

# Simulation of Internal Waves within an ALE ocean model: numerical challenges and modelling

Andreas Alexandris-Galanopoulos <sup>1</sup>    George Papadakis <sup>1</sup>

<sup>1</sup>Laboratory of Naval and Marine Hydrodynamics, National Technical University of Athens



<https://doi.org/10.5194/egusphere-egu26-10233>  
andreas\_alexandris@mail.ntua.gr  
EGU General Assembly 2026  
Vienna, Austria & Online | 38 May 2026

# Motivation: Internal Waves, Overturning, and Numerical Mixing

**Internal Solitary Waves** (ISW) are a demanding benchmark because they combine strong stratification, nonhydrostatic dispersion, pycnocline deformation, and in the most difficult cases, overturning and breaking.

- In a fixed vertical grid, repeated remapping across the pycnocline creates **spurious diapycnal mixing** (SDM).
- In a purely Lagrangian / isopycnal description, SDM is reduced, but true overturning can be overly suppressed because vertical mass transfer is part of the resolved dynamics during breaking.
- The **ALE** strategy [5] offers the flexibility to design the vertical grid motion so that SDM is reduced without overly negating physically relevant vertical fluxes.

# Motivation: Internal Waves, Overturning, and Numerical Mixing II

**Aim:** Reduce numerical mixing while retaining the vertical transfer needed for deforming and breaking waves.

# SLS in Generalized Vertical Coordinates I

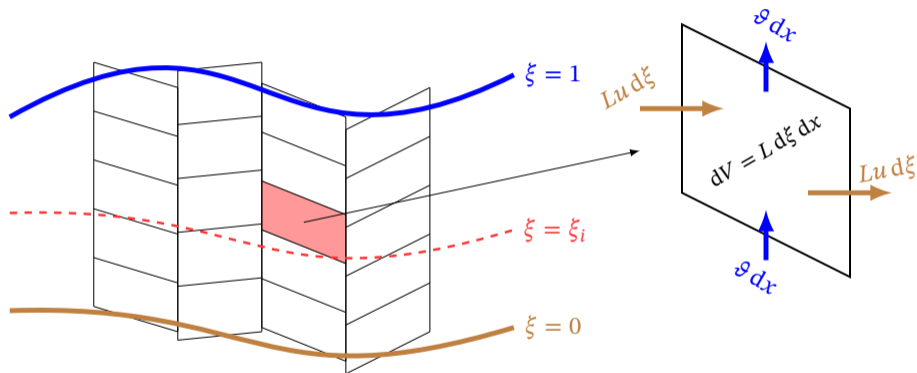
SLS is a hybrid Finite Volume (FV) / Finite Element (FE) solver for stratified, nonhydrostatic flows [3]. The vertical mesh is described by the map  $z(x, y, \xi, t)$ , where  $x, y$  are the horizontal coordinates, and  $\xi$  is the vertical parametric argument that labels the layers:

The local layer thickness is  $L = \frac{\partial z}{\partial \xi}$ , and the *Generalized Continuity Equation* states:

$$\underbrace{\frac{\partial L}{\partial t}}_{\text{volume change}} + \underbrace{\nabla_H \cdot (L\mathbf{u})}_{\text{Lagrangian impulse}} + \underbrace{\frac{\partial \vartheta}{\partial \xi}}_{\text{cross-layer coupling}} = 0$$

where  $L\mathbf{u}$  is the horizontal volume flux through a moving layer, while  $\vartheta$  is the **dia-surface ALE flux** and measures how much fluid crosses the moving layers.

# SLS in Generalized Vertical Coordinates II



Sketch of the FV fluxes in SLS. The horizontal (Lagrangian) flux is  $Lu$  and the vertical ALE flux is  $\vartheta$ .

# Why spurious diapycnal mixing appears I

For a passive density field with no physical diffusion ( $\frac{D\rho}{Dt} = 0$ ), the variance  $\iiint \rho^2 V$  should be conserved. Any decay of the discrete variance is therefore a measure of numerical mixing [2]:

$$\frac{d}{dt} \iiint \rho^2 dV \sim - \iiint |\vartheta| \Delta z |\partial_z \rho|^2 dV \leq 0$$

So SDM increases when:

$$|\vartheta| \text{ is large, } \quad \Delta z \text{ is coarse, } \quad |\partial_z \rho| \text{ is large.}$$

This gives the design principle for ALE movement: keep  $\vartheta$  moderate, and concentrate resolution near the pycnocline where  $|\partial_z \rho|$  is large.

# Variational ALE: mesh update and cost functional I

The GCE separates the mesh evolution into horizontal Lagrangian transport and a cross-layer ALE correction. We write within the timestep  $\Delta t = t^{n+1} - t^n$  the update as:

$$z^{n+1} = z_{lag}^* - \Delta t \vartheta$$

where  $z_{lag}^*$  denotes the mesh position predicted by the Lagrangian part of the GCE. To design the ALE scheme, the  $\vartheta$  in SLS is obtained by minimizing the functional [2]:

$$\mathcal{F}(\vartheta) = \iiint \left[ \underbrace{T_{ref} a_\vartheta \vartheta^2}_{\text{Lagrangian bias}} + \underbrace{\frac{1}{\Delta t} \|\mathbf{A}_S \nabla(z^{n+1} - z_{ref})\|^2}_{\text{mesh regularity}} + \underbrace{\frac{a_M}{\Delta t} \left( M \frac{\partial z^{n+1}}{\partial \xi} \right)^2}_{\text{adaptive refinement}} \right] dx d\xi$$

$$\mathbf{A}_S = \begin{bmatrix} \sqrt{a_x} \Delta x & & \\ & \sqrt{a_y} \Delta y & \\ & & \sqrt{a_\xi} \Delta \xi \end{bmatrix}, \quad \begin{array}{l} z_{ref} \\ M(x, y, \xi, t) \\ T_{ref} \stackrel{\text{def}}{=} \sqrt{\frac{h \rho_0}{g(\rho_{max} - \rho_{min})}} \end{array} \quad \begin{array}{l} : \\ : \\ : \end{array} \quad \begin{array}{l} \text{Reference grid} \\ \text{Monitor function} \\ \text{Characteristic time scale} \end{array}$$

# Variational ALE: mesh update and cost functional II

The parameters entering the functional are:

- $a_\vartheta$ : Controls Lagrangian bias.
- $a_x, a_y, a_\xi$ : set the smoothing strength in the horizontal and vertical directions.
- $a_M$ : weights the adaptive refinement term.

The monitor function is chosen so that mesh resolution is increased in areas with large density gradients:  $M = |\partial_\xi \rho| / |\partial_\xi \rho|_{max}$

# Elliptic problem for the ALE flux I

Based on the calculus of variations [4], the minimizer of  $\mathcal{F}$  satisfies the following elliptic problem:

$$A\vartheta - \nabla \cdot (\mathbf{B}\nabla\vartheta) = R$$

where  $A, \mathbf{B}, R$  are coefficients that do not depend on  $\vartheta$ .

## ALE update within one timestep :

1. **Lagrangian step:** compute the Lagrangian GCE fluxes to get  $z_{lag}^*$
2. **Elliptic problem:** solve for  $\vartheta$  to minimize  $\mathcal{F}$
3. **ALE update:** use this optimal  $\vartheta$  in the vertical fluxes.

# Test case I: ISW over a submerged wedge I

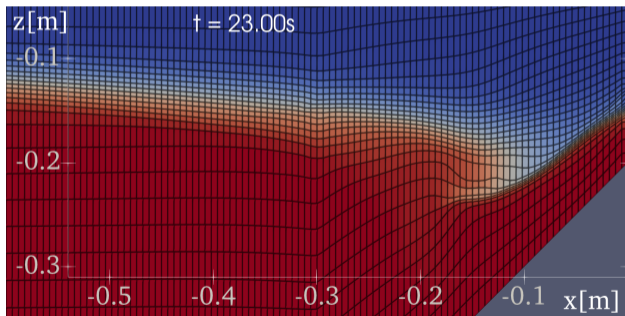
This test isolates the interaction between an ISW and steep topography. The wave remains coherent, the pycnocline undergoes strong local deformation, and we can compare with results from [6].

## Setup

- ISW with thick pycnocline.
- Submerged wedge with a  $45^\circ$  slope.
- SLS simulations: ALE scheme with  $a_\theta = 0.01$  ,  $a_x = a_\xi = 1$  ,  $a_M = 10$

## What it tests

- Ability of the ALE mesh to concentrate near sharp density gradients.
- Suppression of SDM while maintaining good mesh quality.



ISW–wedge interaction: the ALE mesh remains concentrated around the deformed pycnocline while keeping the layers smooth

# Test case II: Breaking-wave results and physical interpretation I

This test examines the performance in the breaking-wave regime, where strong nonlinear deformation and overturning occur. We adopt the configuration of [1, case 60] to study whether the ALE scheme can resolve the overturning with minimal SDM.

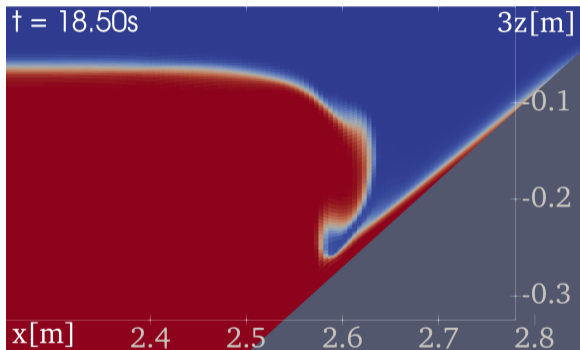
## Setup

- An ISW propagating towards a sloping bottom
- Plunging breaking mechanism with overturning

## Physics

- Induces significant dissipation
- Causes mixing through the pycnocline

# Test case II: Breaking-wave results and physical interpretation II



(0.01, 10): balanced

## Challenges

- Highly sensitive to SDM
- Exposes limitations of Lagrangian / Eulerian approaches

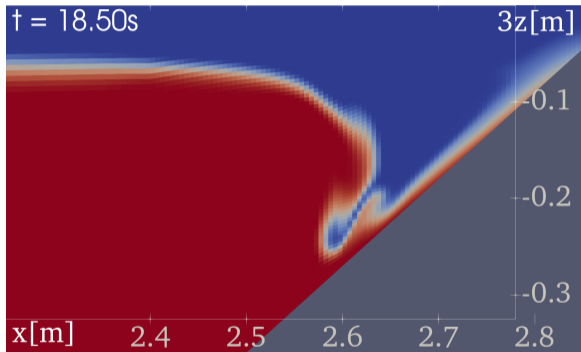
## Parameter effect

- $a_x, a_\xi = 1$  fixed
- $(a_\vartheta, a_M)$  varying between runs

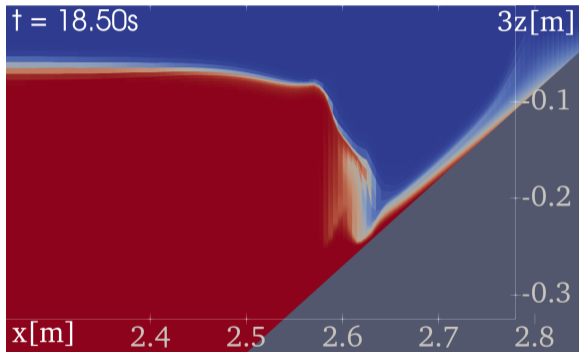
## Takeaway

- **Moderate Lagrangian bias + monitor function refinement** gives best behaviour

# Test case II: Breaking-wave results and physical interpretation III

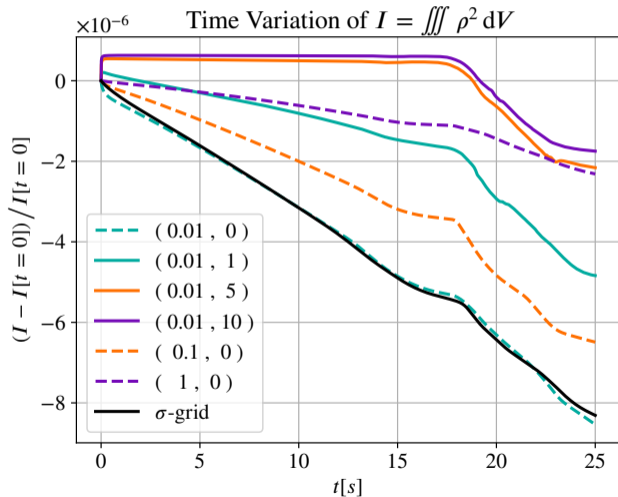


(0.01, 0): overly diffusive



(1, 0): overly constrained

# Test case II: Effect on Spurious Diapycnal Mixing (SDM) I



## Quantitative assessment

- Monitor-based refinement significantly reduces SDM up to the point of breaking
- Excessive Lagrangian bias reduces SDM but suppresses the overturning

## Key insight

- A **moderate Lagrangian bias**, combined with refinement, achieves the best balance between: **physical fidelity** and **low spurious mixing**

# Conclusions and outlook I

- The variational ALE movement gives a compact way to combine three goals in one solve: Lagrangian dynamics, mesh smoothing, and gradient-tracking refinement.
- In the internal-wave benchmarks, SLS captures propagation, bottom effects, and breaking while keeping SDM under control.
- Analysis showed that the **monitor function** approach is especially effective in reducing SDM without suppressing vertical mass transfer.

**Future work** includes larger-scale ocean configurations, Coriolis effects, turbulence / mixing closures, and additional optimality criteria tailored to realistic ocean applications.

# Acknowledgments I

The authors gratefully acknowledge financial support from the Greek State Scholarships Foundation (IKY) under the Chrysovergis scholarship programme. The first author is a recipient of the 2024 IKY scholarship in the field of Physics, which fully supports his doctoral studies at the National Technical University of Athens.

This work was supported by computational time granted from the National Infrastructures for Research and Technology S.A. (GRNET S.A.) in the National HPC facility - ARIS - under project ID pr019009

# References I

- [1] Payam Aghsaei, Leon Boegman, and Kevin G Lamb. Breaking of shoaling internal solitary waves. *Journal of Fluid Mechanics*, 659:289–317, 2010.
- [2] Andreas Alexandris-Galanopoulos and George Papadakis. An ale approach to reduce spurious numerical mixing through variational minimizers: application to internal waves. *arXiv preprint arXiv:2511.20092*, 2025.
- [3] Andreas Alexandris-Galanopoulos, George Papadakis, and Kostas Belibassakis. A semi-lagrangian splitting framework for the simulation of non-hydrostatic free-surface flows. *Ocean Modelling*, 187:102290, 2024.
- [4] Izrail Moiseevitch Gelfand, Richard A Silverman, et al. *Calculus of variations*. Courier Corporation, 2000.
- [5] Stephen M Griffies, Alistair Adcroft, and Robert W Hallberg. A primer on the vertical lagrangian-remap method in ocean models based on finite volume generalized vertical coordinates. *Journal of Advances in Modeling Earth Systems*, 12(10):e2019MS001954, 2020.
- [6] Chih-Min Hsieh, Robert R Hwang, John R-C Hsu, and Ming-Hung Cheng. Numerical modeling of flow evolution for an internal solitary wave propagating over a submerged ridge. *Wave Motion*, 55:48–72, 2015.