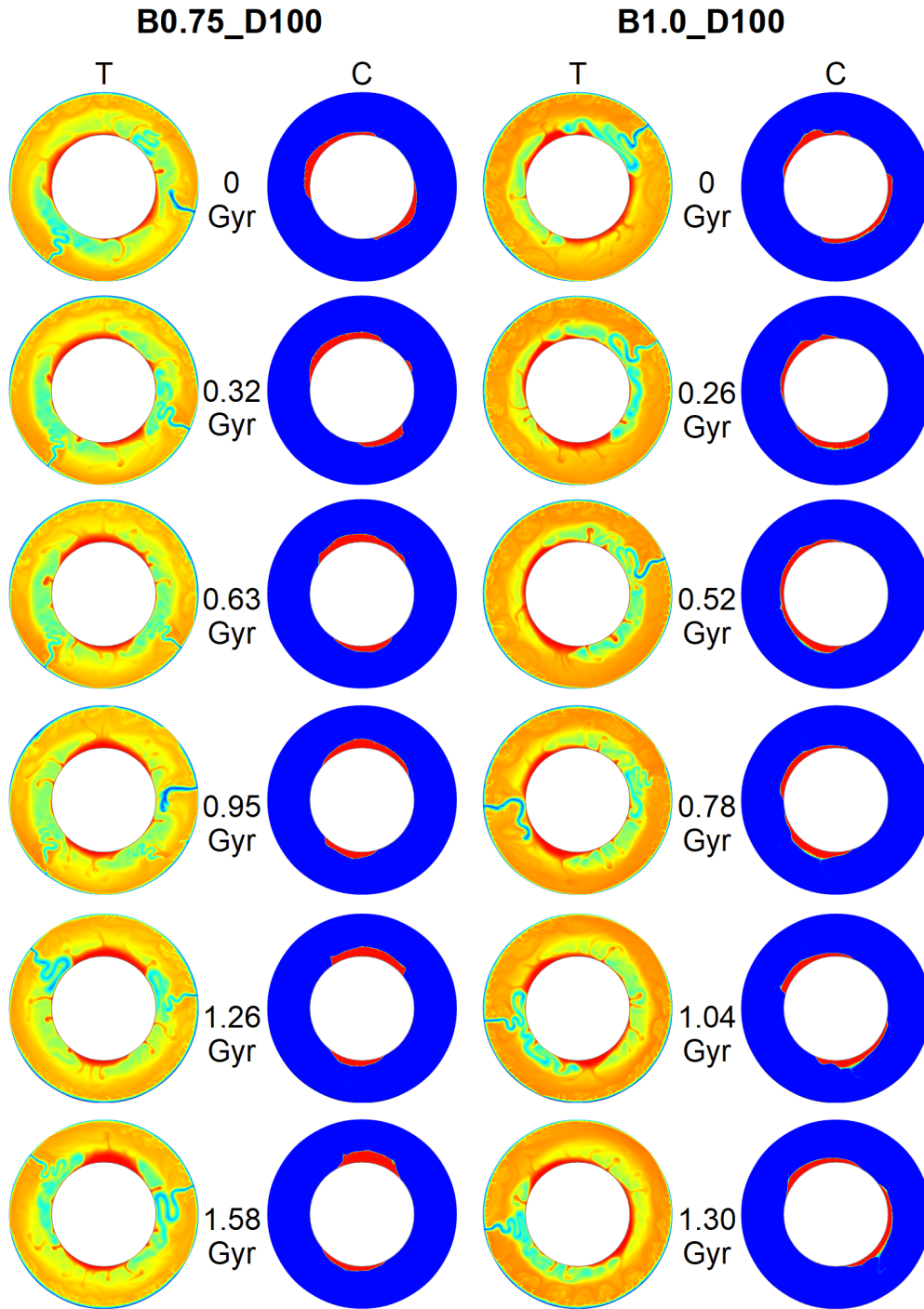


Figure 5. A series of thermal and compositional field snapshots for Models 2DB0.75D100 (left) and 2DB1.0D100 (right) displaying the evolution of each case over approximately 1.5 Gyr. An age is indicated next to each set of annuli images indicating the time that has passed since the top-most panel. The times corresponding to the first and last snapshot are indicated by dashed vertical lines in Figure 4. The temperature scale is the same as in Fig. 1.

415 maintenance of two diametrically opposed provinces. Subduction initiated over a void in
 416 CAID material coverage of the CMB will enforce the coalescing of material into a single
 417 pile, while subduction initiated over a province will often divide the province into two piles.
 418 If, in the latter case, the subduction is robust and long lasting the piles will once again
 419 coalesce into a single province in the opposite hemisphere. Of final note, feedback between
 420 the CAID material and plate convergence zones can result in global temperature changes
 421 that are conducive to the intermittent cessation of surface mobility.

422 3.5 Three-dimensional convection calculations

423 Although we expect some of the behaviour observed in two-dimensional calculations
 424 to be maintained in three-dimensional systems (e.g., the impact of the intrinsic viscosity
 425 contrast of the two component system as well as the influence of the buoyancy number
 426 on province height and total core coverage), the limited degrees of freedom in the two-
 427 dimensional system can result in dynamics that will not be reproduced in a full spherical
 428 shell; suggesting the potential for some departures from the 2D behaviour. For example,
 429 the CAID material piles formed in 2D systems break apart and disperse over the CMB
 430 in a similar way to the modelling of supercontinent breakup and dispersal at the surface
 431 of the mantle (Gurnis, 1988). However, limitations caused by restricting the migration of
 432 distinct components, like continental lithosphere (Zhong & Gurnis, 1991) or CAID material
 433 provinces (Langemeyer et al. 2020), to motion on a great circle can force cycles that are
 434 unlikely to be realized in three-dimensions, or eliminate realistic alternatives for evolution
 435 that require three dimensions. For example, 2D systems can only model supercontinent
 436 cycles that replicate end-member paradigms for ocean opening and closure, rather than the
 437 spectrum of possibilities that actually exist (Murphy & Nance, 2004, Rolf et al., 2012).
 438 Moreover, in two dimensions, changes in the direction of the migration of a dense province
 439 requires reversals, as with changes in plate motion (e.g., Lowman et al., 2001). In the case of
 440 plate motion this restriction can introduce episodicity (Koglin et al., 2005), including brief
 441 periods of stagnation, and therefore an affect on global temperatures.

442 A 3D model will allow for different options in the location, relative orientation and
 443 distribution of downwellings originating along bands of surface convergence. In the remain-
 444 der of this study, we focus on how the feedback between downwellings and CAID material
 445 affects the formation of CAID provinces within a 3D system. Additionally, we analyze the
 446 impact of the CAID material component on the evolution of localized regions of deformation

447 at the surface. Specifically, we investigate whether a two component deep mantle affects
 448 the mobility of plates and whether the contrasting structure of convergent and divergent
 449 surface features is persistent; as observed in the isochemical calculation (Langemeyer et al.,
 450 2021) .

451 In addition to the uniform (2×10^7 ; 110 MPa) yield stress calculations that allow for
 452 a direct comparison with the two dimensional model results, we investigate the impact of a
 453 reduction in the surface yield stress on the interior thermal structure and the distribution of
 454 CAID material. In this case, the surface yield stress has been weakened by a factor of two
 455 but increases linearly until reaching a non-dimensional depth of 0.02 (60 km), below which
 456 the yield stress is again set at a constant valued 2×10^7 . This alternative model is conducive
 457 to generating more convergent bands that result in downwellings (although, for isochemical
 458 models, it is much less effective in producing a dichotomy in the structure of divergent and
 459 convergent boundaries; marked by the appearance of transform faults in the former case).
 460 The choice of investigating cases with a weaker surface is prompted by an understanding
 461 that the CAID material is driven into piles by its interaction with downwellings, and that
 462 adjusting a primary factor affecting the formation of downwellings may have a profound
 463 effect on recovering a system with a pair of distinct provinces and a plate tectonic-like
 464 surface.

465 **3.6 Initial condition for the 3D calculations**

466 Figure 6 presents snapshots of the initial conditions used for the 3D calculations.
 467 Figure 6a shows viscosity and divergence field snapshots for the initial condition used to
 468 start all 3D calculations featuring a uniform yield stress. In addition, the interior thermal
 469 structure is displayed utilizing hot and cold isosurfaces corresponding to focussed upwelling
 470 and downwelling material, respectively, as well as the corresponding temperature field power
 471 spectrum (horizontal) as a function of non-dimensional height (vertical) above the CMB.
 472 Similarly, Figure 6b shows the initial condition utilized for all depth-dependent yield stress
 473 calculations described. The initial conditions were generated from calculations in which a
 474 CAID component is absent. In the uniform yield stress case, the surface features just three
 475 plate-like regions at the time shown, however, for the parameters selected, half-a-dozen
 476 plates often evolve. Moreover, the parameters are identical to those chosen in the earlier 2D
 477 computations and have demonstrated compatibility with the generation of distinct CAID
 478 provinces in that geometry. The surface zones of convergence and divergence are distinct

479 in their structure with the former appearing as smooth continuous (arcuate) bands and the
 480 latter appearing as a series of spreading centres (analogous to ridges) punctuated by offsets
 481 (analogous to transform faults). The depth-dependent yield stress case exhibits an initial
 482 condition featuring more distinct plate-like regions but less well defined divergent boundaries
 483 (and no transform-like offsets). The surface shows a number of zones of focused deformation
 484 and power across a band of harmonics (peaking at degree three). The cases presented in
 485 the remainder of this study are initiated from these fields with a uniform thickness layer
 486 of CAID material (accounting for 3.0% of the mantle volume) enveloping the CMB, unless
 487 noted otherwise.

488 **3.7 CAID material distribution in three-dimensional calculations**

489 Figure 7 presents snapshots from nine calculations incorporating intrinsically dense
 490 material with different buoyancy numbers and viscosity contrast owing to composition.
 491 These cases all feature a uniform non-dimensional yield-stress of 2×10^7 . In addition to
 492 the viscosity field just below the surface, a hot interior isosurface and the CAID material
 493 distribution are shown. The rendering of the surface viscosity field utilizes the same colour
 494 definitions as the images presented in Figure 6, while the red and blue isosurfaces show a
 495 thermal cut-off of non-dimensional temperature 0.82 and the distribution of CAID material,
 496 respectively. For the same cases, images from temporally corresponding but diametrically
 497 opposed viewing angles are presented in Supplementary Figure 1. For a number of cases,
 498 following the introduction and evolution of the CAID material, similar divergent and conver-
 499 gent surface features to those exhibited in the isochemical initial condition are maintained.
 500 In addition, the length-scale of these plate boundaries is maintained in many cases, with
 501 long bands of deformation persisting for a mantle transit time or longer, such as in Models
 502 3DB1.0D10 and 3DB0.85D100 which exhibit focussed weak zone bands subtending 180° .
 503 Some snapshots, such as for Model 3DB1.0D1, display a surface with a greater number
 504 of weak zones (as revealed by the near surface power spectrum) resulting in an increased
 505 number of isolated surface regions analogous to distinct plates. However, in all cases, far
 506 fewer plate-like regions are found than is currently observed on Earth.

507 A variety of CAID material distributions are shown in Figure 7, however, despite
 508 frequent sampling, none of the cases examined with this yield stress model were found
 509 to produce a persisting pair of CAID material provinces, as would be analogous to the
 510 structure of the LLSVPs observed at the base of Earth’s mantle. Supplementary Figure 2

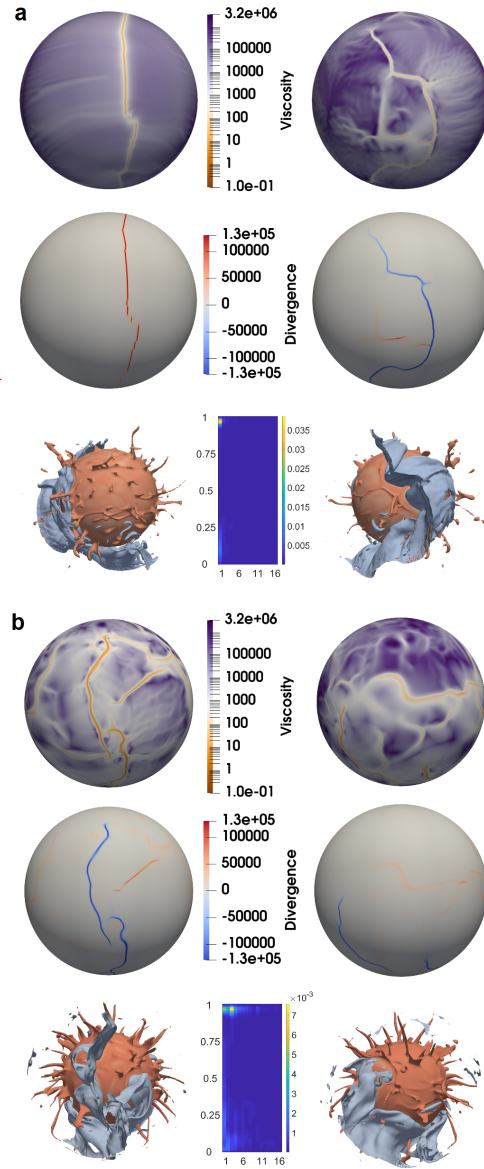


Figure 6. The initial conditions used for the initiation of uniform yield stress (2×10^7 ; 110 MPa) 3D calculations (a) and cases with a depth-dependent yield stress (surface = 1×10^7 , interior = 2×10^7) (b). Near surface viscosity and non-dimensional divergence as well as internal thermal structure and its power spectra (as a function of height above the CMB) are presented for each case. The thermal isosurfaces correspond to non-dimensional temperatures of 0.82 (red) and 0.42 (blue). The left and right columns show diametrically opposed views. Cold isosurfaces are clipped at a non-dimensional depth of 0.05 to reveal the thermal interior structure. All 3D model calculations are carried out in a spherical geometry utilizing a yin-yang grid with a resolution of $96 \times (768 \times 256) \times 2$ and 930 million tracers.

511 presents Mollweide projections of the compositional field 145 km above the CMB in nine
 512 plots corresponding to the snapshots shown in Fig. 7. The most common distribution of
 513 CAID material observed is that of a single large pile, typically extending over an area of
 514 at least one hemisphere. Generally, large voids are carved out of the dense layer by robust
 515 downwellings sinking to the core mantle boundary. Some smaller piles of CAID material are
 516 seen in Model 3DB1.0D100 of Figure 7 and Model 3DB0.85D10 of Supplementary Figure 1.
 517 Only a small amount of the total CAID component is included in these isolated piles and
 518 typically they tend not to be completely detached, but rather are connected to the larger
 519 piles by tendrils of the CAID component reaching across the CMB. As was found in the
 520 study of the 2D cases, the height and steepness of the piles appears to be greatest when the
 521 intrinsic viscosity of the dense component is large relative to the ambient mantle. Those
 522 cases where $\Delta\eta_C$ equals 100 feature the greatest altitude and steepest sided piles. In accord,
 523 these cases can also exhibit less core coverage by the CAID component. A low buoyancy
 524 number CAID component is less resistant to being forced aside by cold downwelling material.
 525 Consequently downwellings can push a lower buoyancy ratio dense component laterally as
 526 the reduced density of the piles means they are more readily deformable as well as able to
 527 rise to higher altitudes. Furthermore, CAID material with an increased $\Delta\eta_C$ will respond
 528 more slowly to the opportunity to spread around the core mantle boundary during periods
 529 when the pile experiences diminished lateral forcing.

530 ***3.7.1 Temperature field power spectra***

531 For each case in Fig. 7 a plot of the thermal power spectra as a function of height
 532 above the CMB is shown in Supplementary Figure 3. The power spectra indicate the
 533 dominant degrees in the upper thermal boundary layer as well as the distribution of the
 534 CAID material in the deep mantle. Long wavelength peaks in the power spectra near the
 535 surface of the systems are typical, with the greatest power usually occurring at degree one or
 536 two, corresponding to the number and spacing of bands of focussed surface deformation. In
 537 addition to the strong degree one or two surface power observed, a subset of cases including
 538 Models 3DB1.0D1 and 3DB0.85D100 display some power in higher degrees. In particular,
 539 these cases feature a greater number of bands of lithospheric weakness traversing shorter
 540 distances across the surface. The power focused in the lowest degrees in the mantle, just
 541 above the CMB, results from the influence of CAID material distribution and is generally
 542 much stronger than focusing observed at the surface. Due to the relatively low buoyancy of

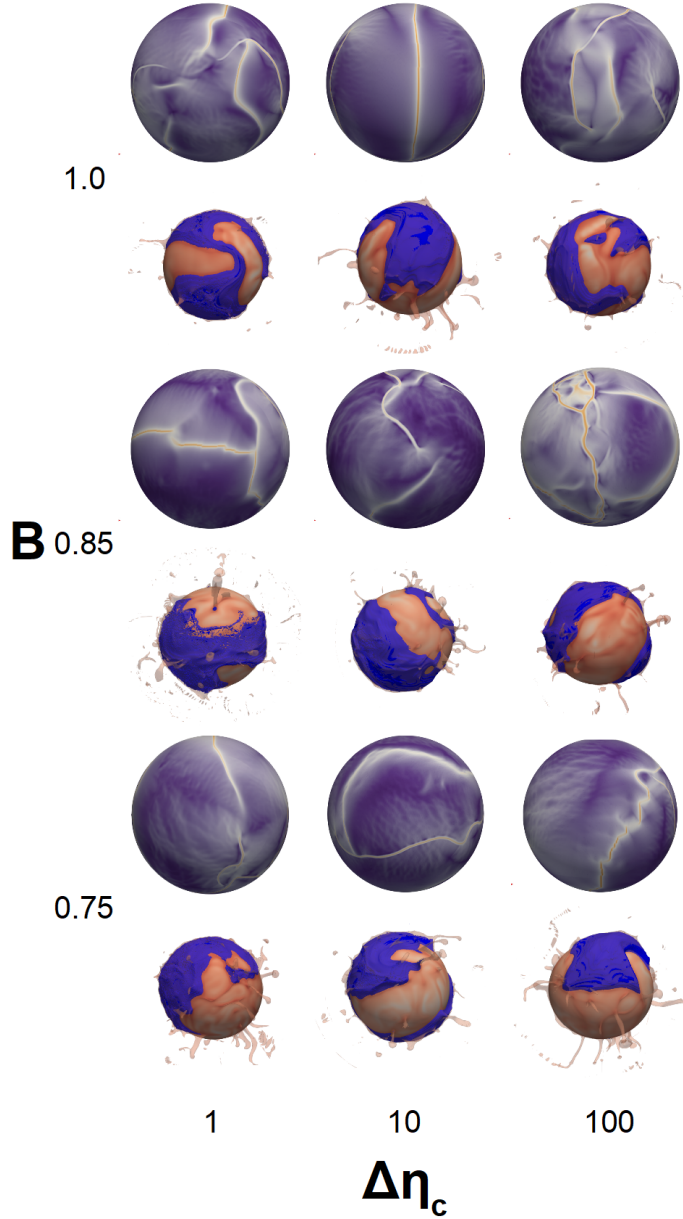


Figure 7. Snapshots from the nine uniform yield stress 3D cases featured in this study. The buoyancy number and intrinsic viscosity contrast for the CAID material and ambient mantle are indicated at the left and bottom of the figure, respectively. For each case, the viscosity field is shown at a depth of $0.005d$ juxtaposed with a (to scale) image of the mantle interior illustrating CAID material distribution (in blue) and thermal plumes (transparent red, non-dimensional temperature of 0.82). (The viewing angle of the viscosity field and model interior are the same.) The temperature power spectra corresponding to each snapshot is presented in Supplementary Fig. 3.

543 the CAID material, a large amount of heat is trapped in the dense provinces so that thermal
 544 power spectra indicate the nature of the intrinsically dense material's distribution. As with
 545 the power spectra at the surface, predominantly degree-one to -two power is observed,
 546 indicating that the CAID material is typically grouped into a single large pile but that a
 547 capacity for distribution into two piles exists. Cases featuring a buoyancy number of 1.0
 548 display power in harmonics as high as degree 3 (and 4), most likely because those cases
 549 exhibit a higher occurrence of shorter, localized, near-surface, deformation zones that (2D
 550 results indicated) are capable of promoting small isolated piles (e.g., Model 3DB1.0D100)
 551 or simply more discontinuity of the CAID layer. We note that the locations associated with
 552 surface weakening are not clearly imprinted on the underlying CMB by an absence of CAID
 553 material. This suggests that the migration of lithospheric weak zones may be at least as fast
 554 as the rate of arrival of sinking material at the CMB. However, as in the two-dimensional
 555 systems analyzed, we find that the arrival of downwellings at the CMB pushes aside CAID
 556 material so that its distribution is largely influenced by plate convergence. The results of
 557 the three-dimensional cases indicate that an apparent influence of the feedback between the
 558 plate boundary distribution and CAID material placement is the similar focus in low degree
 559 powers. Model 3DB1.0D10 is one of the two cases shown that features its strongest power
 560 at the surface in the degree two signature. It is examined in detail in section 3.7.3.

561 *3.7.2 Transience in the heat flux*

562 Figure 8 displays heat flux time series for the three cases appearing in Figure 7 featuring
 563 a buoyancy number of 0.75. We find no clear impact on the trend of the CMB heat flux values
 564 or their temporal variation for the range of intrinsic compositionally originating viscosity
 565 contrasts examined. As in the 2D calculations employing the same parameters (Figure 3),
 566 the surface heat flux is highly time-dependent, however, it shows less variation in the 3D
 567 calculations (e.g., when comparing the ratios of maximum to minimum value). In the two-
 568 dimensional cases, roughly 100% increases in surface heat flux are possible while the largest
 569 swing in heat flux in the 3D cases is closer to 50%. Consistent with the 2D results of Figure
 570 3 we observe that spikes in heat flux are associated with the initiation of new downwellings.
 571 The 3D downwellings are structurally more complicated than the 2D downwellings but a
 572 greater degree of freedom is present in fully spherical environments. Thus, smoother and less
 573 dramatic variations in amplitude occur between periods of low heat flux and high heat flux
 574 because surface velocities do not need to slow when plates change direction. For example,

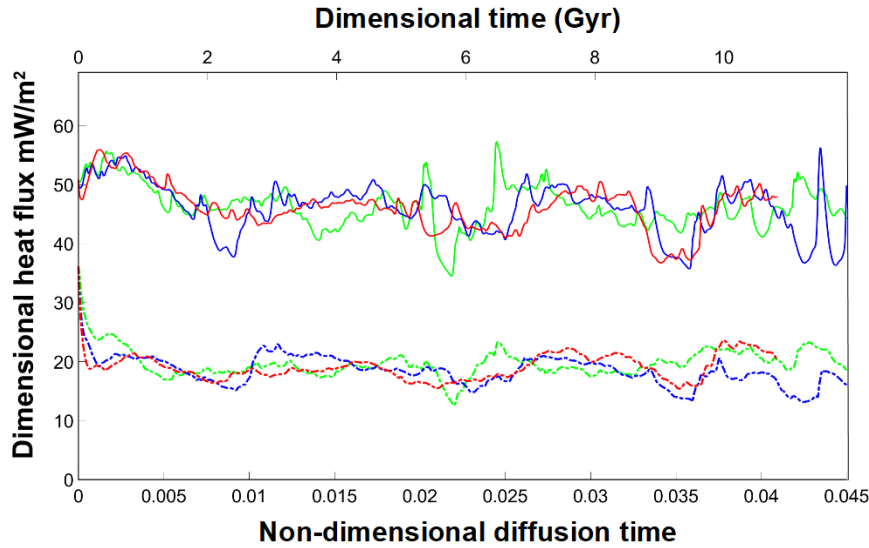


Figure 8. Surface and basal heat flux time series for the three 3D cases with uniform yield stress featuring a buoyancy number of 0.75. Green, blue and red correspond to cases where $\Delta\eta_C$ equals 1, 10 and 100, respectively. The time series illustrate surface and basal heat flux values using solid and dashed lines, respectively.

575 in a 2D model, if one convergent boundary closes while another emerges, plate directions
 576 can reverse and velocity briefly drops to zero. However, in 3D, changes in plate direction do
 577 not require a reduction in the global surface velocity and the initiation of new subduction
 578 zones is less impactful on surface heat flux. A notable difference between the 2D and 3D
 579 calculations is that the variation in heat flux was reduced when $\Delta\eta_C = 1$ in 2D cases, which
 580 was attributed to the prevailing degree-2 flow in this case, versus a degree-1 trend in the
 581 other cases. In the 3D cases, we do not observe such a trend in heat flux or a clear contrast
 582 in the power spectra harmonics, we attribute this to the added degree of freedom of the
 583 3D systems that removes the discretized contrast between degree-1 and degree-2 flow. One
 584 similarity between the two-dimensional and three-dimensional models is that increases in
 585 surface heat flux typically correspond to an increase in heat flux at the CMB.

586 Figure 9 presents heat flux time series for the three cases shown in Figure 7 featuring
 587 $\Delta\eta_C=100$ (n.b., Model 3DB0.75D100 (red) appears in both figures). In contrast to the three
 588 cases in Figure 8 with a common buoyancy number, these heat flux profiles show a trend.

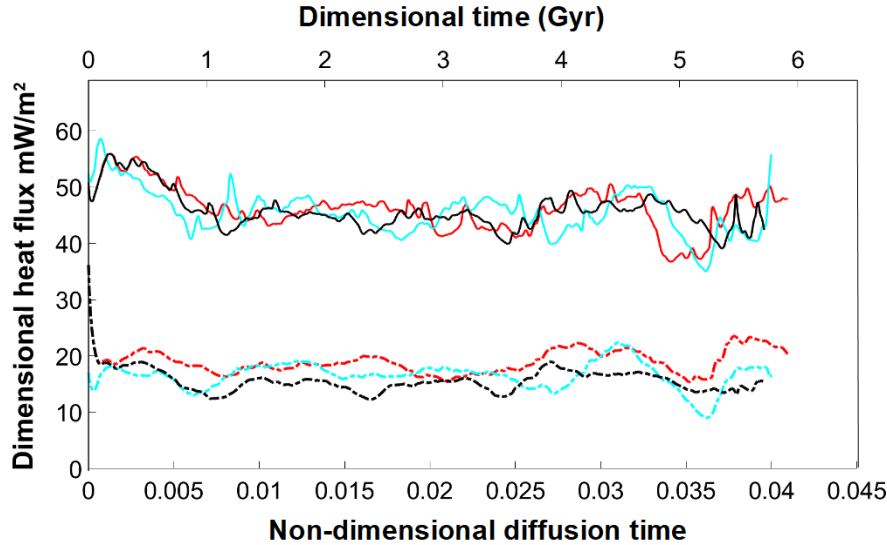


Figure 9. Surface and basal heat flux time series for the three 3D cases with uniform yield stress, featuring CAID material with an intrinsic viscosity that is 100 times greater than the ambient mantle. Red, cyan and black correspond to cases where $B = 0.75, 0.85$ and 1.0 , respectively. The time series illustrate surface and basal heat flux values using solid and dashed lines, respectively.

589 The heat flux diminishes as the buoyancy ratio is increased (this can be seen most clearly in
 590 the basal heat flux times series). Furthermore, for a corresponding CAID material viscosity
 591 the buoyancy number 0.75 cases are hotter in 3D calculations. The transience of surface
 592 and basal heat flux is again observed but the transition from periods of low heat flux to
 593 high heat flux occurs over longer periods and the range of minimum and maximum heat flux
 594 values is narrower than in the analogous 2D cases. The basal heat flux trend agrees with
 595 the findings of the 2D calculations which demonstrated that an increased buoyancy number
 596 can result in greater insulation of the CMB.

597 *3.7.3 Evolution of the plate boundaries and CAID material distribution*

598 We now examine the detailed time-dependence of one of the cases from Figure 7. The
 599 time-averaged power spectrum for the temperature field of Model 3DB0.75D10 showed a
 600 peak in lower mantle power at degree 2. A period of 1 Gyr of evolution (ending at the time

601 shown in Figure 7) is analyzed here in order to determine whether this spectral peak ever
 602 corresponds to two distinct provinces.

603 Figure 10 displays six sequential snapshots of the near surface viscosity field as well
 604 as isosurfaces that reveal plumes (red, non-dimensional temperature of 0.82) and CAID
 605 material distribution (blue) for Model 3DB0.75D10. Each row shows an instant in time as
 606 viewed from diametrically opposed positions. Additional viewing angles are presented in
 607 Supplementary Figure 4. The viscosity field shows the evolution of features such as narrow
 608 weak bands (corresponding to convergence and divergence) that bound the low strain-rate
 609 plate-like regions. In addition, at times 200 Myr and 400 Myr the viscosity fields display
 610 the formation, evolution and dissolution of transform-like offsets along spreading bound-
 611 aries. The feedback between surface features and the distribution of the CAID material is
 612 illustrated in the column marked 0° in Fig. 10, from times 600 Myr to 1 Gyr. The snapshot
 613 at time 600 Myr features CAID material that forms a great province extending from the
 614 northern to southern pole. At time 800 Myr the previously discontinuous convergent bands
 615 in the left and right hemispheres (roughly coincident with the equatorial region in the figure)
 616 have merged, forming a triple junction with a spreading boundary located in the southern
 617 hemisphere. The merging of the convergent boundaries has led to the development of a
 618 sheet-like downwelling that plunges into the deep mantle and impacts the CAID material
 619 below, pushing aside the dense material. Accordingly, the north-to-south pole extending
 620 province becomes split into a north and south fragment. In general, large voids are present
 621 in the CAID material below convergent surface features. Conversely, spreading boundaries
 622 incorporating transform offsets are most typically found over regions of the CMB covered by
 623 CAID material. This characteristic mimics the behaviour observed in the two-dimensional
 624 cases.

625 We note that in this calculation, the movement and repositioning of the CAID mate-
 626 rial's periphery on the CMB occurs on the same time scale as the motion of the plate bound-
 627 aries. Accordingly, plumes anchored at the peripheries of the CAID provinces migrate at
 628 similar rates. Some plumes form on top of the CAID material piles, below divergent surface
 629 features, but they lack the vigour needed to penetrate into the upper mantle.

630 In Supplementary Figure 5 we present Mollweide projections of the compositional field
 631 145 km above the CMB for each of the times corresponding to Fig. 10. Given the full 360°
 632 view of the CAID material shown in Supplementary Fig. 5 a brief period of two province

633 formation is revealed at 0 Myr. However, unlike Earth’s LLSVPs, the separation of the
 634 provinces is relatively small. Moreover, it does not persist. This period marks the only time
 635 we observe the formation of two provinces. The distribution of the CAID material in this
 636 epoch apparently produced the degree-2 signature in the time averaged power spectrum of
 637 the model’s thermal field.

638 Given the evidence that downwellings drive the formation of regions on the CMB that
 639 are void of CAID material, we explored the dependence of the distribution of the CAID
 640 material on downwellings by reducing the surface yield stress to allow for a greater number
 641 of convergent bands in the model lithosphere. Model 3DB0.75D100weak is similar to Model
 642 3DB0.75D100 except that it employs the weaker yield stress model described in section 3.6
 643 and initializes by placing a CAID layer in the thermal field shown in Fig. 6b. The yield
 644 stress increases with depth over the top 2% of the mantle from a non-dimensional surface
 645 value of 1×10^7 to a uniform yield stress of 2×10^7 at all lower depths.

646 Figure 11 presents a series of snapshots for Model 3DB0.75D100weak. The viscosity
 647 field snapshots exhibit the increased number of convergent and divergent surface bands
 648 resulting from the weakening of surface yield stress, leading to the development of a greater
 649 number of downwellings and individual plates. (However, with the weakened surface the
 650 calculation no longer exhibits the transform-like offsets punctuating divergent features.) The
 651 increased number of smaller scale downwellings leads to a greater number of voids within
 652 the layer of CAID material. For example, multiple voids are observed in the column marked
 653 0° at time 540 Myr in Fig. 11; column B at time 900 Myr of Supplementary Figure 6;
 654 and column D times 360 to 720 Myr (also Supplementary Figure 6); varying in size and
 655 number. Accordingly, the CAID material tends to form a greater number of narrow tendril-
 656 like features joining the piles on the CMB, as exhibited in the columns marked 0° of Fig.
 657 11 and 90° (B) in Supplementary Figure 6.

658 Supplementary Figure 7 shows the compositional field 145 km above the CMB at the
 659 times presented in Figure 11 and illustrates the growth and movement of voids in the dense
 660 layer rather than coalescing of the dense material into piles. The formation of numerous
 661 connecting branches between larger nodes occasionally allows for the isolation of a fraction
 662 of the CAID material into small, short-lived piles. This is exhibited in the 0° column at
 663 times 540 to 900 Myr, where a small pile is loosely connected to the greater mass of CAID
 664 material by narrow tendrils, briefly isolated (e.g., at 720 Myr in Supplementary Figure 7)

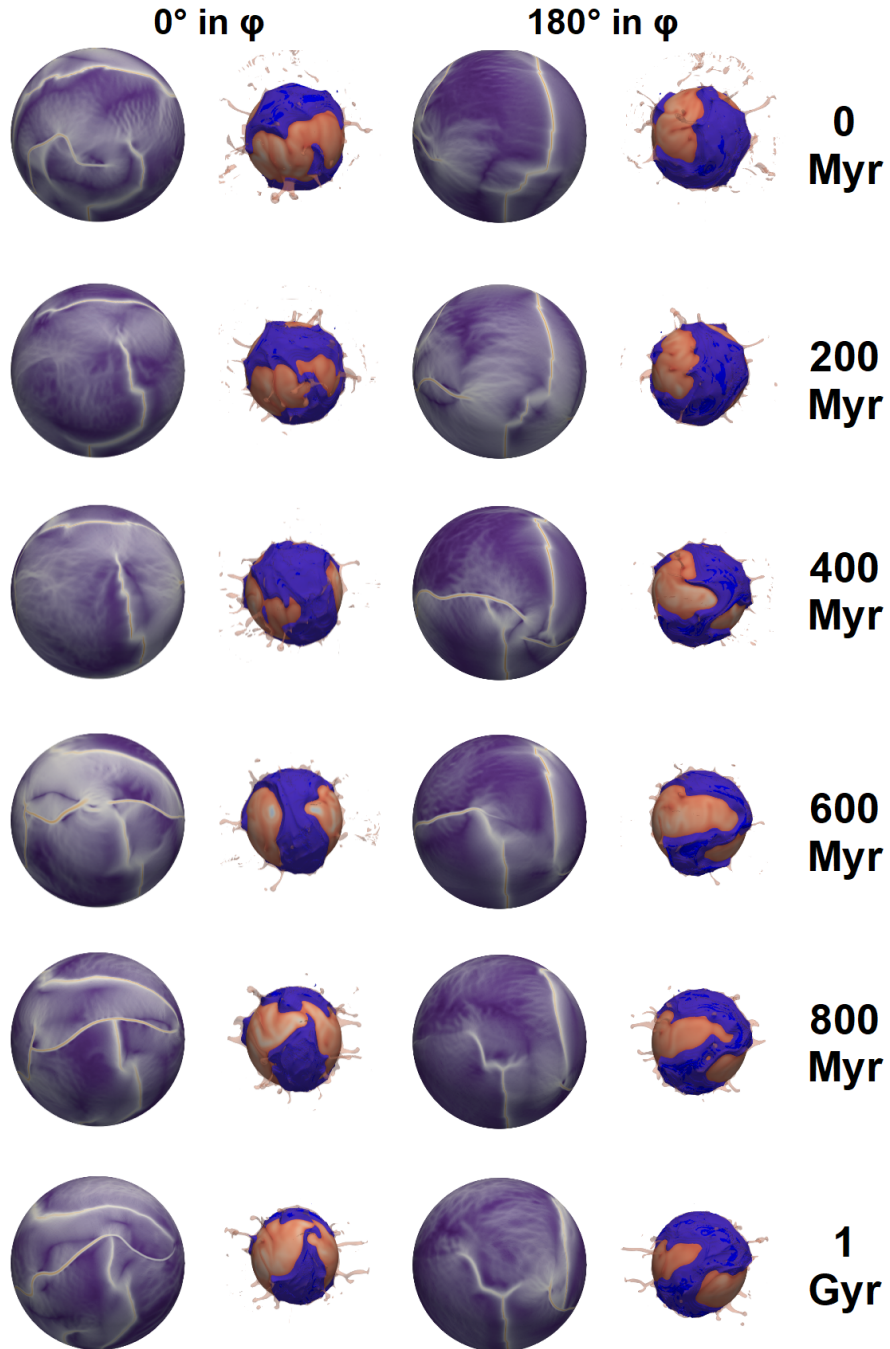


Figure 10. Snapshots of the near surface viscosity field and CAID material distribution at six different times (rows) throughout the evolution of Model 3DB0.75D10. Diametrically opposed viewing angles are presented for each time, with the angle of rotation relative to a vertical axis through the centre of the sphere in the left-most column indicated at the top of the second column. Additional viewing angles are presented in Supplementary Figure 6.

665 and then rejoined to the larger pile through another narrow tendril. The weakening of the
 666 surface yield stress thus leads to the formation of a greater number of small scale features
 667 at the surface (including downwellings) and a CAID distribution on the CMB that might
 668 be described as ‘fragments connected to a large province incorporating voids’. However,
 669 aggregation into two similar volume provinces is not obtained during the more than 1 Gyr
 670 modelled.

671 Figure 12 shows thermal power spectra as a function of height above the CMB for
 672 the model presented in Figure 11. Although the distribution of the CAID material during
 673 this period appears unchanged from a qualitative perspective, the thermal power spectra
 674 indicate a field dominated by degree-2 above the CMB has transitioned to a field with a
 675 degree-1 signature, in addition to lesser power distributed as high as degree-6. Given their
 676 hot signatures we infer that periods dominated by degree-2 CAID material distribution
 677 occur, but detection of such a period is not an indicator of a pair of detached provinces.

678 To explore the possibility that the critical issue inhibiting the formation of two dis-
 679 tinct provinces in our calculations is the specification of an excessive volume of the CAID
 680 material, we examined a final case incorporating a reduction in the volume of the intrin-
 681 sically dense component. Model 3DB0.75D100weak&reduced employs identical parameters
 682 and initial condition to Model 3DB0.75D100weak but the CAID component incorporated in
 683 the calculation comprises only 2% of the mantle volume. Figure 13 shows the evolution of
 684 Model 3DB0.75D100weak&reduced by presenting the divergence field and temperature field
 685 power spectra as a function of height above the CMB. The corresponding evolution of the
 686 near surface viscosity field and thermal power spectra is presented in Supplementary Figure
 687 9. The corresponding evolution of the dense layer is shown in Supplementary Figure 10. As
 688 in the other calculations presented, at time 0.0 Myr the mean temperature of the model has
 689 equilibrated following the incorporation of the CAID layer into the initial condition thermal
 690 field (Fig. 6b) and subsequent forward modelling. Although the reduction in the volume of
 691 the CAID component does not result in a pair of distinct provinces during the evolution of
 692 this case, the introduction of the denser material does have a global impact on temperature
 693 that results in the formation of a greater number of distinct plates and triple junctions than
 694 in either the isochemical initial condition models or the previously described case (Model
 695 3DB0.75D100weak) featuring a higher volume of CAID material. Moreover, the divergent
 696 boundaries exhibit multiple examples of transform-like offsets (e.g., the boundary extending
 697 ‘north-south’ in the column marked 180°). The influence of a CAID mantle component on

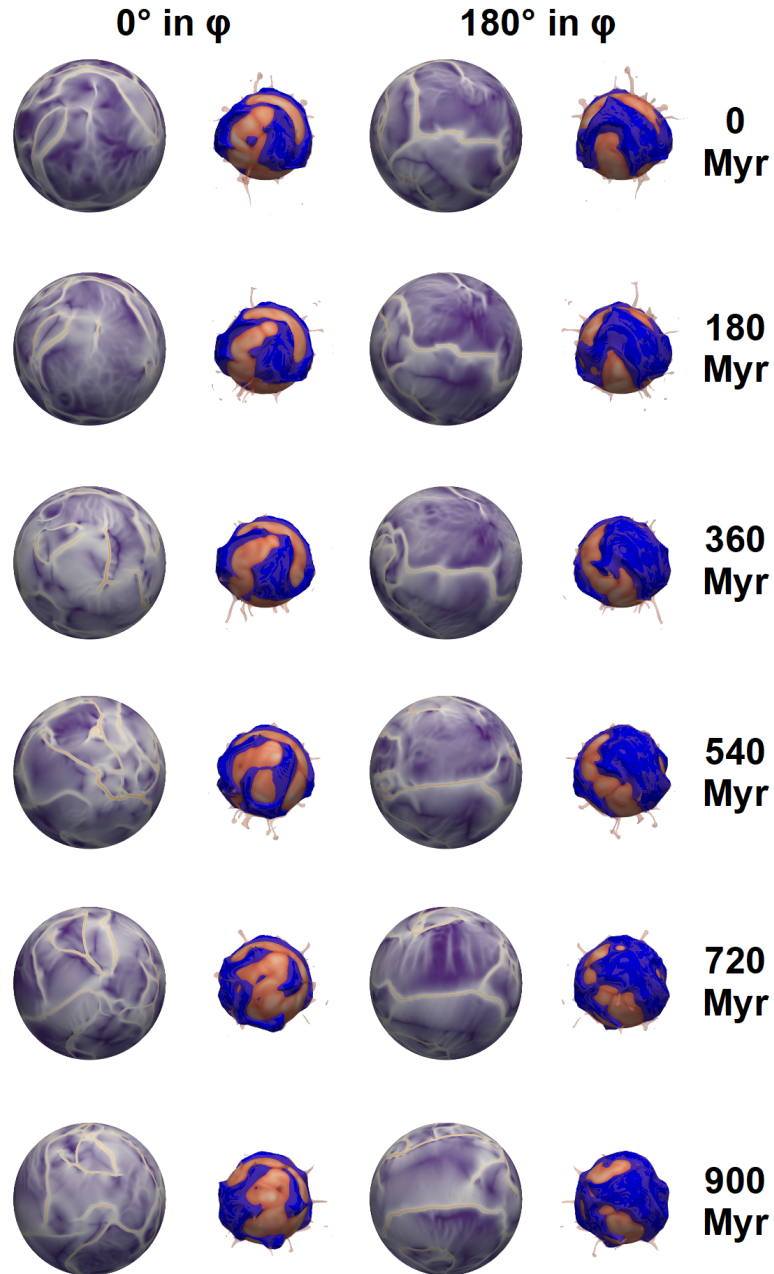


Figure 11. Snapshots of the near surface viscosity field and CAID material distribution at six different times (rows) throughout the evolution of Model 3DB0.75D100weak. Diametrically opposed viewing angles are shown for each time with the angle of rotation relative to the left-most column indicated at the top of the columns. Supplementary Figure 6 presents additional viewing angles of the viscosity field and CAID material distribution at the same times.

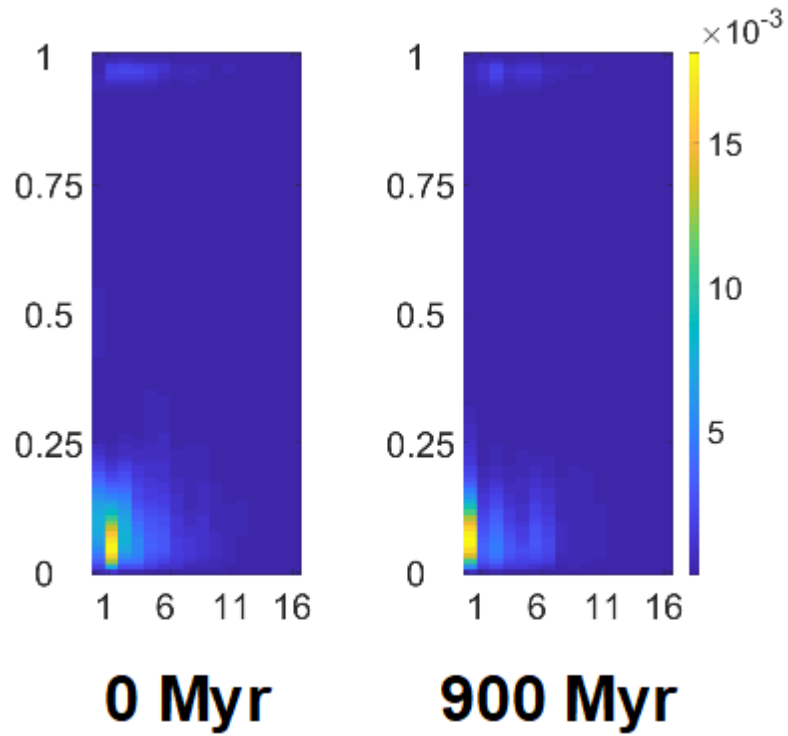


Figure 12. Thermal field power spectra as a function of height above the CMB for the case presented in the previous figure. The timing of the spectra presented corresponds to the first and final frames shown above.

698 the formation of plates is illustrated by the impact of plates and dense provinces on the
 699 temperature field of the systems examined.

700 Figure 14a depicts temperature profiles taken from the initial condition models in
 701 Fig. 6 (red and cyan curves) as well as time-averaged profiles from the cases presented in
 702 Figs. 10, 11 and 13 (magenta, green and blue, respectively) and shows the impact on global
 703 temperature of both a weakened lithospheric yield stress and the presence of a hot CAID
 704 component sitting on the CMB; specifically the insulation of the mantle from core heat flow
 705 that emplacement of this component engenders. The influence of a lower lithospheric yield
 706 stress is revealed by comparing the red and cyan curves, which show the substantial cooling
 707 resulting from a greater number of downwelling sheets that form with a lowered yield stress.
 708 With the addition of the CAID material, temperature increases in the lowest 15-20% of the
 709 mantle relative to the isochemical cases. The increased temperature extends to a smaller
 710 height above the CMB in the case where the volume of the intrinsically dense material is
 711 reduced (blue curve). In all cases featuring a CAID component, the mantle above the deep
 712 layer incorporating the CAID component is cooler than in the corresponding isochemical
 713 case because the denser material sitting on the core reduces heat flow into the mantle. The
 714 degree of mid-mantle cooling is clearly determined by the volume of the CAID material. This
 715 is illustrated by comparing the green and blue curves: the lower volume of CAID material in
 716 Model 3DB0.75D100weak&reduced (blue) results in a warmer mantle in that case, relative
 717 to that of Model 3DB0.75D100weak (green), above the depths that incorporate the CAID
 718 material. (At the same time, the blue curve is cooler than the magenta because the model
 719 producing the latter has a weaker surface and allows for a longer network of interior-cooling
 720 (convergent) plate boundaries.) However, the blue curve (2% CAID material) is hotter than
 721 the cyan (no CAID material) in the upper mantle and the cyan curve is just mildly warmer
 722 than the green (3% CAID material). This departure from the other systematic trends is a
 723 manifestation of what is effectively a regime change in the lithospheric character. The cyan
 724 curve (the initial condition model with a weaker lithospheric yield stress) corresponds to a
 725 case with a mobile surface but less distinct plates and boundaries than in the uniform yield
 726 stress cases. Adding the 2% CAID component to the mantle has affected global flow so that
 727 a cooler mid-mantle and hotter upper mantle evolves. The result is conducive to producing
 728 more clearly defined plates isolated by tightly focussed boundaries.

729 Figure 14b shows the viscosity profiles corresponding to the temperature profiles in
 730 14a, emphasizing that the heat trapped in the CAID material counteracts the high intrinsic

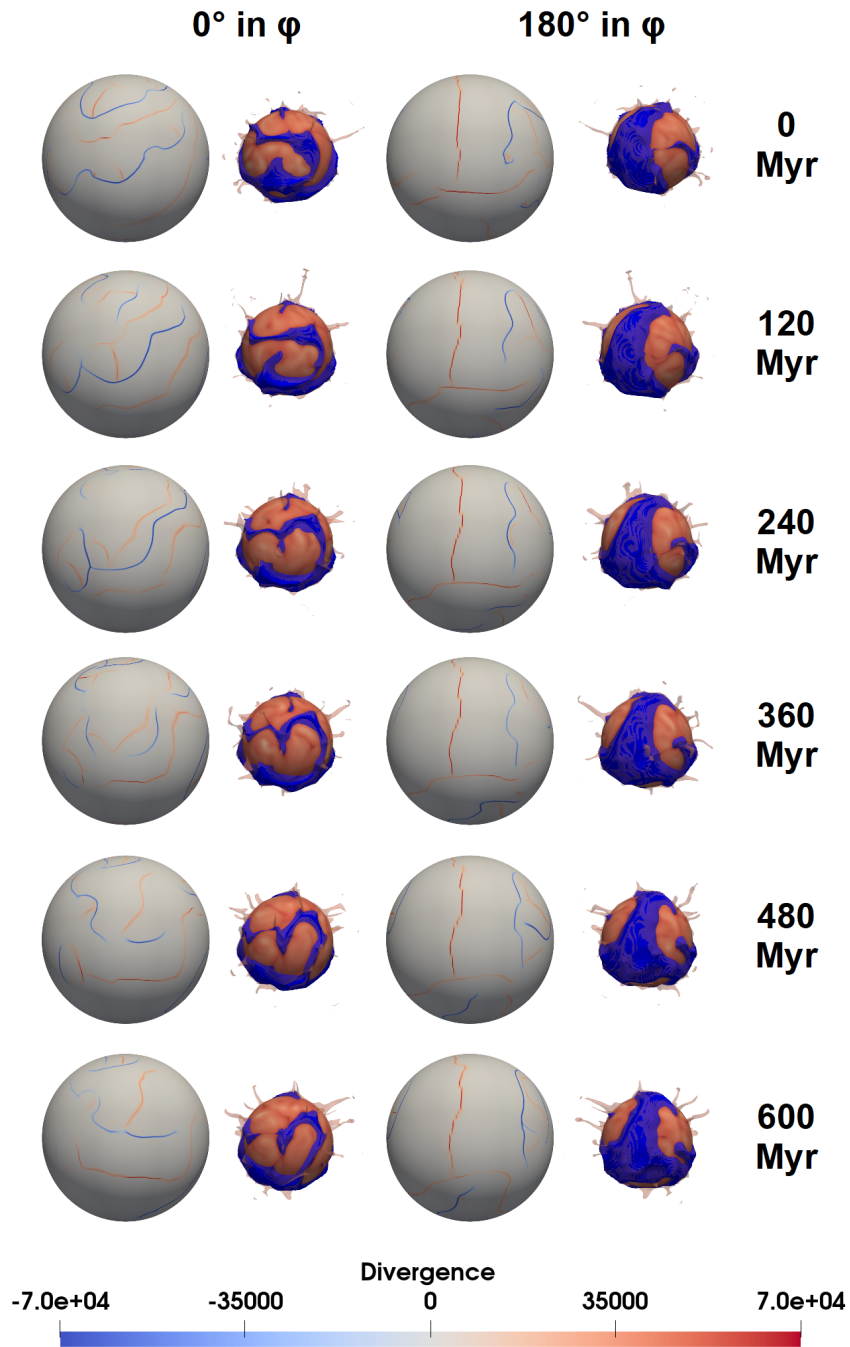


Figure 13. Snapshots of the near surface non-dimensional velocity divergence field and CAID material distribution at six different times (rows) throughout the evolution of Model 3DB0.75D100weak&reduced. Diametrically opposed viewing angles are shown for each time with the angle of rotation relative to the left most column indicated at the top of each column. Additional viewing angles are shown in Supplementary Figure 8.

731 viscosity of the dense components to such a degree that the isochemical cases exhibit the
 732 highest mean viscosity in the region between the deepest five and fifteen percent of the
 733 mantle. The viscosity profiles also show the impact of robust deep penetrating slabs. For
 734 example, although hotter at mid-mantle than Model 3DB0.75D100weak, the viscosity profile
 735 from the initial condition case with a depth-dependent yield stress shows a higher averaged
 736 viscosity. The high mean viscosity is explained by the incorporation of numerous very high
 737 viscosity downwellings into the averaging. The exponential law for the viscosity has a large
 738 impact on averaging where slabs are present while slabs have a relatively smaller impact on
 739 mean temperature at a given height. This effect also produces small scale gradient variation
 740 in the viscosity profiles relative to the smoother temperature profiles, particularly in the
 741 isochemical (initial condition) cases.

742 Previous authors (e.g., Stein et al., 2004; Stein & Hansen, 2008; Höink et al., 2012;
 743 Lenardic et al., 2019) have described the critical role of mid-mantle temperatures and vis-
 744 cosity increase with depth on the generation and sustained mobility of plates. The findings
 745 presented here illustrate that the presence of a compositionally anomalous and intrinsically
 746 dense mantle component can impact the mid-mantle temperature profile in a way that in-
 747 fluences the global viscosity profile and therefore plate formation and mobility. Finally,
 748 lowered lithospheric yield stress and a greater volume of CAID material cool the mantle
 749 overall. However, as described above, the intrinsically dense mantle component becomes
 750 particularly hot. The combined affects of its temperature and intrinsic density result in a
 751 much more marginal increase in the density of the CAID component than is implied by the
 752 buoyancy numbers. We discuss this further below.

753 4 Discussion

754 Although the origin and physical characteristics of the LLSVPs are contentious, with
 755 the exception of secondary details there is broad agreement on the physical bounds and
 756 seismic properties of the regions of the mantle that define the locations of the provinces
 757 (e.g., Cottaar & Lekic, 2016). Specifically, whatever the cause of the seismic signature, the
 758 vast majority of the volume of the mantle satisfying classification as LLSVP is divided into
 759 a pair of detached features. The distribution of a chemically distinct volume of the mantle
 760 into two distinct features blanketing approximately 30 percent of the CMB while rising
 761 over 1000 km above the CMB (Garnero et al., 2016) provides key constraints on efforts
 762 to determine the physical properties of the compositionally anomalous material assumed

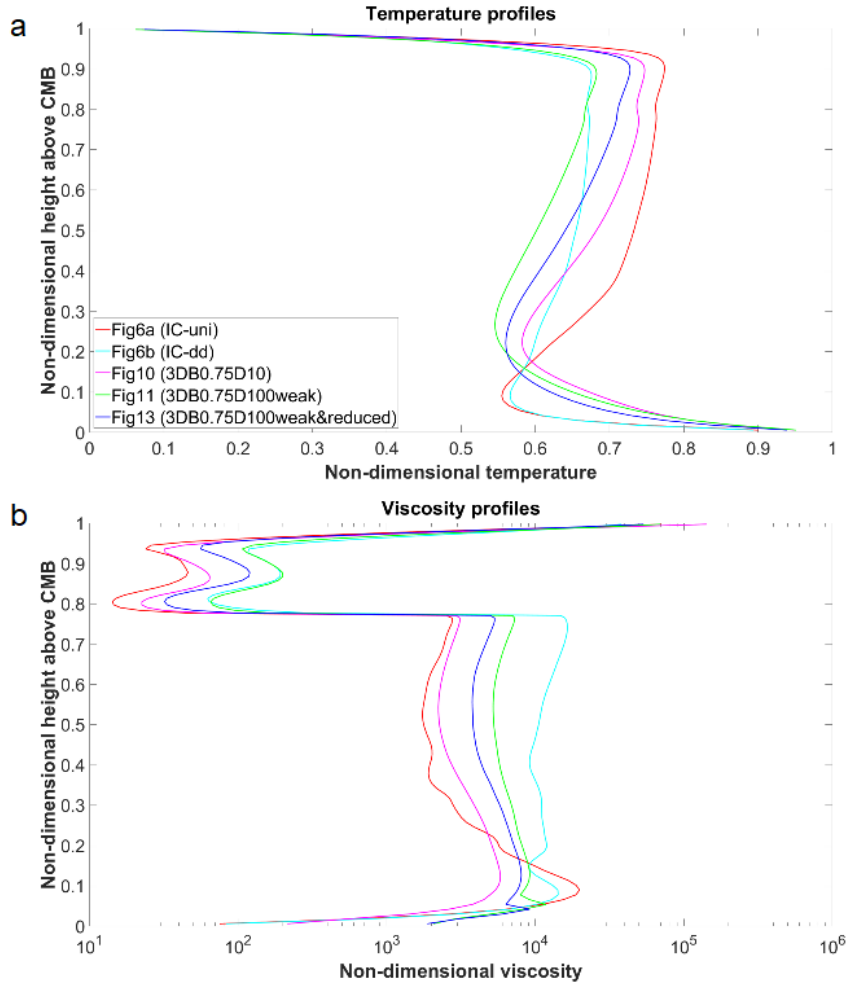


Figure 14. Temporally averaged profiles of the latitudinally and longitudinally averaged temperature (a) and viscosity (b) as a function of height above the core mantle boundary in five of the 3D geometry cases featured in this study. The red curve corresponds to the isochemical initial condition model with a uniform yield stress; the cyan curve corresponds to the isochemical case with the depth-dependent yield stress; the magenta, green and blue curves correspond to Models 3DB0.75D10, 3DB0.75D100weak and 3DB0.75D100weak&reduced, respectively.

763 responsible for the observation of LLSVPs. Obtaining two detached provinces comprised
 764 of such material is not a default distribution of the inclusion of such a component in a
 765 3D spherical shell. In contrast, recovering a pair of large provinces is not as an elusive
 766 outcome in two-dimensional models, including the spherical annuli modelled in the first part
 767 of this study. We suggest that the challenge of identifying the physical properties of the
 768 CAID material that yields LLSVP-type distributions in 3D shells is somewhat analogous
 769 to identifying the properties of a fluid mantle that yield sheet-like downwellings. (Two-
 770 dimensional calculations with mobile surfaces always produce this desired behaviour, but
 771 obtaining slab-like downwelling morphology in 3D spheres is limited to a set of systems with
 772 very specific material parameters, initial conditions and shell thicknesses.)

773 A deficiency of the 3D models that is mostly likely explained by the absence of discrete
 774 CAID provinces and a core largely free of coverage by the dense component, is the
 775 scarcity of vigorous plumes, capable of transiting the entire depth of the mantle. Given
 776 the inferred association of plume generated igneous provinces with chemically originating
 777 LLSVPs (Torsvik et al., 2006; Burke et al., 2008; Li & Zhong, 2017; Heyn et al., 2020),
 778 the relatively small number of plumes is counter to the expectation of observing PGZs.
 779 However, this result is consistent with the observed broad coverage of the CMB by CAID
 780 material. Plume generation zones have been inferred to form at the boundaries of relatively
 781 small footprint provinces, where thermal gradients can generate plumes. Adjacent to the
 782 provinces are broad expanses of the CMB where high heat flow can be drawn into the man-
 783 tle and advected towards province boundaries. In the 3D cases presented here, the CAID
 784 material forms expansive punctured layers with voids that may be too small to draw enough
 785 heat from the CMB to allow the formation of robust plumes. In contrast, Langemeyer et
 786 al. (2021) found examples of several vigorous plumes transiting the mantle in an isochemi-
 787 cal model employing the same parameter values as the 110 MPa uniform yield stress cases
 788 presented here. The generally reduced heat flux (and therefore support for plumes) at the
 789 CMB, found when CAID material is added to the calculations, is illustrated in Figs. 8
 790 and 9. The contribution to surface heat flow from the core, indicated by the time series in
 791 these figures, is in the 10-15% range. This is at the lowest end of widely accepted estimates
 792 of CMB heat flow (e.g., Lay et al., 2008). Figure 14 shows that a strong sub-adiabatic
 793 temperature profile exists in several models due to slabs pooling in the deep mantle. A sub-
 794 adiabatic temperature profile will also decrease the temperature anomaly that characterizes
 795 rising plumes.

796 Overall, our findings do agree with previous studies. By assuming that the origin of
 797 the LLSVPs is explained by a chemically distinct lower mantle component, we conclude
 798 that the buoyancy ratio of this material (relative to the ambient mantle) as well as an
 799 inherent viscosity contrast between the intrinsically dense component and remaining mantle
 800 material, both impact the distribution, durability and mobility of the CAID component.
 801 For example, when all other system parameters are held constant, increasing the intrinsic
 802 viscosity of the denser mantle component tends to result in degree-1 flow, in contrast to
 803 the degree-2 structure more readily obtained in the isochemical or chemically enriched cases
 804 where $\Delta\eta_C = 1$.

805 We have excluded the influence of compressibility in our calculations but do not expect
 806 this omission to impact the overall dynamics of the systems described given the scale height
 807 of the mantle (of order 10^7 m.). Nevertheless, compressibility is responsible for decreasing
 808 thermal expansivity in the lower mantle. Accordingly, in estimating the total density
 809 anomalies occurring in the CAID provinces in these calculations, due to both chemical and
 810 thermal affects, an adjustment of the mean thermal expansion coefficient value given in
 811 Table 1 is necessary.

812 For the range of buoyancy numbers considered (0.75, 0.85 and 1.0), the dimensional
 813 increase in the density of the enriched mantle component is 138.75 kg/m^3 , 157.25 kg/m^3
 814 and 185 kg/m^3 , respectively, for a comparison of surface temperature materials (equating
 815 with density increases of 3.75%, 4.25% and 5%). However, these contrasts must be adjusted
 816 when temperature contrast between the CAID and ambient mantle material is considered.
 817 Moreover, in the lowermost mantle, the thermal expansion coefficient may be up to 50%
 818 lower than its upper mantle value. As illustrated in Fig. 2, the dense provinces are typically
 819 1000-1250 K (0.4 to $0.5\Delta T$) hotter than the ambient mantle, so that thermal influence, com-
 820 bined with a reduction in the thermal expansion coefficient, reduces their density contrast
 821 when compared to the ambient mantle (assuming a thermal expansion coefficient of 1×10^{-5}
 822 K^{-1} and an ambient mantle nondimensional temperature of 0.5). Accordingly, the CAID
 823 material provinces modelled are thus approximately 0.625% to 1.5% more dense than the
 824 adjacent mantle at the same depth. Actual density anomalies associated with the LLSVPs
 825 remain an issue of debate (e.g., McNamara, 2019), but may be encompassed within this
 826 range. However, in these models, the primary factor that determines the choice of the in-
 827 trinsic density contrast between the enriched and ambient mantle components is ultimately
 828 the requirement of the durability of the denser volume of the two-component system. For

829 models in which the denser component is not replenished, such as in this study, the spec-
830 ification of a buoyancy number below 0.7 results in entrainment and mixing of the dense
831 layer given vigorous convection persisting over time periods of a few billion years. Our
832 calculations (and the implied minimum and maximum density anomaly they yield between
833 the ambient mantle and chemically distinct regions) result in a density anomaly estimate
834 that is consistent with that inferred from seismic observations (Trampert et al. 2004).

835 Our study imposed the requirement that plate-like surface motion should be exhibited
836 for calculations producing LLSVP-type piles on the CMB, if model outcome is to be con-
837 sidered applicable to understanding the feedback between surface dynamics and the Earth's
838 deep interior. This requirement is especially important because plate-like surface behaviour
839 produces strong focussed downwellings in the mantle (slabs) and these features have the
840 greatest impact on the distribution and mobility of the CAID material (e.g., McNamara
841 & Zhong, 2005; Zhang et al., 2010). However, the simultaneous modelling of dynamically
842 evolving plates and thermochemical piles increases the number of variables in the system
843 so that the cases presented here comprise coverage of a small fraction of the possible cases
844 that may be relevant to Earth's evolution. Despite this, some specific behaviour appears
845 to be general. A small number of thermochemical piles are not readily obtained in the 3D
846 calculations. Instead, downwelling sheets penetrate CAID material layers to produce a dis-
847 tribution better described as a layer punctuated by multiple holes. Decreasing the volume
848 of the CAID material tends to reduce the mean thickness of the layer featuring the holes
849 rather than prompting the separation of the dense material into piles. Moreover, decreasing
850 the volume of the dense component is contrary to non-consensus estimates of the volume
851 of the LLSVPs which are as great as eight percent of the mantle's volume (Cottaar & Le-
852 kic, 2016). As described by numerous other authors, decreasing the buoyancy number of
853 the denser component can allow for the formation of higher topography, reduced 'footprint'
854 piles, but this occurs at the expense of pile durability. In the models we present, which as-
855 sume a primordial, non-renewing, CAID component, a lower buoyancy number is conducive
856 to mixing and dissipation of the dense component (e.g., Trim et al., 2020). Possible future
857 avenues for investigation that may reconcile the existence of two thermochemical piles in
858 a spherical shell exhibiting plate tectonics may require the modelling of a renewing source
859 lower buoyancy number material for the CAID component than was consider in this study.
860 However, this may be problematic (Brandenburg & van Keken, 2007; Li & McNamara, 2013)
861 rather than offering a solution. Nakagawa et al. (2010) and Nakagawa & Tackley (2011)

862 employed sophisticated three-dimensional spherical models in which the dense material was
863 produced by melting but also did not obtain two piles in the systems studied.

864 In contrast, studies that have imposed plate velocity on 3D spherical shells have read-
865 ily obtained two LLSVP-like features for anomalously dense mantle components similar in
866 volume, relative density and viscosity to those investigated here. The difference in our find-
867 ings and those of investigations that imposed recent plate motion history (e.g., McNamara
868 & Zhong, 2005; Zhang et al., 2010) may result from a lack of feedback in the former studies
869 but could also stem from the neglect of continents in the work presented here. The breakup
870 of a supercontinent might impact the number of piles obtained in the deep mantle. For
871 example, dispersing continents (or the process of supercontinent breakup) may play a role
872 in organizing subduction in a way that results in a dominant degree-2 convection pattern
873 that simultaneously promotes two thermochemical provinces (e.g., Li & Zhong, 2009; Li &
874 Zhong, 2017). However, exploring the feedback between a CAID component, continents and
875 the modelling of dynamic oceanic plates remains a computational challenge in 3D systems
876 with Earth-like convective vigour so that studies will be strongly limited by the number of
877 variables that can be investigated.

878 Despite the difficulty of obtaining two LLSVP-like provinces from the addition of a
879 CAID component to a 3D model, two-dimensional components not only readily produce
880 two distinct piles but can also emulate some of the other seismically inferred morphology.
881 For example, at time 1.58 Gyr in Fig. 5, the calculation featuring a buoyancy number of
882 0.75 exhibits one province that rises approximately 1000 km above the CMB while the other
883 province is just half that height. Together the provinces cover about 30% of the CMB. These
884 figures mimic the approximate dimensions of the LLSVPs determined by seismic studies,
885 including the greater volume and height of the African anomaly (e.g., Cottaar & Lekic,
886 2016). In general, the time-dependence of the CAID material features in the 2D calculations
887 take on a variety of shapes that can mimic cross-sections of LLSVP images. Specifically,
888 the intrinsically dense provinces are more likely to take on heights in excess of 1000 km
889 or more above the CMB when the buoyancy number is in the 0.75 - 0.85 range and the
890 intrinsic viscosity contrast between the enriched and surrounding material is much greater
891 than one. However, we note that we model a uniform distribution of internal heat sources.
892 For higher buoyancy number, enrichment of the CAID material with a greater degree of
893 internal heating (e.g., Li et al., 2019) could produce higher topography features than those
894 found in our study. Nevertheless, the findings presented from this study are cautionary, in

895 that they show that conclusions regarding the physical properties of the LLSVPs, inferred
 896 from the morphology of dense components in 2D thermochemical models do not always
 897 reproduce LLSVP-like features in 3D systems.

898 A similar issue exists with regard to modelling plates in the presence (or absence) of a
 899 two-component lower mantle. The modelling of plates affects system heat flow at both the
 900 upper and lower boundaries. Dramatically different system behaviour is therefore possible
 901 in models featuring the modelling of plates, when the heating conditions are identical. For
 902 example, the presence of a CAID component partially blanketing the CMB reduces heat
 903 flow into the mantle and therefore results in a cooler interior. The result of a cooler mantle
 904 is analogous to reducing the internal heating rate of the mantle, which has been shown in
 905 multiple studies employing plate modelling methods (e.g., Stein et al., 2014) to promote
 906 surface mobility. Similarly, the presence of a CAID component in the lower mantle can
 907 affect the formation of plate boundaries because of the impact of reduced mantle temper-
 908 ature on the tractions that break the model lithosphere. In addition, the two-dimensional
 909 calculations in our study showed not only that slabs could impact, deform and split CAID
 910 material provinces but that the provinces would instil convective patterns that would result
 911 in repeated failure of the lithosphere in the same narrow region. Thus, the modelling of
 912 plates and the inclusion of a CAID mantle component results in a feedback that appears to
 913 affect both CAID material distribution and plate boundary locations. A potential disrup-
 914 tion to the establishment of such feedback might be provided by the inclusion of continents
 915 in these models or the change in the limited degree of freedom for plate motion that ac-
 916 companies three-dimensionality. Accordingly, we conclude that the physical properties of
 917 a CAID mantle component that will promote the formation of a pair of distinct provinces
 918 may require the modelling of continents covering about 30% of the mantle’s surface.

919 **5 Conclusion**

920 Tectonic plate motion has been a corollary of terrestrial mantle convection (e.g.,
 921 Bercovici, 2003; Coltice et al., 2017; 2019; Crameri et al., 2019) for more than a billion
 922 years (Dhuime et al., 2015). Consequently, investigating the evolution of the current struc-
 923 ture of the deep interior with global-scale mantle convection calculations requires modelling
 924 a system yielding the primary aspects of plate tectonics: the existence of focussed sheet-
 925 like downwellings (slabs), persistent piece-wise uniform surface motion, and the presence of
 926 evolving plate boundaries. Previous work has shown that mantle convection models featur-

927 ing methods for reproducing or generating plate-like surface velocity fields (e.g., Monnereau
 928 & Quéré, 2001; Lowman et al., 2001; Lenardic et al., 2019) exhibit internal temperature
 929 structure (and therefore viscosity) that differs from systems with other surface behaviour.
 930 Principally, this effect is produced by the influence that plates have on mantle heat loss.
 931 The presence of chemically dense provinces lying on the core mantle boundary have been
 932 shown (Langemeyer et al., 2020) to inhibit heat flow into the mantle and therefore also
 933 affect mantle temperatures (and viscosity). Here we show that for modest volumes (2-3.5%
 934 of the mantle) the impact of incorporating a compositionally anomalous and intrinsically
 935 dense component in mantle convection calculations can change temperature profiles so that
 936 plate-like surface behaviour is obtained for different parameter values from those required
 937 for isochemical models.

938 Presenting results from eleven vigorously convecting 3D calculations, we also show
 939 that obtaining a pair of compositionally distinct provinces with LLSVP-like coverage of the
 940 CMB is elusive in systems featuring dynamically evolving plate-like surfaces. Not only does
 941 the presence of a CAID component in the mantle affect the surface velocity field character,
 942 but a pair of enduring provinces did not evolve in any of the cases that we considered. In
 943 contrast, two-dimensional systems exhibit a pair of diametrically opposed provinces for a
 944 range of model parameters. We highlight the significance of flow direction in explaining
 945 this discrepancy. The CAID material in a 2D model can only flow in two lateral directions.
 946 Accordingly, slab impact above a dense province inevitably divides the existing feature into
 947 two detached components and drives the resulting features in opposing directions. The
 948 additional degrees of freedom in a 3D calculation allow for flow of the CAID material to
 949 move so that the intrinsically denser material can become perforated by the arrival of a
 950 slab but not necessarily divided. Moreover, a mass of CAID material can be split from a
 951 perimeter location inwards to a radial hinge-point, around which the material will effectively
 952 rotate in a nearly horizontal plane while never separating into two detached masses.

953 The cases we present here are far from exhaustive in terms of the values considered for
 954 CAID material density contrast or viscosity contrast. Similarly, the values specified in our
 955 calculations for the key parameters governing plate formation represent a small subset from
 956 just one possible rheological description of mantle flow. However, the findings illustrate a
 957 few fundamental issues that are likely to prevail in further studies. Namely, the obtain-
 958 ing of LLSVP-type features from thermochemical mantle components is not an inevitable
 959 system outcome, particularly when a simultaneous requirement for a plate-like surface is

960 also imposed; the inclusion of a CAID component in a model can be either conducive to
 961 encouraging the generation of a plate-like surface velocity field or detrimental to producing
 962 plates; and intrinsically dense mantle components may remain rooted in the deep mantle
 963 while trapping enough heat within so that their relative contrast in density (and viscosity)
 964 with the surrounding mantle is much less than implied by the comparative properties at a
 965 common temperature.

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973 **Code Availability**

974 The computer code, STAGYY, used for all calculations described herein can be obtained
 975 upon reasonable request from P.J. Tackley.

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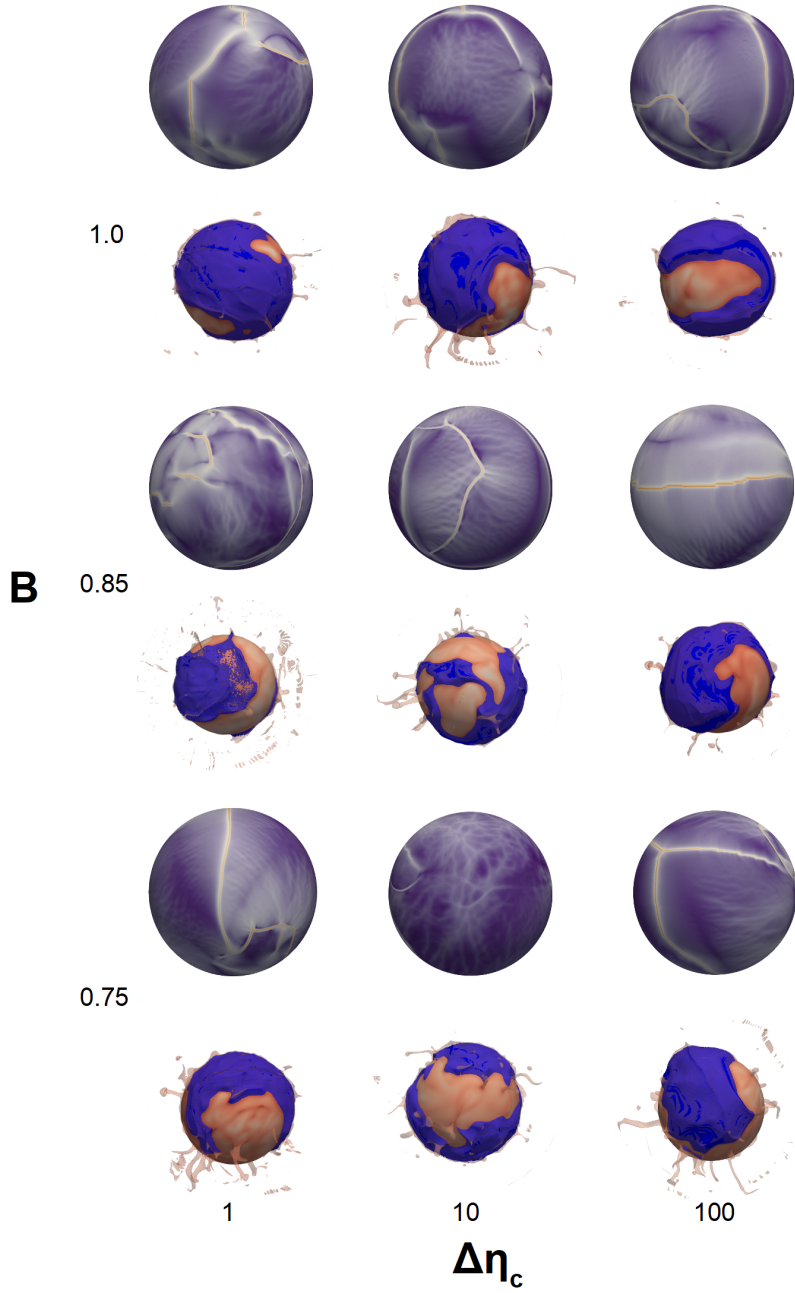


Figure 1. Snapshots of the nine uniform yield stress 3D cases featured in the study. The buoyancy number and intrinsic viscosity contrast for the CAID material and ambient mantle are indicated at the left and bottom of the figure, respectively. For each case, the viscosity field is shown at a depth of $0.005d$ juxtaposed with a (to scale) image of the mantle interior illustrating CAID material distribution (in blue) and thermal plumes (transparent red, non-dimensional temperature of 0.82). The viewing angle of the viscosity field and model interior pairs are the same and they are diametrically opposed to the viewing angle of the corresponding cases in Fig. 7.

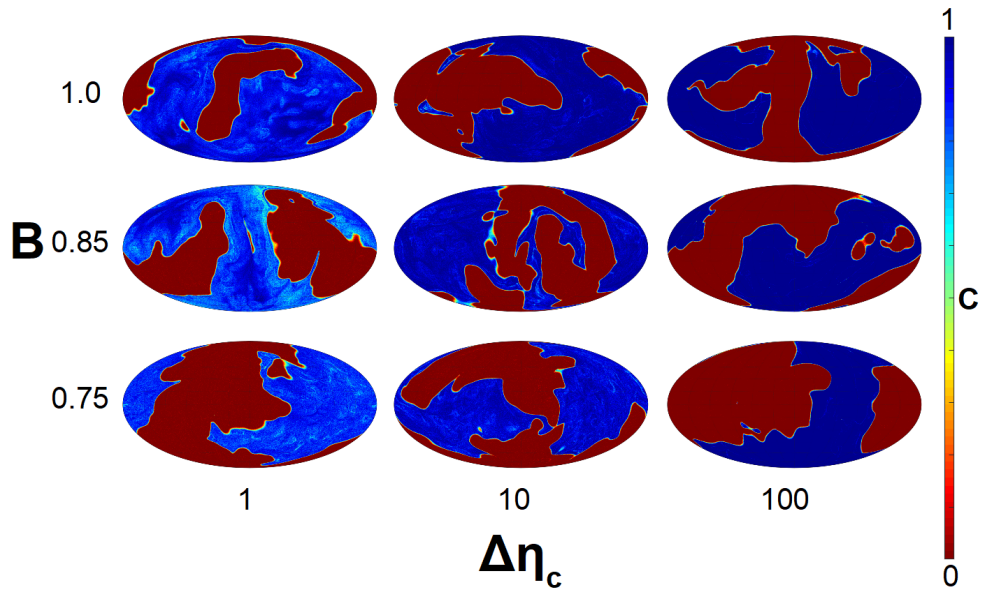


Figure 2. Mollweide projections of the composition field, C , on a surface $0.05d$ above the CMB. The panels correspond to the nine snapshots presented in Fig. 7 (and Supplementary Fig. 1). Buoyancy ratio is fixed in each row and the viscosity contrast between the intrinsically dense and ambient mantle (when both are at the CMB temperature) is fixed in each column. Blue corresponds to regions of the CMB blanketed by CAID material.

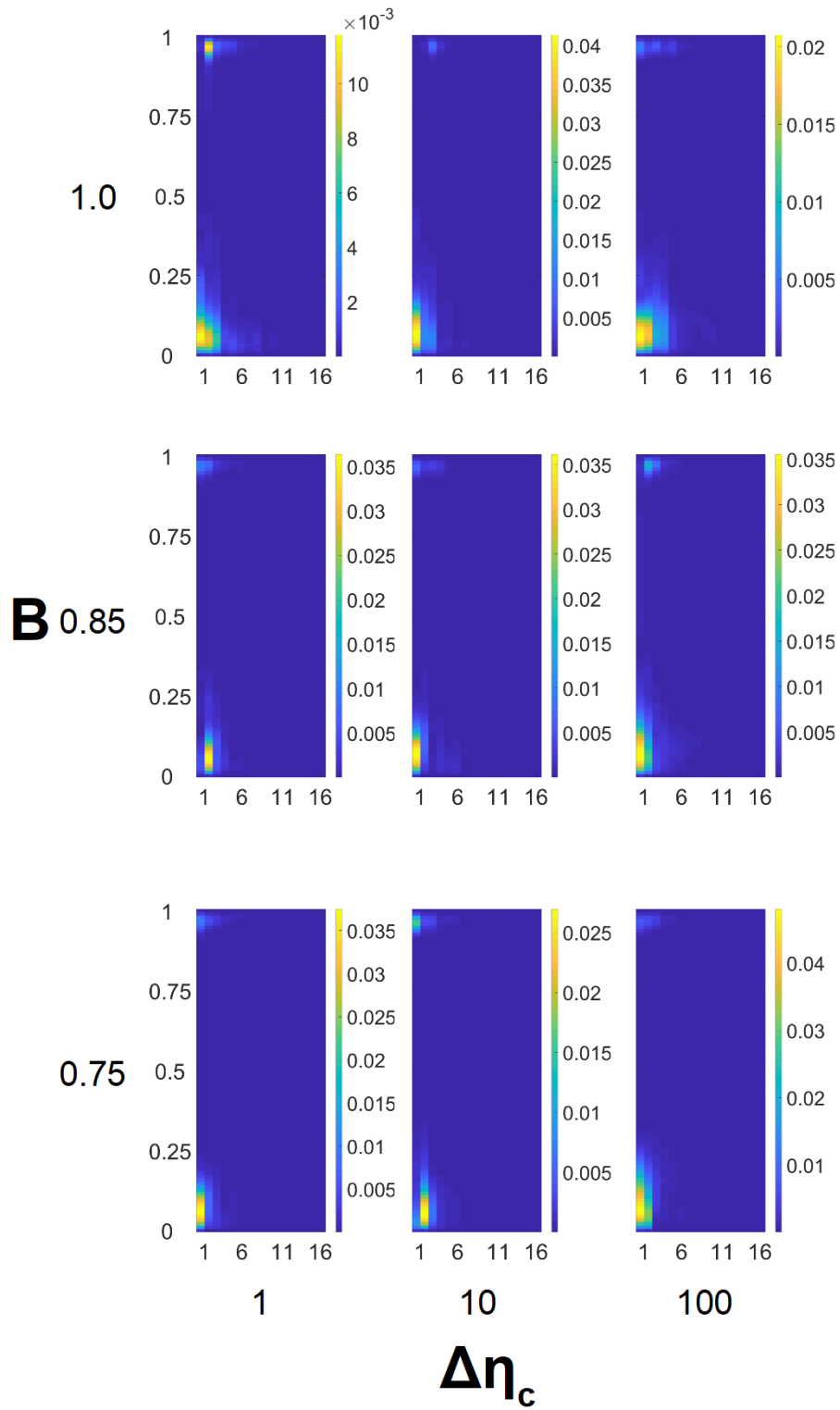


Figure 3. Power in the thermal fields presented in Fig. 7 (and Supplementary Fig. 1), as a function of spherical harmonic and non-dimensional height above the CMB.

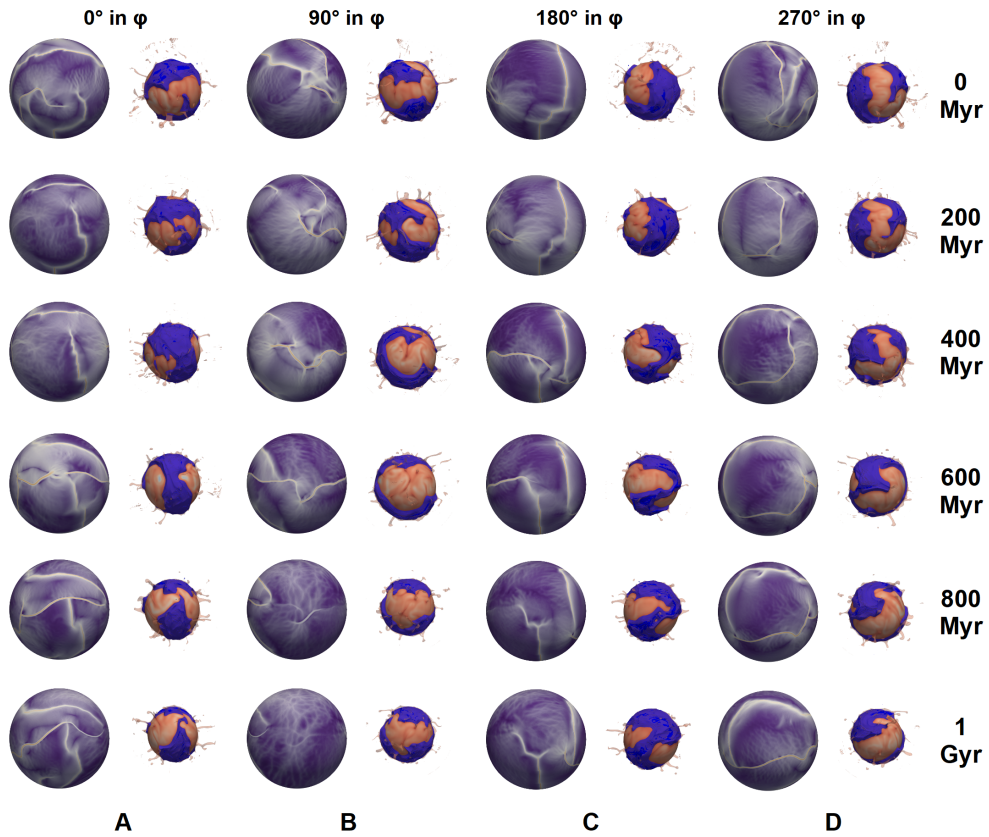


Figure 4. Snapshots of the near surface non-dimensional viscosity field and CAID material distribution at six different times (rows) throughout the evolution of Model 3DB0.75D10. The angle of rotation relative to a vertical axis through the centre of the sphere in the left-most column is indicated at the top of each column. The viewing angles used in Fig. 10 are presented for each time in the columns labelled A and C.

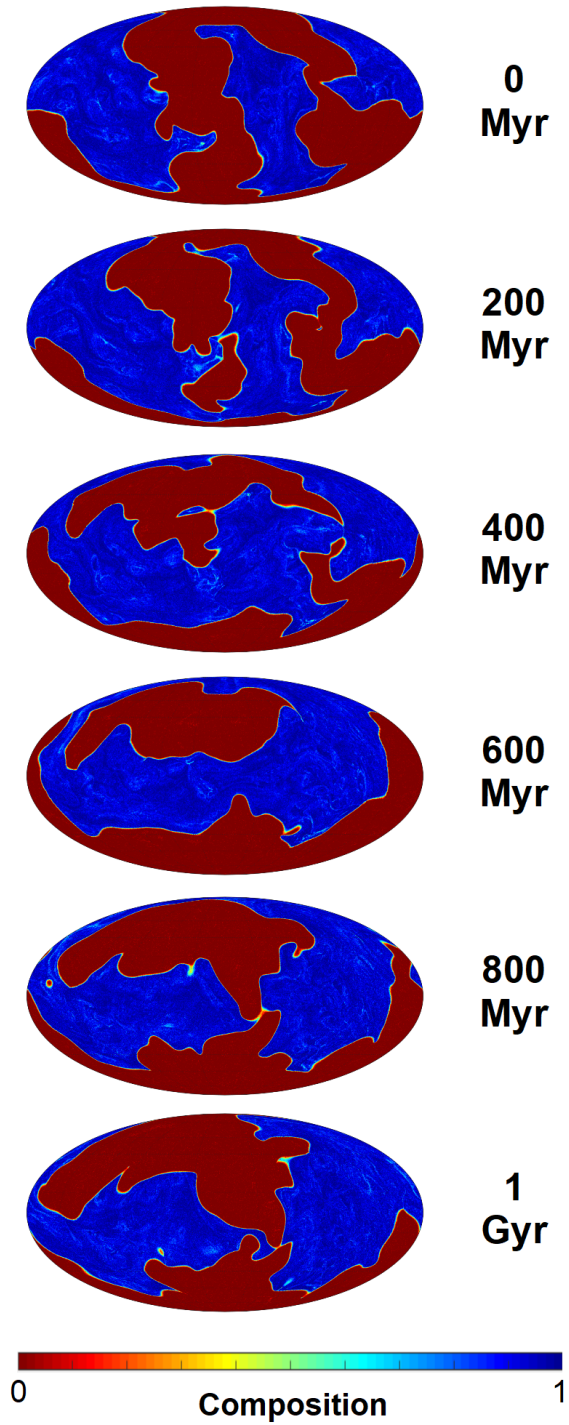


Figure 5. Mollweide projections of the composition field, C , on a surface $0.05d$ above the CMB from Model 3DB0.75D10. The panels correspond to the six snapshots presented in Fig. 10 (and Supplementary Fig. 4). Blue corresponds to regions of the CMB blanketed by CAID material.

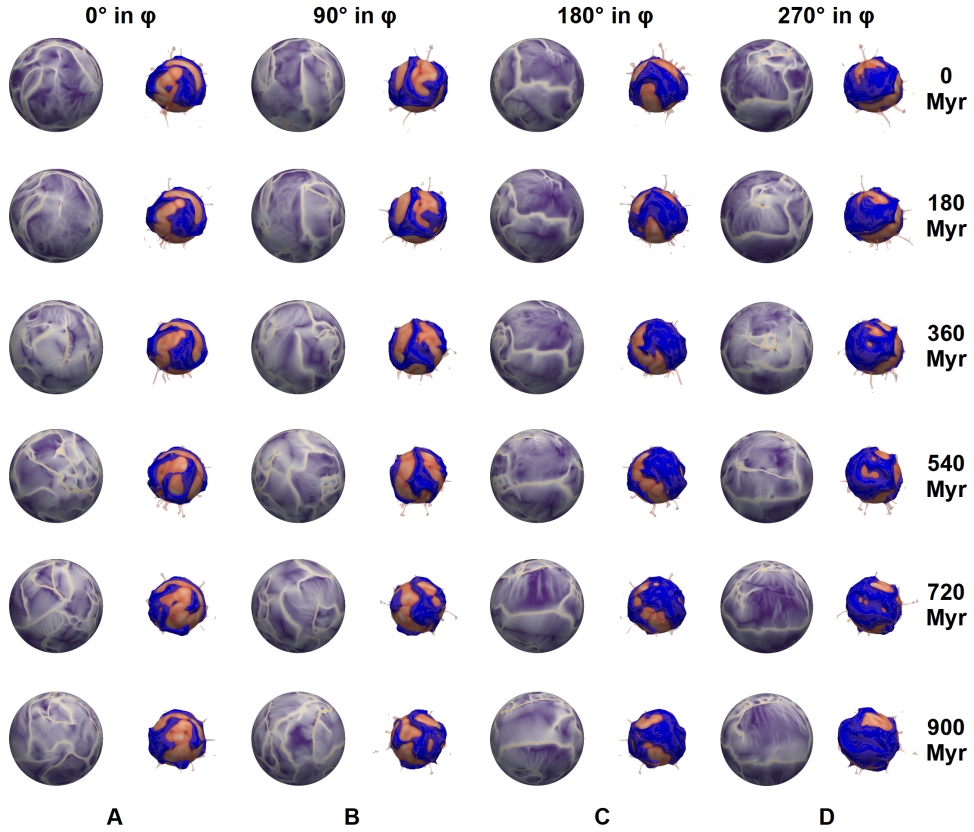


Figure 6. Snapshots of the near surface non-dimensional viscosity field and CAID material distribution at six different times (rows) throughout the evolution of Model 3DB0.75D100weak. The angle of rotation relative to a vertical axis through the centre of the sphere in the left-most column is indicated at the top of each column. The viewing angles used in Fig. 11 are presented for each time in the columns labelled A and C.

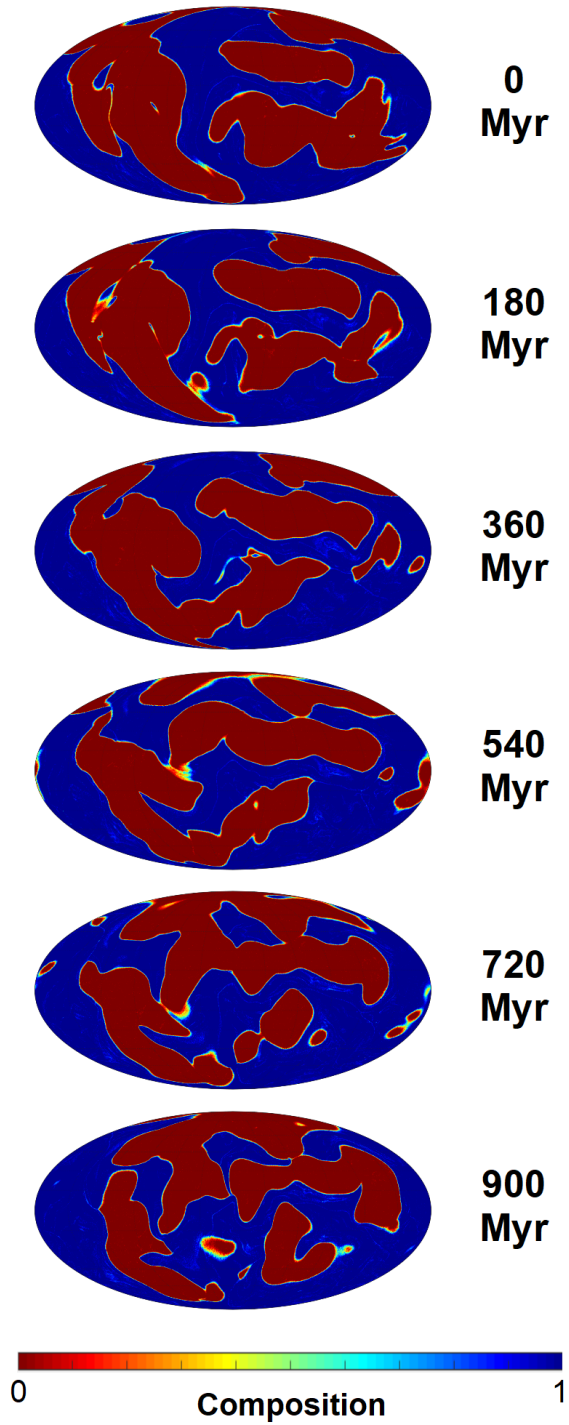


Figure 7. Mollweide projections of the composition field, C , on a surface $0.05d$ above the CMB from Model 3DB0.75D100weak. The panels correspond to the six snapshots presented in Fig. 11 (and Supplementary Fig. 6). Blue corresponds to regions of the CMB blanketed by CAID material.

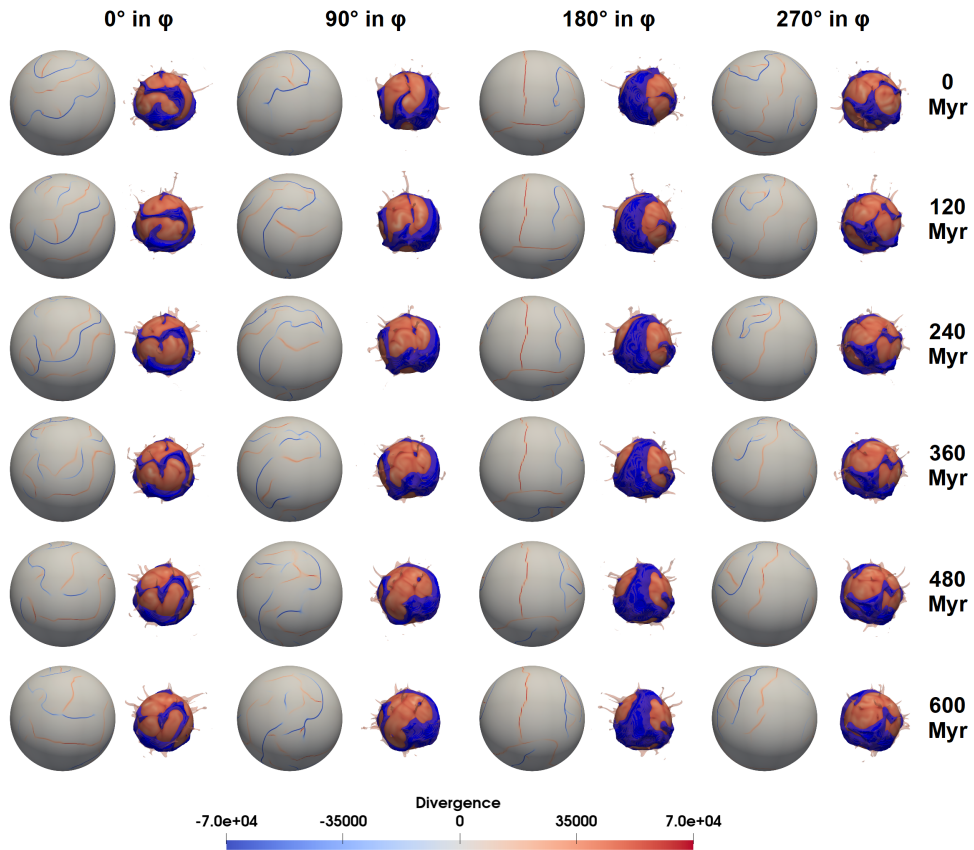


Figure 8. Snapshots of the near surface non-dimensional velocity divergence field and CAID material distribution at six different times (rows) throughout the evolution of Model 3DB0.75D100weak&reduced. The angle of rotation relative to a vertical axis through the centre of the sphere in the left-most column is indicated at the top of each column. The viewing angles used in Fig. 13 are presented for each time in the columns labelled 0° and 180° .

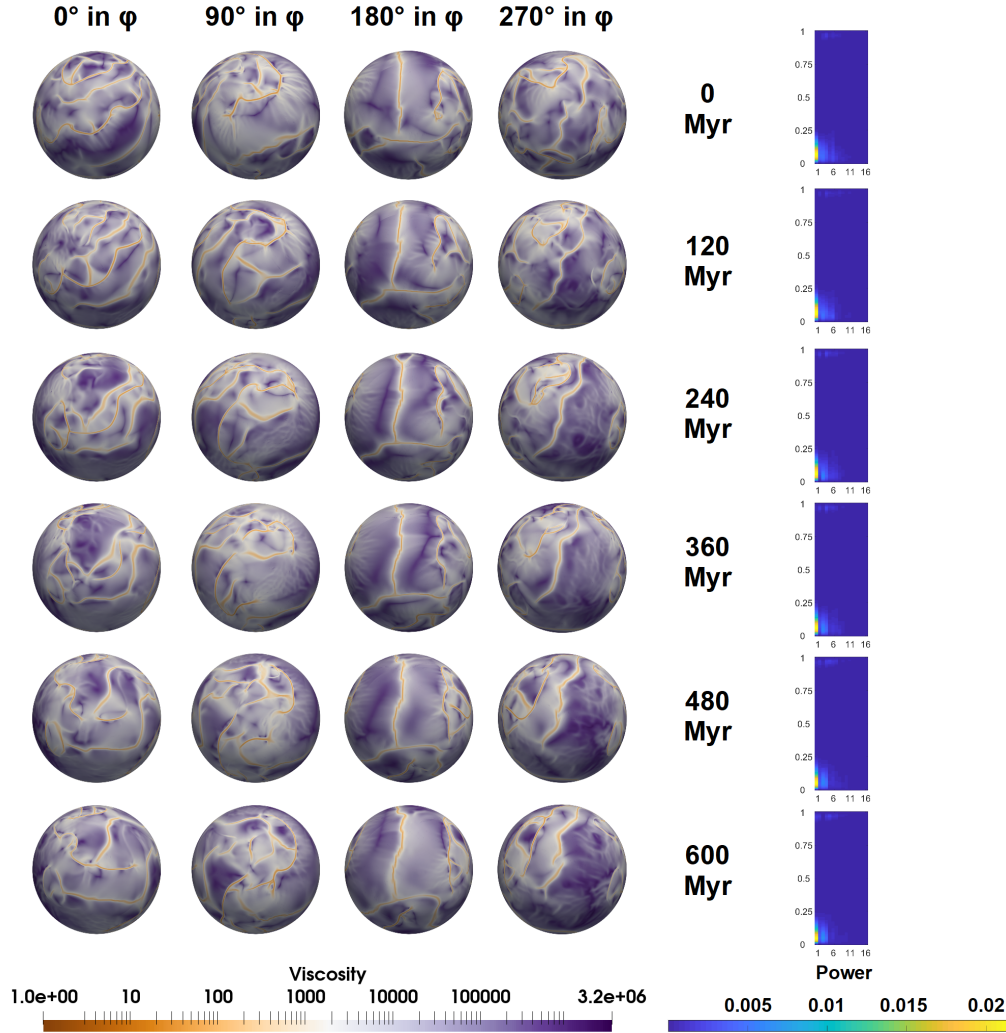


Figure 9. Snapshots of the near surface non-dimensional viscosity field and thermal power spectra at six different times (rows) throughout the evolution of Model 3DB0.75D100weak&reduced. The snapshots shown correspond to the velocity divergence field snapshots shown in Supplementary Fig. 8. The viscosity field is shown at a depth of $0.005d$. Four viewing angles are shown for each time, with the angle of rotation relative to the left most column indicated at the top of the figure. The power spectra of the temperature field at the corresponding time is shown in the right column as a function of non-dimensional height above the CMB and spherical harmonic degree.

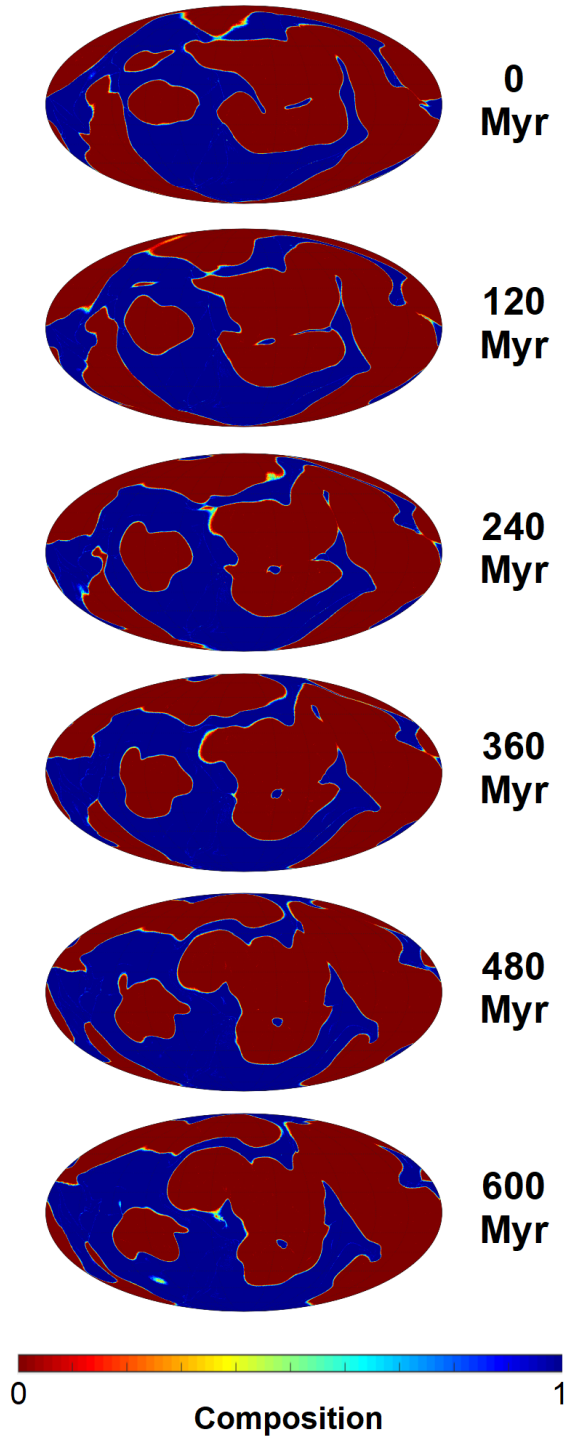


Figure 10. Mollweide projections of the composition field, C , on a surface $0.05d$ above the CMB from Model 3DB0.75D100weak&reduced. The panels correspond to the six snapshots presented in Fig. 13 (and Supplementary Fig. 8). Blue corresponds to regions of the CMB blanketed by CAID material.